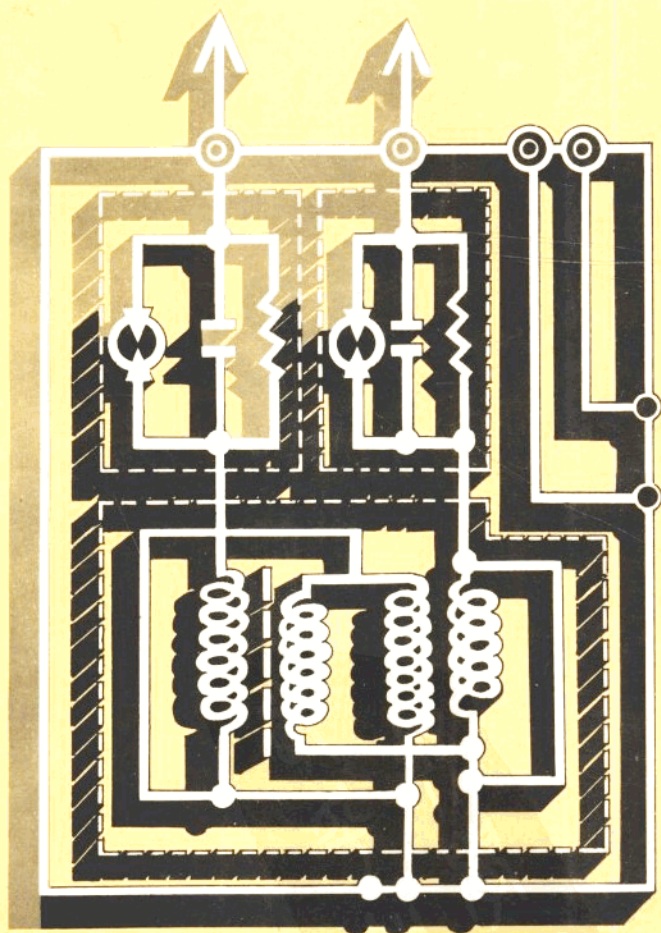


線性IC的應用、製作、實驗

林益海編譯・魏榮堂校閱



自 序

1. 本書係參考北川一雄所著オペアンプ IC 實驗と工作マニュアル一書及各大廠商 IC 資料編譯而成。

2. 在此感謝電機科主任魏榮堂先生之校閱及呂學成先生之提供資料。

3. 尤其感謝內人江雪惠女士給予各方面之協助。

4. 本書編譯如有錯誤之處，尚祈先進前輩不吝指正！

林益海 66年4月25日于台北工專

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1-1 線性 IC 使用說明表

目前市面上出品 IC 的廠商很多:

1. 快捷公司 (Fairchild Semiconductor) 縮寫為 FC
2. 國際半導體 (National Semiconductor) 公司縮寫為 NS
3. 德州儀器公司 (Texas Instrument) 縮寫為 TI
4. 摩托羅拉 (Motorola Semiconductor)
5. RCA
6. 西門子公司 (Simens)

每家公司之產品及代號各不相同例如:

FC 公司以 μ 代表

RCA 以 C 代表

TI 公司以 SN 代表

Motorola 以 MC 代表

Signetics 公司以 E 代表

Rytheon 公司以 R 代表

日本東芝以 T 代表

日本日電以 μP 代表

日立公司以 H 代表

三菱公司以 M 代表

NS 公司以 LM 代表

$\mu A741$ 是 FC 公司產品, 但其他公司亦仿造生產 $\mu A741$ 之命名, 而 $\mu A741$ 因為價錢便宜, 而且有下列之優點故應用極廣, 普遍

應用於市面上之成品。

1. 電路內附有短路保護。
2. 附有抵補 (off set) 電壓調整端子。
3. 輸入訊號範圍大。
4. 不必外加相位補償元件。

典型 $\mu A741$ 電氣特性如下圖所示。

Parameter 參數	Conditions ($T_A = +25^\circ\text{C}$, $V_S = \pm 15\text{V}$)	Value	Unit
Input offset voltage V_{OS}	Source resistance, $R_S \leq 10\text{k}\Omega$	1.0	mV
Input offset current I_{OS}		30	nA
Input bias current		100	nA
Input resistance Z_{in}		1000	k Ω
Large signal voltage gain A_{VOL}	$R_L \geq 2\text{k}\Omega$, $V_{out} = \pm 10\text{V}$	200,000	
Output voltage swing	$R_L \geq 10\text{k}\Omega$, $R_L \geq 2\text{k}\Omega$	± 14	V
		± 13	V
Input voltage range		± 13	V
Usable frequency range		1	MHz
Common-mode rejection ratio (CMRR)	$R_S \leq 10\text{k}\Omega$	90	dB
Supply voltage rejection ratio	$R_S \leq 10\text{k}\Omega$	30	$\mu\text{V/V}$
Power consumption		50	mW
Maximum internal power dissipation		≥ 300	mW
Transient response (unity gain)	$V_{in} = 20\text{mV}$, $R_L = 2\text{k}\Omega$ $C_L \leq 100\text{pF}$		
Rise time		0.3	μs
Overshoot		5.0	μs
Slew rate (unity gain)	$R_L \geq 2\text{k}\Omega$	0.5	V/ μs

圖 1-1

$\mu A741$ 內部電路圖及各腳:

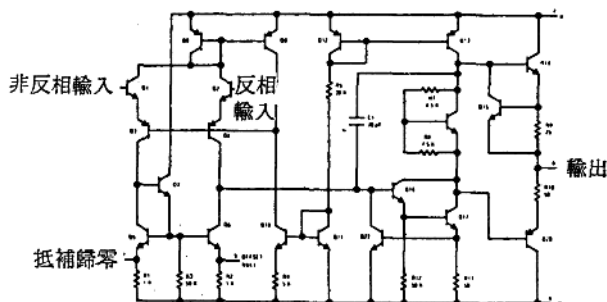


圖 1-2 $\mu A741$ 內部電路

1. Q_1, Q_2 為訊差放大器，輸入由基極（②腳及③腳輸入）。
2. Q_1, Q_2 的集極由偏壓二極體 Q_3 直接接到 V_+ 。射極接 Q_3 和 Q_4 。
3. Q_3 和 Q_4 為基極接地的訊差放大器，當為移位之用，其輸出加到 Q_{16} 當為驅動信號。 Q_{16} 和 Q_{17} 接成達靈頓電路。
4. Q_{16}, Q_{17} 集極的輸出驅動 Q_{14} ； Q_{14}, Q_{20} 為一互補式射極隨耦器；而 Q_{13} 為一定電流源。

5. Q_{14} 和 Q_{20} 間的移位工作由 Q_{16}, R_7 ($4.5K\Omega$)、 R_8 ($7.5K\Omega$) 來完成。

6. $\mu A741$ 的相位補償用 1 個 30 PF 的電容在內部完成。

7. $\mu A741$ 的抵補調整由 Q_5 和 Q_6 的射極間接一可變電阻而完成，其接法如右圖 1-3 所示。

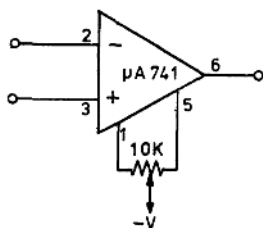


圖 1-3 $\mu A741$ 的抵補調整

- ②—③脚接輸入
 ④脚接正電源
 ①脚⑤脚可接一 $10k\Omega$ 可的變電阻供偏銷電壓調整之用。
- ⑥脚接輸出
 ⑦脚接負電源

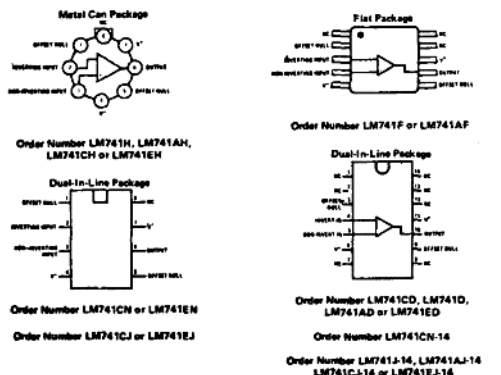


圖 1-4

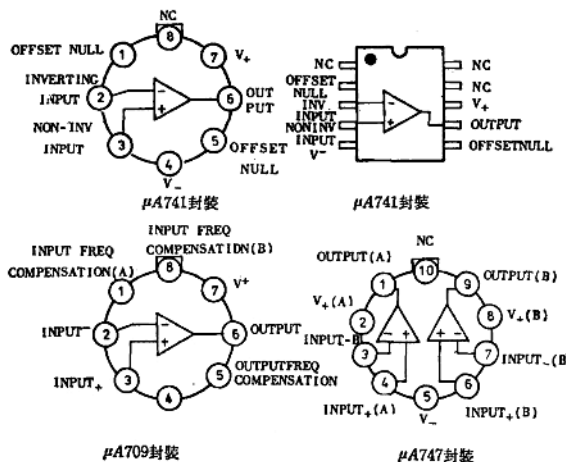


圖 1-5

NS 公司出產之 LM148 及 LM149 含有 4 個單獨 $\mu A741$ 如圖 1-6 下面各圖表即其圖示接法及電氣特性，可比照採用。

absolute maximum ratings (最大額定)

	LM148/LM148	LM248/LM249	LM348/LM349
Supply Voltage	±22V	±18V	±18V
Differential Input Voltage	±44V	±38V	±36V
Input Voltage	±22V	±18V	±18V
Output Short Circuit Duration (Note 1)	Continuous	Continuous	Continuous
Power Dissipation (P_D at 25°C) and Thermal Resistance (θ_{JA}), (Note 2)			
Molded DIP (N)	P_D θ_{JA}	— —	500 mW 150°C/W
Cavity DIP (D) (J)	P_D θ_{JA}	900 mW 100°C/W	900 mW 100°C/W
Flat Pack (F)	P_D θ_{JA}	675 mW 185°C/W	— —
Maximum Junction Temperature (T_{JMAX})	150°C	110°C	100°C
Operating Temperature Range	-55°C ≤ T_A ≤ +125°C	-25°C ≤ T_A ≤ +85°C	0°C ≤ T_A ≤ +70°C
Storage Temperature Range	-65°C to +150°C	-65°C to +150°C	-65°C to +150°C
Lead Temperature (Soldering, 60 seconds)	300°C	300°C	300°C

electrical characteristics (Note 3) 電氣特性

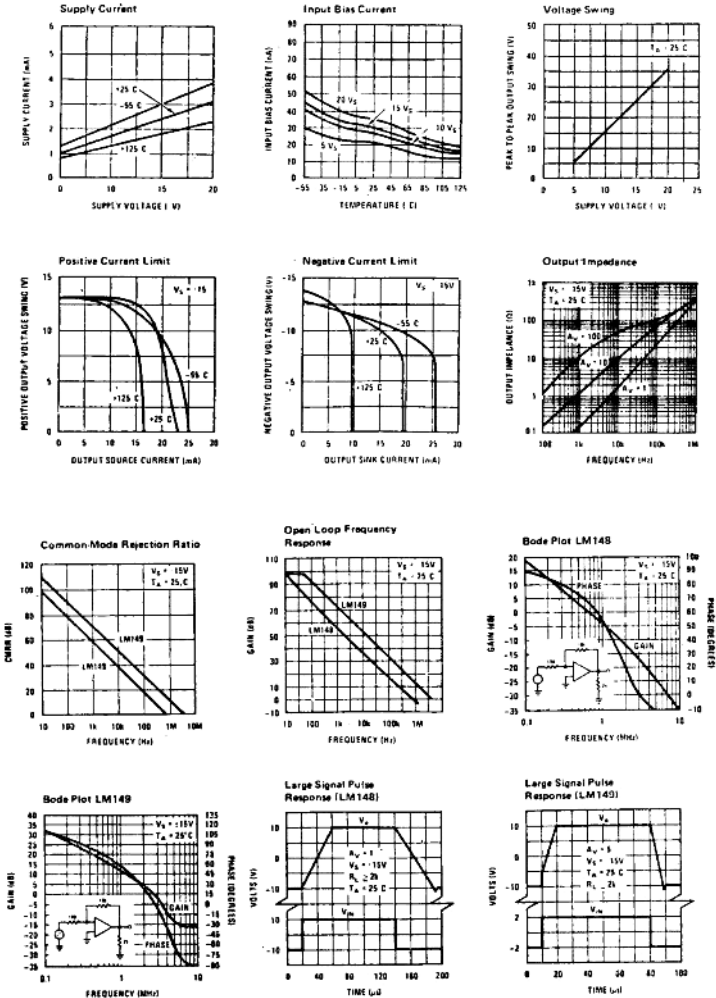
PARAMETER	CONDITIONS	LM148/LM149			LM248/LM249			LM348/LM349			UNITS
		MIN	TYP	MAX	MIN	TYP	MAX	MIN	TYP	MAX	
Input Offset Voltage	$T_A = 25^\circ\text{C}$, $R_S \leq 10\text{ k}\Omega$		5.0		1.2	6.0		1.5	6.0		mV
Input Offset Current	$T_A = 25^\circ\text{C}$		25		5	50		5	50		nA
Input Bias Current	$T_A = 25^\circ\text{C}$		25	100		200			200		nA
Input Resistance	$T_A = 25^\circ\text{C}$	0.8			0.8			0.8			M Ω
Supply Current All Amplifiers	$T_A = 25^\circ\text{C}$, $V_S = \pm 15\text{V}$			3.0		4.5			4.5		mA
Large Signal Voltage Gain	$T_A = 25^\circ\text{C}$, $V_S = \pm 15\text{V}$ $V_{OUT} = \pm 10\text{V}$, $R_L \geq 2\text{ k}\Omega$	50		25	50		25	50			V/mV
Amplifier to Amplifier Coupling	$T_A = 25^\circ\text{C}$, $f = 1\text{ Hz to } 20\text{ kHz}$ (Input Referred) See Crosstalk Test Circuit				20			20			dB
Small Signal Bandwidth	$T_A = 25^\circ\text{C}$ LM148 series LM149 series		1.0		1.0			1.0			MHz
Phase Margin	$T_A = 25^\circ\text{C}$ LM148 series ($A_V = 1$) LM149 series ($A_V = 5$)		30		45			30			degrees
Slew Rate	$T_A = 25^\circ\text{C}$ LM148 series ($A_V = 1$) LM149 series ($A_V = 5$)		0.5		0.5			0.5			V/ μs
Output Short Circuit Current	$T_A = 25^\circ\text{C}$		25		25			25			mA
Input Offset Voltage	$R_S \leq 10\text{ k}\Omega$		6.0		7.5			7.5			mV
Input Offset Current			75		125			100			nA
Input Bias Current			325		500			450			nA
Large Signal Voltage Gain	$V_S = \pm 15\text{V}$, $V_{OUT} = \pm 10\text{V}$, $R_L > 2\text{ k}\Omega$	25		15				15			V/mV
Output Voltage Swing	$V_S = \pm 15\text{V}$, $R_L = 10\text{ k}\Omega$ $R_L = 2\text{ k}\Omega$	±12 ±10	±12 ±10		±12 ±10	±12 ±10		±12 ±10	±12 ±10		V
Input Voltage Range	$V_S = \pm 15\text{V}$	±12			±12			±12			V
Common-Mode Rejection Ratio	$R_S \leq 10\text{ k}\Omega$	70			70			70			dB
Supply Voltage Rejection	$R_S \leq 10\text{ k}\Omega$	77			77			77			dB

Note 1: Any of the amplifier outputs can be shorted to ground indefinitely; however, more than one should not be simultaneously shorted as the maximum junction temperature will be exceeded.

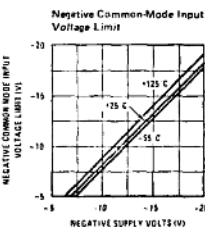
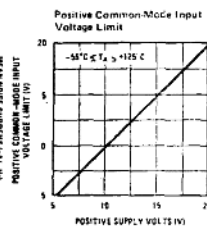
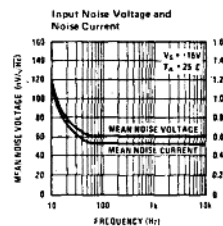
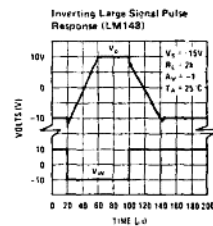
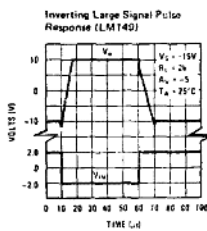
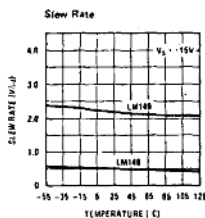
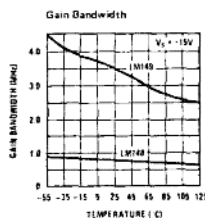
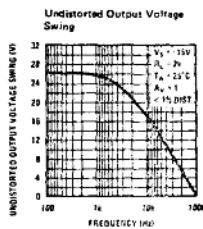
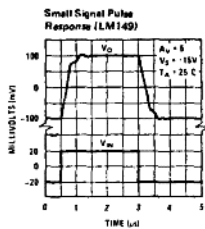
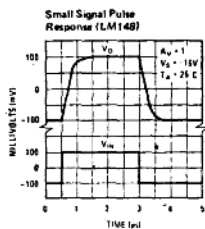
Note 2: The maximum power dissipation for these devices must be derated at elevated temperatures and is dictated by T_{JMAX} , θ_{JA} , and the ambient temperature, T_A . The maximum available power dissipation at any temperature is $P_D = (T_{JMAX} - T_A)/\theta_{JA}$ or the 25°C $P_{D(MAX)}$, whichever is less.

Note 3: These specifications apply for $V_S = \pm 15\text{V}$ and over the absolute maximum operating temperature range ($T_L \leq T_A \leq T_H$) unless otherwise noted.

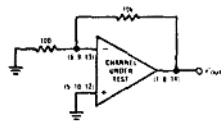
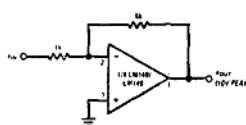
typical performance characteristics (典型運用特性)



typical performance characteristics (con't) (典型運用特性)



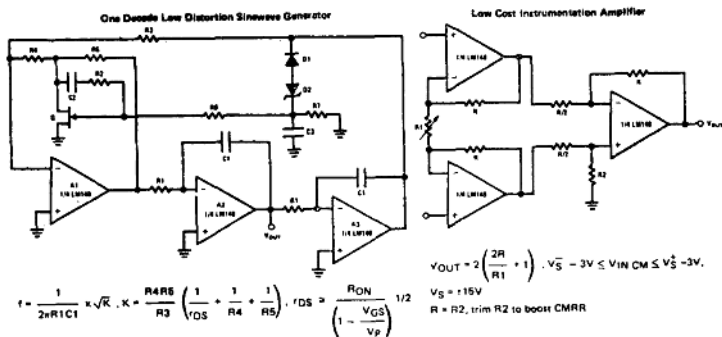
cross talk test circuits



$$\text{Crosstalk} = -20 \log \frac{e^+_{OUT}}{101 \times e^-_{OUT}} \text{ (dB)}$$

$V_S = \pm 15V$

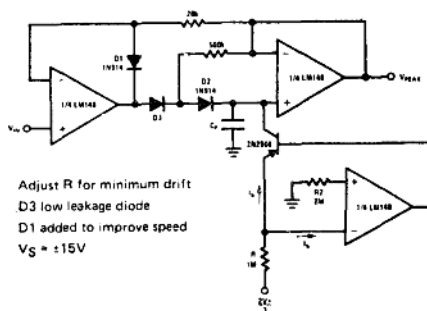
typical applications-LM148 (典型應用例)



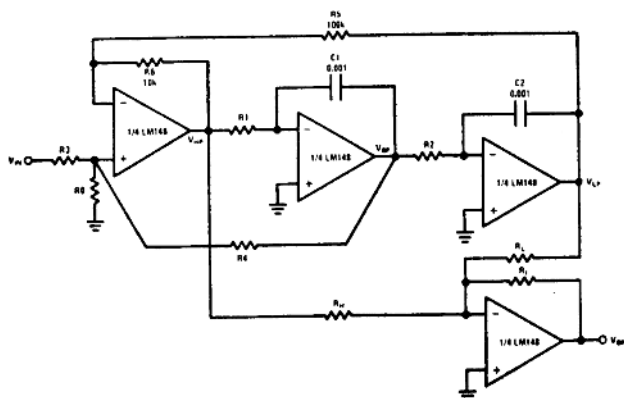
$f_{MAX} = 5 \text{ kHz}$, THD $\leq 0.03\%$
 $R_1 = 100k \text{ pot.}$, $C_1 = 0.0047\mu F$, $C_2 = 0.01\mu F$, $C_3 = 0.1\mu F$, $R_2 = R_6 = R_7 = 1M$,
 $R_3 = 5.1k$, $R_4 = 12\Omega$, $R_5 = 240\Omega$, $Q = NS5102$, $D_1 = 1N914$, $D_2 = 3.6V \text{ avalanche}$
 diode (ex. LM103), $V_S = \pm 15V$
 A simpler version with some distortion degradation at high frequencies can be
 made by using A1 as a simple inverting amplifier, and by putting back to back
 zeners in the feedback loop of A3.

typical applications-LM148 (con't) (典型應用例)

Low Drift Peak Detector with Bias Current Compensation



Universal State-Space Filter



Tune Q through R_0 .

For predictable results: $f_0 Q \leq 4 \times 10^4$

Use Band Pass output to tune for Q

$$\frac{V(s)}{V_{IN}(s)} = \frac{N(s)}{D(s)} \quad D(s) = s^2 + \frac{s\omega_0}{Q} + \omega_0^2$$

$$N_{HP}(s) \approx s^2 H_{OHP}, \quad N_{BP}(s) = \frac{-s\omega_0 H_{OHP}}{Q}, \quad N_{LP} = \omega_0^2 H_{OLP}$$

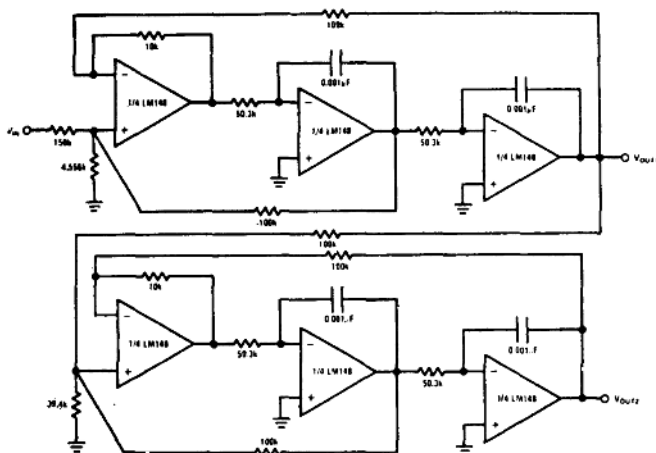
$$f_0 = \frac{1}{2\pi} \sqrt{\frac{R_6}{R_5}} \sqrt{\frac{1}{t_1 t_2}}, \quad t_1 = R_1 C_1, \quad Q = \left(\frac{1 + R_4/R_3 + R_4/R_5}{1 + R_6/R_5} \right) \left(\frac{R_6}{R_5} \frac{t_1}{t_2} \right)^{1/2}$$

$$f_{NOTCH} = \frac{1}{2\pi} \left(\frac{R_H}{R_L t_1 t_2} \right)^{1/2}, \quad H_{OHP} = \frac{1 + R_6/R_5}{1 + R_3/R_0 + R_3/R_4}, \quad H_{OHP} = \frac{1 + R_4/R_3 + R_4/R_0}{1 + R_3/R_0 + R_3/R_4}$$

$$H_{OLP} = \frac{1 + R_5/R_6}{1 + R_3/R_0 + R_3/R_4}$$

typical applications-LM148 (con't) (典型應用例)

A 1 kHz 4 Pole Butterworth

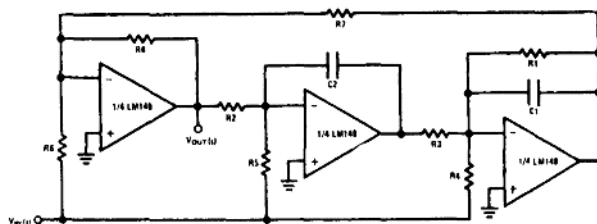


Use general equations, and tune each section separately

 $Q_{1stSECTION} = 0.541, Q_{2ndSECTION} = 1.306$

The response should have 0 dB peaking

A 3 Amplifier Bi-Quad Notch Filter



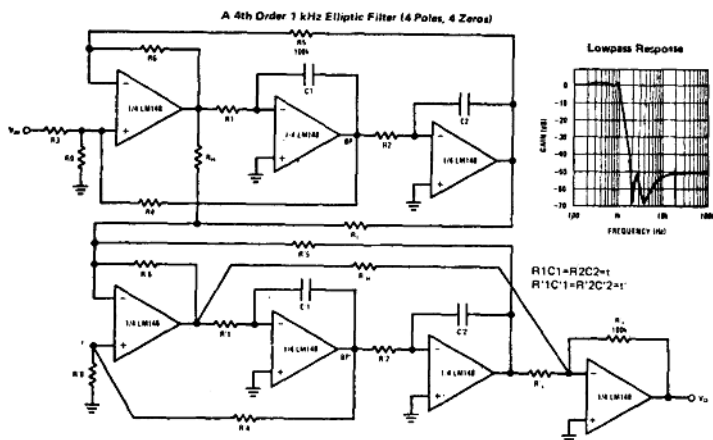
$$Q = \sqrt{\frac{R8}{R7}} \times \frac{R1C1}{\sqrt{R3C2R2C1}} \cdot f_o = \frac{1}{2\pi} \sqrt{\frac{R8}{R7}} \times \frac{1}{\sqrt{R2R3C1C2}} \cdot f_{NOTCH} = \frac{1}{2\pi} \sqrt{\frac{R6}{R3R5R7C1C2}}$$

$$\text{Necessary condition for notch: } \frac{1}{R6} = \frac{R1}{R4R7}$$

Ex: $f_{NOTCH} = 3 \text{ kHz}, Q = 5, R1 = 270k, R2 = R3 = 20k, R4 = 27k, R5 = 20k, R6 = R8 = 10k, R7 = 100k, C1 = C2 = 0.001\mu F$

Better noise performance than the state-space approach

typical applications-LM148 (con't) (典型應用例)



$$f_C = 1 \text{ kHz}, f_Z = 2 \text{ kHz}, f_p = 0.543, f_z = 2.14, Q = 0.841, f'_p = 0.987, f'_z = 4.92, Q' = 4.403, \text{normalized to ripple BW}$$

$$f_p = \frac{1}{2\pi} \sqrt{\frac{R_6}{R_5} \times \frac{1}{t}} \times \frac{1}{2\pi} \sqrt{\frac{R_H}{R_L} \times \frac{1}{t}} \times \left(\frac{1 + R_4/R_3 + R_4/R_0}{1 + R_6/R_5} \right) \times \sqrt{\frac{R_6}{R_5} \cdot Q'} = \sqrt{\frac{R_6}{R_5} \cdot \frac{1 + R_4/R_0}{1 + R_6/R_5 + R_6/R_p}}$$

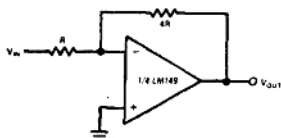
$$R_p = \frac{R_H R_L}{R_H + R_L}$$

*Use the BP outputs to tune Q, Q' ; tune the 2 sections separately

$R1 = R2 = 92.6k, R3 = R4 = R5 = 100k, R6 = 10k, R0 = 107.8k, R_L = 100k, R_H = 155.1k,$
 $R1' = R2' = 50.9k, R4' = R5' = 100k, R6' = 10k, R0' = 5.78k, R'_L = 100k, R'_H = 248.12k, R1' = 100k.$ All capacitors are $0.001\mu F$.

typical applications-LM149

Minimum Gain to Insure LM149 Stability



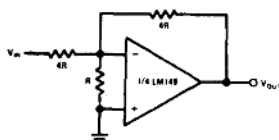
$$A_{CL}(s) = \frac{V_{OUT}}{V_{IN}} = \frac{4}{\left(1 + \frac{5}{A_{OL}(s)}\right)}$$

$$V_O \Big|_{V_{IN}=0} \approx \pm 5 V_{OS}$$

Power BW = 40 kHz

Small Signal BW = G BW/5

The LM149 as a Unity Gain Inverter



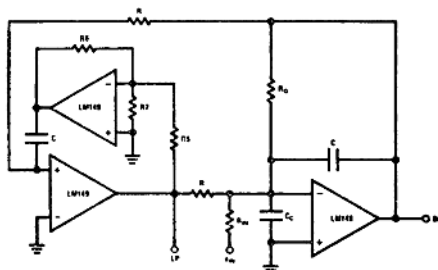
$$A_{CL}(s) = \frac{V_{OUT}}{V_{IN}} = \left(\frac{1}{1 + \frac{6}{A_{OL}(s)}} \right)$$

$$V_O \Big|_{V_{IN}=0} \approx \pm 5 V_{OS}$$

Small signal BW = G BW/5

typical applications-LM149 (con't) (典型應用例)

Non-inverting-Integrator Bandpass Filter (非反相積分帶通濾波器)



For stability purposes: $R7 = R6/4$, $10R6 = R5$, $Cc = 10C$

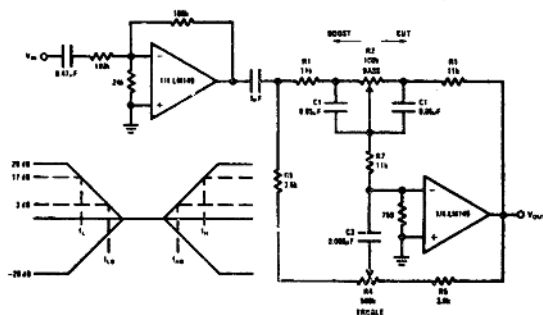
$$f_0 = \frac{1}{2\pi} \sqrt{\frac{R5}{R6}} \times \frac{1}{RC}, Q = \frac{RQ}{R}, \text{Hogp} = \frac{RQ}{R_{IN}}$$

$$(f_{OMAX}), Q_{MAX} = 20 \text{ kHz}, 10$$

Better Q sensitivity with respect to open loop gain variations than the state variable filter.

$R7, Cc$ added for compensation

Active Tone Control with Full Output Swing (No Slew Limiting at 20 kHz)(音調控制)



$V_S = \pm 15V$, $V_{OUT(MAX)} = 9.1 \text{ VRMS}$.

$f_{MAX} = 20 \text{ kHz}$, $THD \leq 1\%$

Duplicate the above circuit for stereo

$$f_L = \frac{1}{2\pi R2 C1}, f_{LB} = \frac{1}{2\pi R1 C1}$$

$$f_H = \frac{1}{2\pi R5 C3}, f_{HB} = \frac{1}{2\pi (R1 + 2R7) C3}$$

Max Bass Gain $\approx (R1 + R2)/R1$

Max Treble Gain $\approx (R1 + 2R7)/R5$

as shown: $f_L \approx 32 \text{ Hz}$, $f_{LB} \approx 320 \text{ Hz}$

$f_H \approx 11 \text{ kHz}$, $f_{HB} \approx 1.1 \text{ Hz}$