Fracture Mechanics, Creep and Fatigue Analysis

edited by

C. Becht IV

S. K. Bhandari

B. Tomkins



Library of Congress Catalog Number 88-71016 Statement from By-Laws: The Society shall not be responsible for statements or opinions advanced in papers . . . or printed in its publications (7.1.3) Any paper from this volume may be reproduced without written permission as long as the authors and publisher are acknowledged.

Copyright © 1988 by
THE AMERICAN SOCIETY OF MECHANICAL ENGINEERS
All Rights Reserved
Printed in U.S.A.

FOREWORD

The primary objective of the Design and Analysis Committee of ASME Pressure Vessels and Piping Division is to provide a forum for the dissemination of information and the advancement of current theories and practices in the design and analysis of pressure vessels, piping systems and related components. This is achieved largely through presentations and discussions at the annual PVP Division conference, as well as through encouragement and sponsorship for publication of the technical literature.

This publication is comprised of technical papers on various topics of interest to the pressure vessels and piping industries and includes international contributions by authors from Canada, the People's Republic of China, France, the Federal Republic of Germany, the United Kingdom, and the United States of America.

All the papers in this volume were prepared for presentation in technical sessions developed under the auspices of the Design and Analysis Committee for the 1988 ASME Pressure Vessels and Piping Division Conference in Pittsburgh, Pennsylvania.

This volume, "Fracture Mechanics, Creep and Fatigue Analysis" is presented in three chapters:

Creep and Fatigue Analysis

Fracture Mechanics

Flaw Evaluation in Fast Breeder Reactors

The first chapter contains: An approximate technique for assessing multiaxial stress-relaxation using uniaxial behavior corrected with multiaxiality correction factors, an evaluation of high cycle fatigue service of piping fillet weld joints using piping code stress intensification factors and endurance limits, and a case study in which six years of pressure fluctuation data from two chemical plant towers were used to derive a pressure amplitude spectrum which was applied to a CCT speciman to determine crack growth rate under representative variable-amplitude loading.

The second chapter contains: Development of a three-dimensional failure assessment diagram which uses crack extension as a third independent variable, a fatigue crack growth analysis of a 45 lateral to evaluate the margin to fatigue failure based on a postulated defect and a 40 year service life, extension of net section plastic collapse evaluation of flawed pipe to permit evaluation of arbitrarily shaped cracks, and an elastic-plastic evaluation of a prototype metal-matrix fuel waste disposal container subjected to water pressure in a 1000 meter deep vault.

The third chapter presents developments in the European Fast Breeder Reactor Program to establish the leakbefore-break concept for application to austenitic stainless steel piping and vessels in liquid sodium service.

C. Becht IV

CONTENTS

Estimation of Multiaxial Stress Relaxation Using Isochronous Curves	
R. Seshadri	1
Suitability for Steady-State Vibrations of Piping Fillet Welds — A Fracture Mechanics Approach	
M. D. Ratiu, G. Hau, and W. Bak	11
Fatigue Crack Growth: A Case Study of Synthetic Tower Spectrum Loading	
Jianguo Cheng and Jin Qian	19
Three-Dimensional Failure Assessment Diagram Method to Flaw Evaluation	
K. K. Yoon	25
Fatigue Crack Growth Analysis of a 45° PWR — Lateral	
P. Taupin and F. Flamand	31
Plastic Collapse Analysis of Pipes With Arbitrarily Shaped Circumferential Cracks	
N. G. Cofie and C. H. Froehlich	39
Structural Performance of a Nuclear Fuel Waste Disposal Container	
L. K. Grover	47
Comparative Elastic Analyses of a Cracked Elbow	
P. Jamet, M. Stamm, S. Bhandari, L. Gruter, and D. Green	55
Comparative Stress Intensity Factor Calculations for a Thermally Shocked Plate	
D. Green and K. Bethge	59
Stable Crack Growth in Large Austenitic Pipes Under Bending	
L. Gruter, J. P. Debaene, C. Faidy	65
The Treatment of Residual Stress in Defect Assessment of Austenitic Fast Reactor Structures	
R. H. Leggett and D. G. Hooton	71
Fatigue Crack Growth on Straight Pipes Under Thermal Shocks	
C. Poette	77
The Development of a Validated Leak-Before-Break Methodology for Application to Fast Reactor Sodium	
Boundary Components	
B. Tomkins	83

ESTIMATION OF MULTIAXIAL STRESS RELAXATION USING ISOCHRONOUS CURVES

R. Seshadri

Industrial Systems Engineering University of Regina Regina, Saskatchewan, Canada

ABSTRACT

The state of stress in pressure components is usually In evaluating component damage and multiaxial. inelastic deformations for temperature service, it is essential to understand how the stresses relax with time. Most of the available stress-relaxation data are based on relaxation tests that use a one-dimensional configuration in which the strain is held fixed, and the decrease of the initial stress is measured as a function of time. therefore useful to relate the multiaxial relaxation behavior of a pressure component to the uniaxial relaxation behavior so that the available relaxation data can be used effectively. This paper discusses a simple approximate technique for assessing multiaxial stress-relaxation by utilizing the isochronous curves in conjunction with "multiaxiality correction factors".

NOMENCLATURE

- A = material constant for time-hardening creep relationship
- B = material constant for steady-state creep relationship
- E = modulus of elasticity
- m = material constant
- n = material constant
- α = stress-ratio (σ_2/σ_1)
- $\beta = \text{stress-ratio} (\sigma_3/\sigma_1)$
- $\bar{\epsilon}$ = equivalent-strain
- ε_{+} : = total-strain in the i-direction (i = 1,2,3)
- ε_{i} = elastic-strain in the i-direction (i = 1,2,3)

- ε_{i} = plastic-strain in the i-direction (i = 1,2,3)
- ϵ' = creep-strain in the i-direction (i = 1,2,3) first stage of creep
- ε" = creep-strain in the i-direction (i = 1,2,3) second stage of creep
- $\bar{\sigma}$ = equivalent stress
- $\sigma^{(i)}$ = initial stress before relaxation occurs
- σ_1 σ_2 = principal stresses σ_3
- τ = time
- τ_{1d} = time-scale (uniaxial)
- τ_{id} = time-scale (multiaxial), i = 2, or 3
- i. = multiaxiality parameter, i = 2 for two-dimensional constraint and i = 3 for three-dimensional constraint.
- ν = Poisson's ratio

1. INTRODUCTION

Proper estimation of the amount of creep-damage incurred during elevated temperature operation of pressure components requires an understanding of the stress-relaxation behaviour. Relaxation is the decay and redistribution of stresses in a component operating at elevated temperatures when the total strain in one or more directions is held fixed. The accumulated creep deformations are essentially counterbalanced by equivalent changes in elastic strains. Some practical examples of multiaxial