Adriano A. G. Siqueira · Marco H. Terra Marcel Bergerman

# Robust Control of Robots

**Fault Tolerant Approaches** 

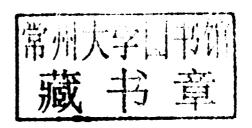




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Fault Tolerant Approaches





Dr. Adriano A. G. Siqueira Engineering School of São Carlos University of São Paulo Av. Trabalhador Sãocarlense 400 São Carlos SP 13566-590 Brazil

e-mail: siqueira@sc.usp.br

Dr. Marco H. Terra Engineering School of São Carlos University of São Paulo Av. Trabalhador Sãocarlense 400 São Carlos SP 13566-590 Brazil

e-mail: terra@sc.usp.br

Dr. Marcel Bergerman CMU Robotics Institute 5000 Forbes Avenue Pittsburgh PA 15213-3890 USA

e-mail: marcel@cmu.edu

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To My Wife Flaviane and My Son João Vítor A. A. G. S.

To My Son Diego

M. H. T.

To My Family

M. B.

# **Preface**

The world is teeming with machines that grow crops, process our food, drive us to work, assemble products, clean our homes, and perform thousands of other daily tasks. They are complex systems built on a myriad of electronic, mechanic, and software components, each one prone to malfunction and even fail at any given time. Robust, fault tolerant control of such machines is key to guaranteeing their performance and avoiding accidents. Robotic manipulators, in particular, are especially important when it comes to robust, fault tolerant control. Our society relies on these machines for a large variety of industrial operations; any unscheduled downtime caused by a faulty component can have significant economic costs—not to mention the consequences of a potential injury.

Robust and fault tolerant systems have been studied extensively by academic and industrial researchers and many different design procedures have been developed in order to satisfy rigorous robustness criteria. An important class of robust control methods, introduced by G. Zames in 1980, is based on  $\mathcal{H}_{\infty}$  theory. The main concept behind this approach is the robustness of the control system to internal uncertainties and exogenous disturbances. Hundreds of works were written extending the seminal results obtained by Prof. Zames. Some of them are sufficiently elegant and effective to be of value in industrial environments. Transforming theory into practice, however, is not a trivial task, as the mathematics involved in robust control can be daunting. This monograph proposes to bridge the gap between robust control theory and applications, with a special focus on robotic manipulators.

The book is organized in nine chapters. In Chap. 1 we present the experimental robot manipulator system used throughout the book to illustrate the various control methodologies discussed. We also present there the simulation and control environment we use to develop and test the methodologies. The environment, named CERob for Control Environment for Robots, is a freeware included with this book and available at http://extras.springer.com. The remaining eight chapters are divided in three parts. Part 1 (Chaps. 2–4) deals with robust control of regular, fully-actuated robotic manipulators. Part 2 (Chaps. 5–6) deals with robust fault tolerant control of robotic manipulators, especially the post-failure control

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problem. Finally, Part 3 (Chaps. 7–9) deals with robust control of cooperative robotic manipulators.

In Chaps. 2, 3, and 4 we present model-based linear, non-linear, adaptive, and neural network-based  $\mathcal{H}_{\infty}$  controllers for robotic manipulators. Models based on the Lagrange–Euler formulation and neural networks are used to enable robust control of robots where performance, stability and convergence are guaranteed. One interesting scenario in robot modeling is when the neural network works as a complement of the Lagrange–Euler equations to decrease modeling errors. In these chapters we also explore the use of output feedback controllers, motivated by the fact that in some cases sensors are not available to measure the full array of variables needed for robot control.

In Chaps. 5 and 6 we present strategies to control the position of underactuated manipulators, or manipulators equipped with both regular (active) and failed (passive) joints based on linear parameter-varying models and linear matrix inequalities, and also on game theory. The objective in these chapters is to demonstrate that the system is able to reject disturbances while achieving good position tracking performance. For robotic systems subject to faults, we present a fault tolerant methodology based on linear systems subject to Markovian jumps. We describe in detail the design of  $\mathcal{H}_2, \mathcal{H}_\infty$ , and mixed  $\mathcal{H}_2/\mathcal{H}_\infty$  trajectory-following controllers for manipulators subject to several consecutive faults.

In Chaps. 7, 8, and 9 we consider actuated and underactuated cooperative manipulators. One of the most important issues in the robust control of cooperative manipulators is the relationship between disturbance rejection and control of squeeze forces on the load, particularly when the manipulator is underactuated.

Throughout the book we illustrate the concepts presented with simulations and experiments conducted with two 3-link planar robotic manipulators especially designed to pose as fully-actuated or underactuated devices.

São Carlos, Brazil São Carlos, Brazil Pittsburgh, USA Adriano A. G. Siqueira Marco H. Terra Marcel Bergerman

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# **Acronyms**

AAA Active-active-active
AAP Active-active-passive
ADP Adaptive controller
ANN Artificial neural network
APA Active-passive-active
APP Active-passive-passive

CERob Control environment for robots

CM Center of mass

CMCE Cooperative manipulator control environment

DC Direct current

DLCC Dynamic load carrying capacity dll Dynamically linked library

DOF Degree of freedom

FDI Fault detection and isolation FSJF Free-swinging joint fault

FTMCE Fault tolerant manipulator control environment

GTH Game theory controller

 $\begin{array}{lll} \text{HBC} & \text{Hybrid controller} \\ \text{HIN} & \text{Linear } \mathcal{H}_{\infty} \text{ controller} \\ \text{JPF} & \text{Joint position fault} \\ \text{JVF} & \text{Joint velocity fault} \\ \text{LJF} & \text{Locked joint fault} \end{array}$ 

LMI Linear matrix inequality
LPV Linear parameter-varying
MJLS Markov jump linear systems

MLP Multilayer perceptron MTD Mean time to detection NET Neural network controller NLH Nonlinear  $\mathcal{H}_{\infty}$  controller PAA Passive-active-passive

xvi Acronyms

PCI Peripheral component interconnect

PD Proportional-derivative PPA Passive-passive-active

RBFN Radial basis function network
UARM Underactuated robotic manipulator

UMCE Underactuated manipulator control environment

VSC Variable structure controller

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# Chapter 1 Experimental Set Up

## 1.1 Introduction

The field of Robotics is, by its very nature, an experimental one. No robot control methodology can be deemed to perform satisfactorily if it has not been validated on an actual physical system. In this book we illustrate all control methods presented by applying them to custom-designed robotic manipulators.

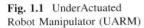
The manipulators are two 3-link open-chain, serial link arms built by Ben Brown, Jr. from Pittsburgh, PA, USA, which we name the UARMs, or UnderActuated Robotic Manipulators (Fig. 1.1). The two most salient features of these manipulators are that their joint motors possess very low friction and are equipped with on/off brakes, thus allowing us to simulate a variety of joint failure conditions. We created an open source MATLAB®-based UARM simulator that readers can utilize to validate the control methodologies presented throughout the chapters. The simulator includes also the Matlab source code for all methods described. This Control Environment for Robots (CERob) is in fact more than just a standard simulator; in our laboratory, control methodologies can be validated in the virtual manipulators and then transferred to the actual ones at the click of a button.

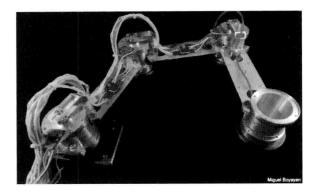
In the first part of this chapter we describe in detail the UARM hardware and its dynamic model. In the second part we describe the basic functionality of CERob. Specific details on CERob as it applies to particular controllers are presented in the pertinent chapters.

# 1.2 UARM Experimental Manipulator

## 1.2.1 Hardware

Each UARM is a 3-link planar, open-chain, serial-link manipulator. They are equipped with low-friction DC motors directly connected to the links, with no gearboxes. When the motors are powered, the joints behave as regular





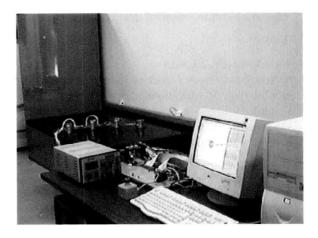
fully-actuated ones; and when they are not powered, the joints can move essentially freely and dub as unactuated or passive joints. The manipulator's configuration (fully-actuated or underactuated) can then be defined at will in real time by simply powering or not each joint. Additionally, the joints are equipped with diaphragm-based on/off brakes, which can be used to simulate locking-type faults or to enable underactuated manipulator position control. Joints are numbered from 1 to 3, with joint 1 fixed to a smooth marble table. A dummy load can be attached to the end-effector's cup-shaped housing to provide for meaningful manipulation experiments. The entire system resides on a horizontal plane and runs on a thin air film that reduces to practically zero the friction with the table. Pressurized air pumps and computer-controlled solenoid valves complete the hardware of the system.

Incremental encoders with quadrature decoding, located at the top of each joint, are used to measure the relative angular joint positions. The angular velocities are computed via numerical differentiation and low-pass filtering. Such procedure is known to result in measurement noise and can therefore lead to poor position control performance. This is one of our motivations to use output feedback control laws, where only joint position measurements are used.

An equipment board provides a mounting surface for the motor amplifiers, valves and air pressure regulators for brake and flotation air, and a custom interface board. Two feeding voltages are supplied by a power unit: 48 V/20 A for the motors, and 24 V/1 A for the interface board. A kill switch ("emergency stop") mounted in a small yellow enclosure can be located remotely, and controls the power supply to the interface board and amplifiers. The equipment board also provides a location where the UARM can be secured for safe transport without disconnecting it from the rest of the system. Figure 1.2 shows the complete system, with the robot manipulator, the equipment board, the power supply unit, and the control computer.

The communication between the control computer and the hardware is performed by a PCI (Peripheral Component Interconnect) input-output board from Motenc. This device is able to control up to eight servo motors simultaneously

Fig. 1.2 Complete UARM hardware setup



(eight robot joints). The Motenc board connects to the custom interface board via two 50-conductor ribbon cables. The features available on this board include:

- 8 differential encoder inputs, 32-bit resolution;
- 8 analog outputs, ±10 V range, 13-bit resolution;
- 8 analog inputs, ±5 V range, 14-bit resolution;
- 100 digital I/O (68 inputs and 32 outputs) in four 50-pin headers, opto-22 compatible;
- +5 V available on headers, fused (resetable), max current 2 A;
- Programmable timer interrupts;
- · Watchdog timer;
- Hardware board ID for multiple board applications;
- Filters at digital inputs to remove high frequency noise; and
- Hardware ESTOPs.

The designer can access the board I/O channels by using the *dll* library provided by the manufacturer. Table 1.1 shows the MATLAB®-based functions we developed to communicate with the UARM hardware. Most of the time only four commands are necessary to control the robot: those to set the desired voltages, read the current encoders' values, reset the encoders, and activate or release the brakes, at the same time activating or inhibiting the motors.

Table 1.1 MATLAB®-based functions for control of the UARM

Function	Description	
set_dac_all_stg([v1 v2 v3])	Set the desired voltages to the DC motors	
get_position	Read joint encoders	
set_encoder_one_stg(enc, value)	Set encoder to the specified value	
setbrakemotor(value)	Activate/release brakes and activate/inhibit motors	

Electrical and mechanical details of the system are as follows:

### 1. Links

Link length: 20.3 cm

• Arm length from center of joint 1 to center of tip: 60.96 cm

• Joint size: 76 mm (diameter) × 86 mm (height)

Joint mass: 670 g

• Tip mass: 220 g (default, customized by user)

• Link mass: 30 g (excluding wires, air hoses, and connectors).

### 2. Joint motors

Model: Kollmorgen RBE-1213 brushless DC

Nominal voltage: 48 V CC
 Winding resistance: 2.4 Ω

Torque constant: 0.14 Nm/A

• Peak torque: 2.8 Nm

Back EMF constant: 15 V/kRPMContinuous stall torque: 0.35 Nm

• Motor mass: 344 g

• Rotor inertia: 0.0000148 kg m<sup>2</sup>.

# 3. Motor amplifiers

Model: Elmo SBA 10/100H-4

· Peak current: 20 A

• Continuous current: 10 A

Supply voltage: 20–90 V CC

• Current-to-voltage constant (adjustable): 1.61 A/V.

### 4. Brakes

• Type: air actuated diaphragm

• Pressure: 100 psi (700 kPa) max.

Valves: Clippard model EVO-3M, 24 VDC, 0.67 W

• Torque: 2.8 Nm max.

# Optical encoders

• Model: Hewlett Packard HEDS 9040-T00

Disk: HEDS 6140-T08Lines: 2000/revolution

• Counts: 8000/revolution after quadrature decoding.

## 6. Air bearings

Orifice diameter: 0.36 mmAir gap: approx. 0.08 mm

• Air supply pressure: 100 psi (700 kPa) max.