SEBORG • EDGAR • MELLICHAMP • DOYLE

Process Dynamics and Control

International Student Version

Process Dynamics and Control

Third Edition

International Student Version

Dale E. Seborg

University of California, Santa Barbara

Thomas F. Edgar

University of Texas at Austin

Duncan A. Mellichamp *University of California, Santa Barbara*

Francis J. Doyle III

University of California, Santa Barbara



Copyright © 2011 John Wiley & Sons (Asia) Pte Ltd

Cover image from © Vladimir Vladimirov/iStockphoto

Founded in 1807, John Wiley & Sons, Inc. has been a valued source of knowledge and understanding for more than 200 years, helping people around the world meet their needs and fulfill their aspirations. Our company is built on a foundation of principles that include responsibility to the communities we serve and where we live and work. In 2008, we launched a Corporate Citizenship Initiative, a global effort to address the environmental, social, economic, and ethical challenges we face in our business. Among the issues we are addressing are carbon impact, paper specifications and procurement, ethical conduct within our business and among our vendors, and community and charitable support. For more information, please visit our website: www.wiley.com/go/citizenship.

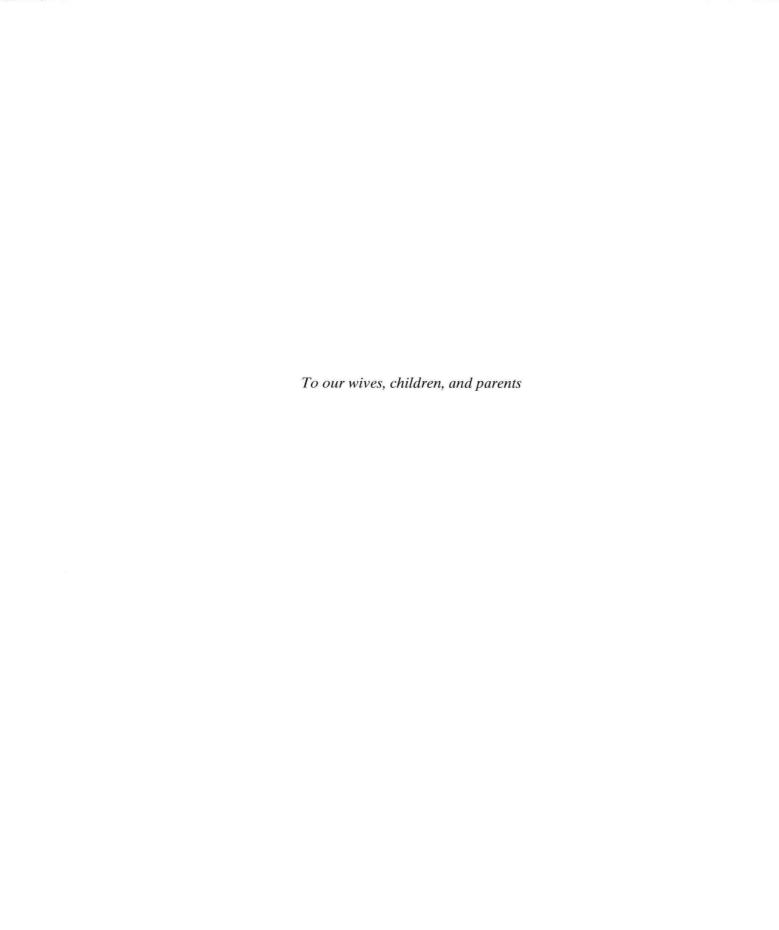
All rights reserved. This book is authorized for sale in Europe, Asia, Africa and the Middle East only and may not be exported outside of these territories. Exportation from or importation of this book to another region without the Publisher's authorization is illegal and is a violation of the Publisher's rights. The Publisher may take legal action to enforce its rights. The Publisher may recover damages and costs, including but not limited to lost profits and attorney's fees, in the event legal action is required.

No part of this publication may be reproduced, stored in a retrieval system, or transmitted in any form or by any means, electronic, mechanical, photocopying, recording, scanning, or otherwise, except as permitted under Section 107 or 108 of the 1976 United States Copyright Act, without either the prior written permission of the Publisher or authorization through payment of the appropriate per-copy fee to the Copyright Clearance Center, Inc., 222 Rosewood Drive, Danvers, MA 01923, website www.copyright.com. Requests to the Publisher for permission should be addressed to the Permissions Department, John Wiley & Sons, Inc., 111 River Street, Hoboken, NJ 07030, (201) 748-6011, fax (201) 748-6008, website http://www.wiley.com/go/permissions.

ISBN: 978-0-470-64610-6

Printed in Asia

10 9 8 7 6 5 4 3 2



About the Authors

Dale E. Seborg is a Professor and Vice Chair of the Department of Chemical Engineering at the University of California, Santa Barbara. He received his B.S. degree from the University of Wisconsin and his Ph.D. degree from Princeton University. Before joining UCSB, he taught at the University of Alberta for nine years. Dr. Seborg has published over 200 articles and co-edited three books on process control and related topics. He has received the American Statistical Association's Statistics in Chemistry Award, the American Automatic Control Council's Education Award, and the ASEE Meriam-Wiley Award. He was elected to the Process Automation Hall of Fame in 2008. Dr. Seborg has served on the Editorial Advisor Boards for control engineering journals and book series, and has been a co-organizer of several major conferences. He is an active industrial consultant who serves as an expert witness in legal proceedings.

Thomas F. Edgar holds the Abell Chair in chemical engineering at the University of Texas at Austin. He earned a B.S. degree in chemical engineering from the University of Kansas and a Ph.D. from Princeton University. Before receiving his doctorate, he was employed by Continental Oil Company. His professional honors include the AIChE Colburn and Lewis Awards, ASEE Meriam-Wiley and Chemical Engineering Division Awards, ISA Education Award, and AIChE Computing in Chemical Engineering Award. He is listed in Who's Who in America. He has published over 300 papers in the field of process control, optimization, and mathematical modeling of processes such as separations, combustion, and microelectronics processing. He is co-author of Optimization of Chemical Processes, published by McGraw-Hill in 2001. Dr. Edgar was president of AIChE in 1997 and President of the American Automatic Control Council in 1989-91.

Duncan A. Mellichamp is professor Emeritus and founding member of the faculty of the chemical engineering department at the University of California, Santa Barbara. He is editor of an early book on data acquisition and control computing and has published more than one hundred papers on process modeling, large scale/plantwide systems analysis, and computer control. He earned a B.S. degree from Georgia Tech and a Ph.D. from Purdue University with intermediate studies at the Technische Universität Stuttgart (Germany). He worked for four years with the Textile Fibers Department of the DuPont Company before joining UCSB. Dr. Mellichamp has headed several organizations, including the CACHE Corporation (1977), the UCSB Academic Senate (1990-92), and the University of California Systemwide Academic Senate (1995-97), where he served on the UC Board of Regents. He presently serves on the governing boards of several nonprofit organizations.

Francis J. Doyle III is the Associate Dean for Research in the College of Engineering at the University of California, Santa Barbara. He holds the Duncan and Suzanne Mellichamp Chair in Process Control in the Department of Chemical Engineering, as well as appointments in the Electrical Engineering Department, and the Biomolecular Science and Engineering Program. He received his B.S.E. from Princeton, C.P.G.S. from Cambridge, and Ph.D. from Caltech, all in Chemical Engineering. Prior to his appointment at UCSB, he has held faculty appointments at Purdue University and the University of Delaware, and held visiting positions at DuPont, Weyerhaeuser, and Stuttgart University. He is a Fellow of IEEE, IFAC, and AIMBE; he is also the recipient of multiple research awards (including the AIChE Computing in Chemical Engineering Award) as well as teaching awards (including the ASEE Ray Fahien Award).

Preface

Process control has become increasingly important in the process industries as a consequence of global competition, rapidly changing economic conditions, faster product development, and more stringent environmental and safety regulations. Process control and its allied fields of process modeling and optimization are critical in the development of more flexible and more complex processes for manufacturing high-value-added products. Furthermore, the rapidly declining cost of digital devices and increased computer speed (doubling every 18 months, according to Moore's Law) have enabled high-performance measurement and control systems to become an essential part of industrial plants.

It is clear that the scope and importance of process control technology will continue to expand during the 21st century. Consequently, chemical engineers need to master this subject in order to be able to design and operate modern plants. The concepts of dynamics, feedback, and stability are also important for understanding many complex systems of interest to chemical engineers, such as in bioengineering and advanced materials. An introductory course should provide an appropriate balance of process control theory and practice. In particular, the course should emphasize dynamic behavior, physical and empirical modeling, computer simulation, measurement and control technology, basic control concepts, and advanced control strategies. We have organized this book so that the instructor can cover the basic material while having the flexibility to include advanced topics. The textbook provides the basis for 10 to 30 weeks of instruction for a single course or a sequence of courses at either the undergraduate or first-year graduate levels. It is also suitable for self-study by engineers in industry. The book is divided into reasonably short chapters to make it more readable and modular. This organization allows some chapters to be omitted without a loss of continuity.

The mathematical level of the book is oriented toward a junior or senor student in chemical engineering who has taken at least one course in differential equations. Additional mathematical tools required for the analysis of control systems are introduced as needed. We emphasize process control techniques that are used in practice and provide detailed mathematical analysis only when it is essential for understanding the material. Key theoretical concepts are illustrated with numerous examples and simulations.

The textbook material has evolved at the University of California, Santa Barbara, and the University of Texas at Austin over the past 40 years. The first edition (SEM1) was published in 1989, adopted by over 80 universities worldwide, and translated into Korean and Japanese. In the second edition (SEM2, 2004), we added new chapters on the important topics of process monitoring (Chapter 21), batch process control (Chapter 22), and plantwide control (Chapters 23 and 24). Even with the new chapters, the length of the second edition was about the same as SEM1. Interactive computer software based on MATLAB® and Simulink® software was extensively used in examples and exercises. The second edition was translated into Chinese in 2004.

For the third edition (SEMD3), we are very pleased to have added a fourth co-author, Professor Frank Doyle (UCSB), and we have made major changes that reflect the evolving field of chemical and biological engineering, as well as the practice of process control, which are described in the following.

The book is divided into five parts. Part I provides an introduction to process control and an in-depth discussion of process modeling. Control system design and analysis increasingly rely on the availability of a process model. Consequently, the third edition includes additional material on process modeling based on first principles, such as conservation equations and thermodynamics. Exercises have been added to several chapters based on MATLAB® simulations of two physical models, a distillation column and a furnace. These simulations are based on the book, Process Control Modules, by Frank Doyle, Ed Gatzke, and Bob Parker. Both the book and the MATLAB simulations are available on the book Web site (www.wiley.com/go/global/seborg). National Instruments has provided multimedia modules for a number of examples in the book based on their LabVIEWTM software.

Part II (Chapters 3 through 7) is concerned with the analysis of the dynamic (unsteady-state) behavior of processes. We still rely on the use of Laplace transforms and transfer functions, to characterize the dynamic behavior of linear systems. However, we have kept analytical methods involving transforms at a minimum and prefer the use of computer simulation to determine dynamic responses. In addition, the important topics of empirical models and their development from plant data are presented.

Part III (Chapters 8 through 15) addresses the fundamental concepts of feedback and feedforward control. The topics include an overview of the process instrumentation (Chapter 9) and control hardware and software that are necessary to implement process control (Chapter 8 and Appendix A). Chapter 13 (new) presents the important topic of process control strategies at the unit level, and additional material on process safety has been added to Chapter 10. The design and analysis of feedback control systems still receive considerable attention, with emphasis on industry-proven methods for controller design, tuning, and troubleshooting. The frequency response approach for open and closed-loop processes is now combined into a single chapter (14), because of its declining use in the process industries. Part III concludes with a chapter on feedforward and ratio control.

Part IV (Chapters 16 through 22) is concerned with advanced process control techniques. The topics include digital control, multivariable control, and enhancements of PID control, such as cascade control, selective control, and gain scheduling. Up-to-date chapters on real-time optimization and model predictive control emphasize the significant impact these powerful techniques have had on industrial practice. Other chapters consider process monitoring and batch process control. The two plantwide control chapters that were introduced in SEM2 have been moved to the book Web site, as Appendices G and H. We have replaced this material with two new chapters on biosystems control, principally authored by our recently added fourth author, Frank Doyle. Part V (new Chapters 23 and 24) covers the application of process control in biotechnology and biomedical systems, and introduces basic ideas in systems biology.

The following resources for instructors (only) are provided: solutions manual, lecture slides, and figures from the text. Instructors need to visit the book Web site to register for a password to access the protected resources. The book Web site is located at www.wiley.com/go/global/seborg.

We gratefully acknowledge the very helpful suggestions and reviews provided by many colleagues in academia and industry: Joe Alford, Anand Asthagiri, Karl Aström, Tom Badgwell, Max Barolo, Larry Biegler, Don Bartusiak, Terry Blevins, Dominique Bonvin, Richard Braatz, Dave Camp, Jarrett Campbell, I-Lung Chien, Will Cluett, Oscar Crisalle, Patrick Daugherty, Bob Deshotels, Rainer Dittmar, Jim Downs, Ricardo Dunia, David Ender, Stacy Firth, Rudiyanto Gunawan, Juergen Hahn, Sandra Harris, Karlene Hoo, Biao Huang, Babu Joseph, Derrick Kozub, Jietae Lee, Bernt Lie, Cheng Ling, Sam Mannan, Tom McAvoy, Greg McMillan, Randy Miller, Samir Mitragotri, Manfred Morari, Duane Morningred, Kenneth Muske, Mark Nixon, Srinivas Palanki, Bob Parker, Michel Perrier, Mike Piovoso, Joe Qin, Larry Ricker, Dan Rivera, Derrick Rollins, Alan Schneider, Sirish Shah, Mikhail Skliar, Sigurd Skogestad, Tyler Soderstrom, Ron Sorensen, Dirk Thiele, John Tsing, Ernie Vogel, Doug White, Willy Wojsznis, Robert Young, and the late Cheng-Ching Yu.

We also gratefully acknowledge the many current and recent students and postdocs at UCSB and UT-Austin who have provided careful reviews and simulation results: Ivan Castillo, Marco Castellani, David Castineira, Dan Chen, Jeremy Cobbs, Jeremy Conner, Eyal Dassau, Doug French, Scott Harrison, John Hedengren, Xiaojiang Jiang, Ben Juricek, Fred Loquastro III, Doron Ronon, Lina Rueda, Ashish Singhal, Jeff Ward, Dan Weber, and Yang Zhang. Eyal Dassau was instrumental in converting the old PCM modules to the version posted to this book's Web site. We revised the solution manual, which was originally prepared for the first and second editions by Mukul Agarwal and David Castineira, with the help of Yang Zhang. We greatly appreciate their careful attention to detail. We commend Chris Bailor for her word processing skill during the numerous revisions for the third edition. We also acknowledge the patience of our editor, Jenny Welter, during the long revision process. Finally, we are deeply grateful for the support and patience of our long-suffering wives (Judy, Donna, Suzanne, and Diana) during the revisions of the book.

In the spirit of continuous improvement, we are interested in receiving feedback from students, faculty, and practitioners who use this book. We hope you find it to be useful.

Dale E. Seborg Thomas F. Edgar Duncan A. Mellichamp Francis J. Doyle III

Contents

PART ONE INTRODUCTION TO PROCESS CONTROL

1. Introduction to Process Control 1

- 1.1 Representative Process Control Problems 1
- 1.2 Illustrative Example—A Blending Process 3
- 1.3 Classification of Process Control Strategies 5
- 1.4 A More Complicated Example— A Distillation Column 7
- 1.5 The Hierarchy of Process Control Activities 8
- 1.6 An Overview of Control System Design 10

2. Theoretical Models of Chemical Processes 15

- 2.1 The Rationale for Dynamic Process Models 15
- 2.2 General Modeling Principles 17
- 2.3 Degrees of Freedom Analysis 21
- 2.4 Dynamic Models of Representative Processes 22
- 2.5 Process Dynamics and Mathematical Models 35

PART TWO DYNAMIC BEHAVIOR OF PROCESSES

3. Transfer Function Models 43

- 3.1 An Illustrative Example: A Continuous Blending System 43
- 3.2 Transfer Functions of Complicated Models 45
- 3.3 Properties of Transfer Functions 46
- 3.4 Linearization of Nonlinear Models 49

4. Dynamic Behavior of First-Order and Second-Order Processes 58

- 4.1 Standard Process Inputs 58
- 4.2 Response of First-Order Processes 61

- 4.3 Response of Integrating Processes 64
- 4.4 Response of Second-Order Processes 66

5. Dynamic Response Characteristics of More Complicated Processes 78

- 5.1 Poles and Zeros and Their Effect on Process Response 78
- 5.2 Processes with Time Delays 82
- 5.3 Approximation of Higher-Order Transfer Functions 86
- 5.4 Interacting and Noninteracting Processes 88
- 5.5 State-Space and Transfer Function Matrix Models 90
- 5.6 Multiple-Input, Multiple-Output (MIMO) Processes 93

6. Development of Empirical Models from Process Data 102

- 6.1 Model Development Using Linear or Nonlinear Regression 103
- 6.2 Fitting First- and Second-Order Models Using Step Tests 107
- 6.3 Neural Network Models 112
- 6.4 Development of Discrete-Time Dynamic Models 113
- 6.5 Identifying Discrete-Time Models from Experimental Data 115

PART THREE FEEDBACK AND FEEDFORWARD CONTROL

7. Feedback Controllers 124

- 7.1 Introduction 124
- 7.2 Basic Control Modes 126
- 7.3 Features of PID Controllers 131
- 7.4 On-Off Controllers 134
- 7.5 Typical Responses of Feedback Control Systems 134
- 7.6 Digital Versions of PID Controllers 135

8. Control System Instrumentation 141	13.3 Bode Diagrams 251
8.1 Sensors, Transmitters, and Transducers 1428.2 Final Control Elements 1478.3 Signal Transmission and Digital	 13.4 Frequency Response Characteristics of Feedback Controllers 255 13.5 Nyquist Diagrams 260 13.6 Bode Stability Criterion 260
Communication 153 8.4 Accuracy in Instrumentation 154	13.7 Gain and Phase Margins 264
9. Process Safety and Process Control 160	14. Feedforward and Ratio Control 271
 9.1 Layers of Protection 161 9.2 Alarm Management 165 9.3 Abnormal Event Detection 169 9.4 Risk Assessment 171 	 14.1 Introduction to Feedforward Control 271 14.2 Ratio Control 273 14.3 Feedforward Controller Design Based on Steady-State Models 275
10. Dynamic Behavior and Stability of Closed-Loop Control Systems 176	14.4 Feedforward Controller Design Based on Dynamic Models 27714.5 The Relationship Between the Steady-State
 10.1 Block Diagram Representation 176 10.2 Closed-Loop Transfer Functions 179 10.3 Closed-Loop Responses of Simple 	and Dynamic Design Methods 281 14.6 Configurations for Feedforward-Feedback Control 282 14.7 Tuning Feedforward Controllers 282
Control Systems 182 10.4 Stability of Closed-Loop Control Systems 188 10.5 Root Locus Diagrams 194	PART FOUR ADVANCED PROCESS CONTROL
11. PID Controller Design, Tuning, and Troubleshooting 204	15. Enhanced Single-Loop Control Strategies 288
 11.1 Performance Criteria for Closed-Loop Systems 204 11.2 Model-Based Design Methods 206 11.3 Controller Tuning Relations 211 11.4 Controllers with Two Degrees of Freedom 216 11.5 On-Line Controller Tuning 217 	 15.1 Cascade Control 288 15.2 Time-Delay Compensation 293 15.3 Inferential Control 296 15.4 Selective Control/Override Systems 297 15.5 Nonlinear Control Systems 300 15.6 Adaptive Control Systems 307
11.6 Guidelines for Common Control Loops 22311.7 Troubleshooting Control Loops 225	16. Multiloop and Multivariable Control 317 16.1 Process Interactions and Control Loop
12. Control Strategies at the Process Unit Level 232	Interactions 317 16.2 Pairing of Controlled and Manipulated
 12.1 Degrees of Freedom Analysis for Process Control 232 12.2 Selection of Controlled, Manipulated, and Measured Variables 234 	Variables 323 16.3 Singular Value Analysis 330 16.4 Tuning of Multiloop PID Control Systems 334
12.3 Applications 238	16.5 Decoupling and Multivariable Control
	Strategies 334
13. Frequency Response Analysis and Control System Design 248	Strategies 334 16.6 Strategies for Reducing Control Loop Interactions 336
	16.6 Strategies for Reducing Control Loop

 17.3 z-Transform Analysis for Digital Control 352 17.4 Tuning of Digital PID Controllers 358 17.5 Direct Synthesis for Design of Digital 	PART FIVE APPLICATIONS TO BIOLOGICAL SYSTEMS
Controllers 360	22. Biosystems Control Design 456
17.6 Minimum Variance Control 364 18. Batch Process Control 371 18.1 Potch Control Systems 373	 22.1 Process Modeling and Control in Pharmaceutical Operations 456 22.2 Process Modeling and Control for Drug Delivery 462
 18.1 Batch Control Systems 373 18.2 Sequential and Logic Control 374 18.3 Control During the Batch 380 18.4 Run-to-Run Control 386 18.5 Batch Production Management 387 	 23. Dynamics and Control of Biological Systems 470 24.1 Systems Biology 470 24.2 Gene Regulatory Control 472
Chapters 19 through 23 are online at www.wiley.com/go/global/seborg	24.3 Signal Transduction Networks 476 Appendix A: Laplace Transforms A-1
19. Real-Time Optimization 395	A.1 The Laplace Transform of Representative Functions A-1
 19.1 Basic Requirements in Real-Time Optimization 396 19.2 The Formulation and Solution of RTO Problems 399 19.3 Unconstrained and Constrained Optimization 401 	 A.2 Solution of Differential Equations by Laplace Transform Techniques A-5 A.3 Partial Fraction Expansion A-7 A.4 Other Laplace Transform Properties A-10 A.5 A Transient Response Example A-13
19.4 Linear Programming 40419.5 Quadratic and Nonlinear	Appendix B: Digital Process Control Systems: Hardware and Software A-21
Programming 408 20. Model Predictive Control 414	 B.1 Distributed Digital Control Systems A-22 B.2 Analog and Digital Signals and Data Transfer A-22
20.1 Overview of Model Predictive Control 414 20.2 Predictions for SISO Models 416 20.3 Predictions for MIMO Models 421 20.4 Model Predictive Control Calculations 423	 B.3 Microprocessors and Digital Hardware in Process Control A-24 B.4 Software Organization A-27 Appendix C: Review of Thermodynamic Concepts
20.5 Set-Point Calculations 42720.6 Selection of Design and Tuning Parameters 429	C.1 Single-Component Systems A-34
20.7 Implementation of MPC 434	C.2 Multicomponent Systems A-35 Appendix D: Control Simulation Software A-36
21. Process Monitoring 439	D.1 MATLAB Operations and Equation
 21.1 Traditional Monitoring Techniques 440 21.2 Quality Control Charts 441 21.3 Extensions of Statistical Process 	Solving A-36 D.2 Computer Simulation with Simulink A-38 D.3 Computer Simulation with LabVIEW A-40

21.3 Extensions of Statistical Process

21.5 Control Performance Monitoring 451

Control 447

21.4 Multivariate Statistical Techniques 449

Appendix E: Process Control Modules A-43

- E.1. Introduction A-43
- E.2. Module Organization A-43

E.3. Ha	rdware	and	Software	Requirements	A-44
---------	--------	-----	----------	--------------	------

- E.4. Installation A-44
- E.5. Running the Software A-44

Appendices F through K are online at www.wiley.com/go/global/seborg

Appendix F: Introduction to Plantwide Control A-45

- F.1 Plantwide Control Issues A-45
- F.2 Hypothetical Plant for Plantwide Control Studies A-47
- F.3 Internal Feedback of Material and Energy A-51
- F.4 Interaction of Plant Design and Control System Design A-59

Appendix G: Plantwide Control System Design A-63

- G.1 Procedures for the Design of Plantwide Control Systems A-63
- G.2 A Systematic Procedure for Plantwide Control System Design A-64
- G.3 Case Study: The Reactor/Flash Unit Plant A-67
- G.4 Effect of Control Structure on Closed-Loop Performance A-78

Appendix H: Dynamic Models and Parameters Used for Plantwide Control Chapters A-82

- H.1 Energy Balance and Parameters for the Reactor/Distillation Column Model A-82
- H.2 Core Reactor/Flash Unit Model and Parameters A-82

Appendix I: Instrumentation Symbols A-88

Appendix J: Review of Basic Concepts from Probability and Statistics A-90

- J.1 Probability Concepts A-90
- J.2 Means and Variances A-91
- J.3 Standard Normal Distribution A-91
- J.4 Error Analysis A-92

Appendix K: Contour Mapping and the Principle of the Argument A-93

K.1 Development of the Nyquist Stability Criterion A-93

Index I-1

Introduction to Process Control

In recent years the performance requirements for process plants have become increasingly difficult to satisfy. Stronger competition, tougher environmental and safety regulations, and rapidly changing economic conditions have been key factors in tightening product quality specifications. A further complication is that modern plants have become more difficult to operate because of the trend toward complex and highly integrated processes. For such plants, it is difficult to prevent disturbances from propagating from one unit to other interconnected units.

In view of the increased emphasis placed on safe, efficient plant operation, it is only natural that the subject of *process control* has become increasingly important in recent years. Without computer-based process control systems it would be impossible to operate modern plants safely and profitably while satisfying product quality and environmental requirements. Thus, it is important for chemical engineers to have an understanding of both the theory and practice of process control.

The two main subjects of this book are process dynamics and process control. The term process dynamics refers to unsteady-state (or transient) process behavior. By contrast, most of the chemical engineering curricula emphasize steady-state and equilibrium conditions in such courses as material and energy balances, thermodynamics, and transport phenomena. But process dynamics are also very important. Transient operation occurs during important situations such as start-ups and shutdowns, unusual process disturbances, and planned transitions from one product grade to another. Consequently, the first part of this book is concerned with process dynamics.

The primary objective of process control is to maintain a process at the desired operating conditions, safely and efficiently, while satisfying environmental and product quality requirements. The subject of process control is concerned with how to achieve these goals. In large-scale, integrated processing plants such as oil refineries or ethylene plants, thousands of process variables such as compositions, temperatures, and pressures are measured and must be controlled. Fortunately, large numbers of process variables (mainly flow rates) can usually be manipulated for this purpose. Feedback control systems compare measurements with their desired values and then adjust the manipulated variables accordingly.

As an introduction to the subject, we consider representative process control problems in several industries.

1.1 REPRESENTATIVE PROCESS CONTROL PROBLEMS

The foundation of process control is *process under-standing*. Thus, we begin this section with a basic question: what is a process? For our purposes, a brief definition is appropriate:

Process: The conversion of feed materials to products using chemical and physical operations. In practice, the term process tends to be used for both the processing operation and the processing equipment.

Note that this definition applies to three types of common processes: continuous, batch, and semi-batch. Next, we consider representative processes and briefly summarize key control issues.

1.1.1 Continuous Processes

Four continuous processes are shown schematically in Figure 1.1:

(a) *Tubular heat exchanger*. A process fluid on the tube side is cooled by cooling water on the shell side. Typically, the exit temperature of the process fluid is controlled by manipulating

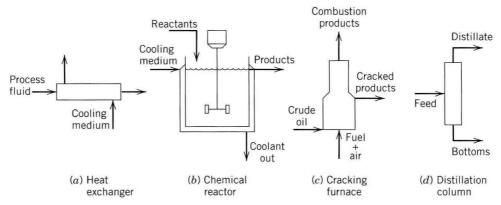


Figure 1.1 Some typical continuous processes.

the cooling water flow rate. Variations in the inlet temperatures and the process fluid flow rate affect the heat exchanger operation. Consequently, these variables are considered to be disturbance variables.

- (b) Continuous stirred-tank reactor (CSTR). If the reaction is highly exothermic, it is necessary to control the reactor temperature by manipulating the flow rate of coolant in a jacket or cooling coil. The feed conditions (composition, flow rate, and temperature) can be manipulated variables or disturbance variables.
- (c) Thermal cracking furnace. Crude oil is broken down ("cracked") into a number of lighter petroleum fractions by the heat transferred from a burning fuel/air mixture. The furnace temperature and amount of excess air in the flue gas can be controlled by manipulating the fuel flow rate and the fuel/air ratio. The crude oil composition and the heating quality of the fuel are common disturbance variables.
- (d) Multicomponent distillation column. Many different control objectives can be formulated for distillation columns. For example, the distillate composition can be controlled by adjusting the reflux flow rate or the distillate flow rate. If the composition cannot be measured on-line, a tray temperature near the top of the column can be controlled instead. If the feed stream is supplied by an upstream process, the feed conditions will be disturbance variables.

For each of these four examples, the process control problem has been characterized by identifying three important types of process variables.

- Controlled variables (CVs): The process variables that are controlled. The desired value of a controlled variable is referred to as its set point.
- Manipulated variables (MVs): The process variables that can be adjusted in order to keep the controlled variables at or near their set points. Typically, the manipulated variables are flow rates.
- Disturbance variables (DVs): Process variables that affect the controlled variables but cannot be manipulated. Disturbances generally are related to changes in the operating environment of the process: for example, its feed conditions or ambient temperature. Some disturbance variables can be measured on-line, but many cannot such as the crude oil composition for Process (c), a thermal cracking furnace.

The specification of CVs, MVs, and DVs is a critical step in developing a control system. The selections should be based on process knowledge, experience, and control objectives.

Batch and Semi-Batch Processes

Batch and semi-batch processes are used in many process industries, including microelectronics, pharmaceuticals, specialty chemicals, and fermentation. Batch and semi-batch processes provide needed flexibility for multiproduct plants, especially when products change frequently and production quantities are small. Figure 1.2 shows four representative batch and semi-batch processes:

(e) Batch or semi-batch reactor. An initial charge of reactants is brought up to reaction conditions,

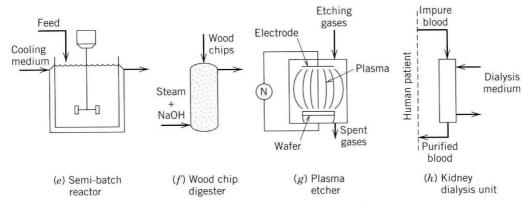


Figure 1.2 Some typical processes whose operation is noncontinuous.

and the reactions are allowed to proceed for a specified period of time or until a specified conversion is obtained. Batch and semi-batch reactors are used routinely in specialty chemical plants, polymerization plants (where a reaction byproduct typically is removed during the reaction), and in pharmaceutical and other bioprocessing facilities (where a feed stream, e.g., glucose, is fed into the reactor during a portion of the cycle to feed a living organism, such as a yeast or protein). Typically, the reactor temperature is controlled by manipulating a coolant flow rate. The end-point (final) concentration of the batch can be controlled by adjusting the desired temperature, the flow of reactants (for semi-batch operation), or the cycle time.

- (f) Batch digester in a pulp mill. Both continuous and semi-batch digesters are used in paper manufacturing to break down wood chips in order to extract the cellulosic fibers. The end point of the chemical reaction is indicated by the kappa number, a measure of lignin content. It is controlled to a desired value by adjusting the digester temperature, pressure, and/or cycle time.
- (g) Plasma etcher in semiconductor processing. A single wafer containing hundreds of printed circuits is subjected to a mixture of etching gases under conditions suitable to establish and maintain a plasma (a high voltage applied at high temperature and extremely low pressure). The unwanted material on a layer of a microelectronics circuit is selectively removed by chemical reactions. The temperature, pressure, and flow rates of etching gases to the reactor are con-

trolled by adjusting electrical heaters and control valves.

(h) Kidney dialysis unit. This medical equipment is used to remove waste products from the blood of human patients whose own kidneys are failing or have failed. The blood flow rate is maintained by a pump, and "ambient conditions," such as temperature in the unit, are controlled by adjusting a flow rate. The dialysis is continued long enough to reduce waste concentrations to acceptable levels.

Next, we consider an illustrative example in more detail.

ILLUSTRATIVE EXAMPLE-A 1.2 **BLENDING PROCESS**

A simple blending process is used to introduce some important issues in control system design. Blending operations are commonly used in many industries to ensure that final products meet customer specifications.

A continuous, stirred-tank blending system is shown in Fig. 1.3. The control objective is to blend the two inlet streams to produce an outlet stream that has the desired composition. Stream 1 is a mixture of two chemical species, A and B. We assume that its mass flow rate w_1 is constant, but the mass fraction of A, x_1 , varies with time. Stream 2 consists of pure A and thus $x_2 = 1$. The mass flow rate of Stream 2, w_2 , can be manipulated using a control valve. The mass fraction of A in the exit stream is denoted by x and the desired value (set point) by x_{sp} . Thus for this control problem, the controlled variable is x, the manipulated variable is w_2 , and the disturbance variable is x_1 .

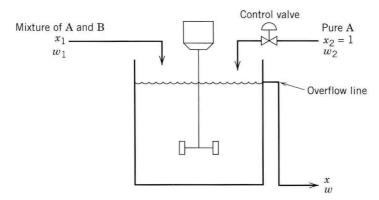


Figure 1.3 Stirred-tank blending system.

Next we consider two questions.

Design Question. If the nominal value of x_1 is \overline{x}_1 , what nominal flow rate \overline{w}_2 is required to produce the desired outlet concentration, x_{sp} ?

To answer this question, we consider the steady-state material balances:

Overall balance:

$$0 = \overline{w}_1 + \overline{w}_2 - \overline{w} \tag{1-1}$$

Component A balance:

$$0 = \overline{w}_1 \overline{x}_1 + \overline{w}_2 \overline{x}_2 - \overline{w} \overline{x} \tag{1-2}$$

The overbar over a symbol denotes its nominal steadystate value, for example, the value used in the process design. According to the process description, $\bar{x}_2 = 1$ and $\bar{x} = x_{sp}$. Solving Eq. 1-1 for \bar{w} , substituting these values into Eq. 1-2, and rearranging gives:

$$\overline{w}_2 = \overline{w}_1 \frac{x_{sp} - \overline{x}_1}{1 - x_{sp}} \tag{1-3}$$

Equation 1-3 is the design equation for the blending system. If our assumptions are correct and if $x_1 = \overline{x}_1$, then this value of w_2 will produce the desired result, $x = x_{sp}$. But what happens if conditions change?

Control Question. Suppose that inlet concentration x_1 varies with time. How can we ensure that the outlet composition x remains at or near its desired value, x_{sp} ?

As a specific example, assume that x_1 increases to a constant value that is larger than its nominal value, \bar{x}_1 . It is clear that the outlet composition will also increase

due to the increase in inlet composition. Consequently, at this new steady state, $x > x_{sp}$.

Next we consider several strategies for reducing the effects of x_1 disturbances on x.

Method 1. Measure x and adjust w_2 . It is reasonable to measure controlled variable x and then adjust w_2 accordingly. For example, if x is too high, w_2 should be reduced; if x is too low, w_2 should be increased. This control strategy could be implemented by a person (manual control). However, it would normally be more convenient and economical to automate this simple task (automatic control).

Method 1 can be implemented as a simple control algorithm (or control law),

$$w_2(t) = \overline{w}_2 + K_c[x_{sp} - x(t)]$$
 (1-4)

where K_c is a constant called the *controller gain*. The symbols, $w_2(t)$ and x(t), indicate that w_2 and x change with time. Equation 1-4 is an example of *proportional control*, because the change in the flow rate, $w_2(t) - \overline{w}_2$, is proportional to the deviation from the set point, $x_{sp} - x(t)$. Consequently, a large deviation from set point produces a large corrective action, while a small deviation results in a small corrective action. Note that we require K_c to be positive because w_2 must increase when x decreases, and vice versa. However, in other control applications, negative values of K_c are appropriate, as discussed in Chapter 7.

A schematic diagram of Method 1 is shown in Fig. 1.4. The outlet concentration is measured and transmitted to the controller as an electrical signal. (Electrical signals are shown as dashed lines in Fig. 1.4.) The controller executes the control law and sends the calculated value of w_2 to the control valve as an electrical signal. The control

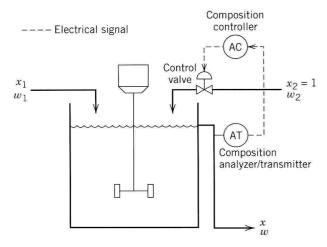


Figure 1.4 Blending system and Control Method 1.

valve opens or closes accordingly. In Chapters 7 and 8 we consider process instrumentation and control hardware in more detail.

Method 2. Measure x_1 , adjust w_2 . As an alternative to Method 1, we could measure disturbance variable x_1 and adjust w_2 accordingly. Thus, if $x_1 > \overline{x}_1$, we would decrease w_2 so that $w_2 < \overline{w}_2$. If $x_1 < \overline{x}_1$, we would increase w_2 . A control law based on Method 2 can be derived from Eq. 1-3 by replacing \overline{x}_1 with $x_1(t)$ and \overline{w}_2 with $w_2(t)$:

$$w_2(t) = \overline{w}_1 \frac{x_{sp} - x_1(t)}{1 - x_{sp}}$$
 (1-5)

The schematic diagram for Method 2 is shown in Fig. 1.5. Because Eq. 1-3 is valid only for steady-state condi-

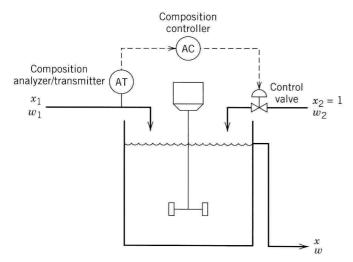


Figure 1.5 Blending system and Control Method 2.

tions, it is not clear just how effective Method 2 will be during the transient conditions that occur after an x_1 disturbance.

Method 3. Measure x_1 and x, adjust w_2 . This approach is a combination of Methods 1 and 2.

Method 4. Use a larger tank. If a larger tank is used, fluctuations in x_1 will tend to be damped out as a result of the larger volume of liquid. However, increasing tank size is an expensive solution due to the increased capital cost.

1.3 **CLASSIFICATION OF PROCESS CONTROL STRATEGIES**

Next, we will classify the four blending control strategies of the previous section and discuss their relative advantages and disadvantages. Method 1 is an example of a feedback control strategy. The distinguishing feature of feedback control is that the controlled variable is measured, and that the measurement is used to adjust the manipulated variable. For feedback control, the disturbance variable is *not* measured.

It is important to make a distinction between *negative* feedback and positive feedback. In the engineering literature, negative feedback refers to the desirable situation in which the corrective action taken by the controller forces the controlled variable toward the set point. On the other hand, when positive feedback occurs, the controller makes things worse by forcing the controlled variable farther away from the set point. For example, in the blending control problem, positive feedback takes place if $K_c < 0$, because w_2 will increase when x increases. Clearly, it is of paramount importance to ensure that a feedback control system incorporates negative feedback rather than positive feedback.

An important advantage of feedback control is that corrective action occurs regardless of the source of the disturbance. For example, in the blending process, the feedback control law in (1-4) can accommodate disturbances in w_1 , as well as x_1 . Its ability to handle disturbances of unknown origin is a major reason why feedback control is the dominant process control strategy. Another important advantage is that feedback control reduces the sensitivity of the controlled variable to

¹Note that social scientists use the terms negative feedback and positive feedback in a very different way. For example, they would say that teachers provide "positive feedback" when they compliment students who correctly do assignments. Criticism of a poor performance would be an example of "negative feedback."

unmeasured disturbances and process changes. However, feedback control does have a fundamental limitation: no corrective action is taken until after the disturbance has upset the process, that is, until after the controlled variable deviates from the set point. This shortcoming is evident from the control law of (1-4).

Method 2 is an example of a *feedforward control strategy*. The distinguishing feature of feedforward control is that the disturbance variable is measured, but the controlled variable is not. The important advantage of feedforward control is that corrective action is taken *before* the controlled variable deviates from the set point. Ideally, the corrective action will cancel the effects of the disturbance so that the controlled variable is not affected by the disturbance. Although ideal cancelation is generally not possible, feedforward control can significantly reduce the effects of measured disturbances, as discussed in Chapter 14.

Feedforward control has three significant disadvantages: (i) the disturbance variable must be measured (or accurately estimated), (ii) no corrective action is taken for unmeasured disturbances, and (iii) a process model is required. For example, the feedforward control strategy for the blending system (Method 2) does not take any corrective action for unmeasured w_1 disturbances. In principle, we could deal with this situation by measuring both x_1 and w_1 and then adjusting w_2 accordingly. However, in industrial applications it is generally uneconomical to attempt to measure all potential disturbances. A more practical approach is to use a combined feedforward–feedback control system, in which feedback control provides corrective action for unmeasured disturbances, while feedforward control reacts to elimi-

Table 1.1 Concentration Control Strategies for the Blending System

Method	Measured Variable	Manipulated Variable	Category
1	X	w_2	FB
2	x_1	w_2	FF
3	x_1 and x	w_2	FF/FB
4	_		Design change

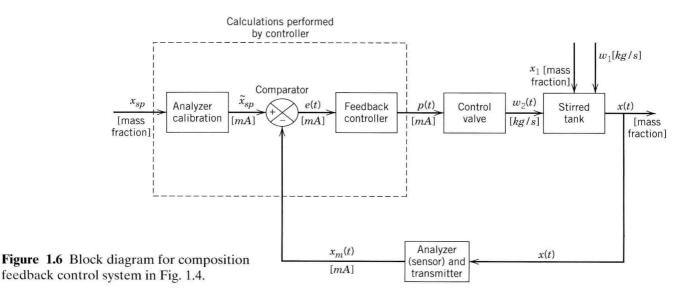
FB = feedback control; FF = feedforward control; FF/FB = feedforward control and feedback control.

nate measured disturbances before the controlled variable is upset. Consequently, in industrial applications feedforward control is normally used in combination with feedback control. This approach is illustrated by Method 3, a combined feedforward-feedback control strategy because both x and x_1 are measured.

Finally, Method 4 consists of a process design change and thus is not really a control strategy. The four strategies for the stirred-tank blending system are summarized in Table 1.1.

1.3.1 Process Control Diagrams

Next we consider the equipment that is used to implement control strategies. For the stirred-tank mixing system under feedback control in Fig. 1.4, the exit concentration x is controlled and the flow rate w_2 of pure species A is adjusted using proportional control. To consider how this feedback control strategy could be implemented, a block diagram for the stirred-tank control system is shown in Fig. 1.6. Operation of the



此为试读,需要完整PDF请访问: www.ertongbook.com