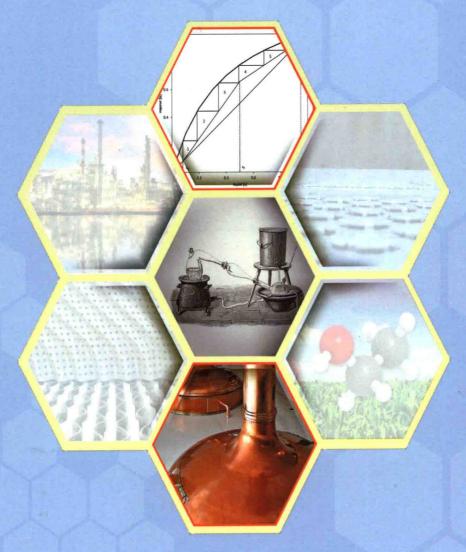
# DISTILLATION

FUNDAMENTALS AND PRINCIPLES



Andrzej Górak and Eva Sorensen

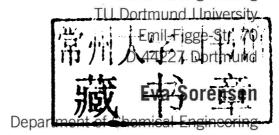


# Distillation: Fundamentals and Principles

Edited by

### Andrzej Górak

Laboratory of Fluid Separations
Department of Biochemical and
Chemical Engineering



UCL, Torrington Place, UK-London WC1E 7JE





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# Distillation: Fundamentals and Principles

# Preface to the Distillation Collection

For more than 5,000 years distillation has been used as a method for separating binary and multicomponent liquid mixtures into pure components. Even today, it belongs to the most commonly applied separation technologies and is used at such a large scale worldwide that it is responsible for up to 50% of both capital and operating costs in industrial processes. It moreover absorbs about 50% of the total process energy used by the chemical and petroleum refining industries every year. Given that the chemical industry consumed 19% of the entire energy in Europe (2009), distillation is *the* big driver of overall energy consumption.

Although distillation is considered the most mature and best-understood separation technology, knowledge on its manifold aspects is distributed unevenly among different textbooks and manuals. Engineers, by contrast, often wish for just one reference book in which the most relevant information is presented in a condensed and accessible form. *Distillation* aims at filling this gap by offering a succinct overview of distillation fundamentals, equipment, and applications. Students, academics, and practitioners will find in *Distillation* a helpful summary of pertinent methods and techniques and will thus be able to quickly resolve any problems in the field of distillation.

This book provides a comprehensive and thorough introduction into all aspects of distillation, covering distillation history, fundamentals of thermodynamics, hydrodynamics, mass transfer, energy considerations, conceptual process design, modeling, optimization and control, different column internals, special cases of distillation, troubleshooting, and the most important applications in various industrial branches, including biotechnological processes.

Distillation forms part of the "Handbook of Separation Sciences" series and is available as a paper book and as an e-book, thus catering to the diverging needs of different readers. It is divided into three volumes: "Fundamentals and Principles" (Editors A. Górak and E. Sorensen), "Equipment and processes" (Editors A. Górak and Ž. Olujić), and "Operation and applications" (Editors A. Górak and H. Schoenmakers). Each volume contains chapters written by individual authors with acclaimed expertise in their fields. In addition to that, readers will find cross-references to other chapters, which allow them to gain an extensive overview of state-of-the-art technologies and various research perspectives. Helpful suggestions for further reading conclude each chapter.

A comprehensive and complex publication such as *Distillation* is impossible to complete without the support of an entire team whose enduring help I wish to acknowledge. In particular, I wish to express my heartfelt gratitude to the 42 leading world experts from the academia and industry who contributed to the chapters of this book. I thank the co-editors of the three volumes of *Distillation*—Dr Eva Sorensen,

UCL, Dr Žarko Olujić, Delft University of Technology, and Dr Hartmut Schoenmakers, former member of BASF SE, Ludwigshafen—for their knowledgeable input and expertise, unremitting patience, and continuous encouragement. The invaluable editorial assistance of Dipl.-Ing. Johannes Holtbrügge during the entire editorial process is also greatly acknowledged.

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**Dr Andrzej Górak** TU Dortmund University

# Preface to *Distillation: Fundamentals* and *Principles*

This is the first book in a three-volume series covering all aspects of *Distillation*. This volume focuses on the fundamental principles of distillation with particular emphasis on practical understanding of design and operation. The chapters are written by different authors and the approach, depth, and extent of subject matter coverage may therefore differ from chapter to chapter, however, together they represent a comprehensive overview of the current state of the art.

The first chapter traces the historical development of distillation from the first applications over 5000 years ago, via the medieval period, and the nineteenth-century industrial developments, to contemporary applications with emphasis on the applications and equipment which led to our current technology. A prerequisite for the design of distillation columns is knowledge of vapor—liquid equilibrium (VLE) and of mass transfer phenomena. Chapter 2 considers thermodynamic models for the prediction of VLEs, and the conditions for the occurrence of azeotropes. In Chapter 3, an account is given of the fundamental principles of mass transfer including diffusion, mass transfer coefficients, and mass transfer of both binary and multicomponent mixtures in both tray and packed columns.

Chapter 4 sets out the fundamental principles of binary distillation including simple calculation and analysis methods. This is followed by an account of batch distillation in Chapter 5, giving an overview of the fundamentals of batch distillation, including different operating modes, alternative column configurations and more complex batch distillation processes. Chapter 6 considers energy-efficient distillation design and operation, including columns operating both above and below ambient temperatures. Various advanced and complex distillation column configurations are also introduced.

Chapters 7 and 8 consider design of distillation processes. Chapter 7 describes the conceptual design of zeotropic multicolumn distillation configurations. A computationally efficient mathematical framework is described that synthesizes configurations that use n-1 distillation columns for separating a zeotropic mixture into n product streams. Chapter 8 turns the attention to azeotropic systems and describes a systematic framework for their conceptual design, considering and comparing different approaches. Several shortcut methods are presented, followed by an account of rigorous optimization, and their applicability for design is discussed.

Aspects of design, analysis, and application of hybrid distillation schemes are covered in Chapter 9. These hybrid distillation schemes become necessary when separation tasks such as separation of azeotropic or close-boiling mixtures cannot

#### Preface to Distillation: Fundamentals and Principles

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be achieved in a single conventional distillation column. Chapter 10 presents an overview of modeling methods covering both simplified and rigorous models. Conceptual features are highlighted and basic equations are shown for both equilibrium- and nonequilibrium-based approaches. In addition to classical distillation, modeling of related and more complex processes is also discussed. Finally, Chapter 11 presents an overview of the main advances in optimization of zeotropic systems, ranging from systems using only conventional columns, to fully thermally coupled systems, with main focus on mathematical programming approaches for design.

I would like to thank all the authors for their contributions and assiduous efforts in making this the most comprehensive account of distillation fundamentals available to date.

Dr Eva Sorensen UCL

# List of Contributors

Rakesh Agrawal

School of Chemical Engineering, Purdue University, West Lafayette, IN, USA

Deenesh K. Babi

Department of Chemical and Biochemical Engineering, Technical University of Denmark, Lyngby, Denmark

Sergei Blagov

BASF SE, GT/SI, Ludwigshafen, Germany

José A. Caballero

Department of Chemical Engineering, University of Alicante, Alicante, Spain

Rafiqul Gani

Department of Chemical and Biochemical Engineering, Technical University of Denmark, Lyngby, Denmark

Jürgen Gmehling

University of Oldenburg, Industrial Chemistry, Oldenburg, Germany

Ignacio E. Grossmann

Department of Chemical Engineering, Carnegie Mellon University, Pittsburgh, PA. USA

Andreas Harwardt

AVT-Process Systems Engineering, RWTH Aachen University, Aachen, Germany

Megan Jobson

School of Chemical Engineering and Analytical Science, The University of Manchester, Manchester, UK

Eugeny Y. Kenig

Department of Mechanical Engineering, University of Paderborn, Pohlweg 55, Paderborn, Germany

Michael Kleiber

Hattersheim, Germany

Norbert Kockmann

Laboratory of Equipment Design, Department of Biochemical and Chemical Engineering, TU Dortmund University, Dortmund, Germany

Hendrik A. Kooijman

Clarkson University; Potsdam, NY, USA

**Wolfgang Marquardt** 

AVT-Process Systems Engineering, RWTH Aachen University, Aachen, Germany

Vishesh H. Shah

Engineering and Process Sciences Laboratory, The Dow Chemical Company, Midland. MI. USA

#### xii List of Contributors

#### Mirko Skiborowski

AVT-Process Systems Engineering, RWTH Aachen University, Aachen, Germany

#### Eva Sorensen

Department of Chemical Engineering, UCL, London, UK

#### **Ross Taylor**

Clarkson University; Potsdam, NY, USA

# List of Symbols and Abbreviations

## Latin symbols

Symbol	Explanation	Unit	Chapter
A	Matrix of constant coefficients		11
A <sub>AB</sub>	Coefficient in van Laar's equation	-	4
40	column cross section area	$m^2$	10
Ą <sub>e</sub>	Effective adsorption factor (Group methods)	-	11
A <sub>ht</sub>	Heat transfer area	m <sup>2</sup>	6
$\Delta_{i}$	Coefficient in Antoine's equation for component i	Pa, bar	4
$A_z$	Azeotropic composition	mol/mol	5
a	Attractive parameter in cubic equations of state	Jm <sup>3</sup> /mol <sup>2</sup>	2
a <sup>l</sup>	specific vapor-liquid interfacial area	$m^2/m^3$	10
$a_i$	Activity of component i	=	2
В	Bottom stream flow rate	kmol/s, kg/s	4, 11
3	Matrix of coefficients		11
Bi	Coefficient in Antoine's equation for component i	Pa K, bar °C, Pa °C,	4
BT	Total molar bottom stream flow rate	kmol/s	11
b	Co-volume in cubic equations of state	cm <sup>3</sup> /mol, m <sup>3</sup> /mol	2
b	Content dependent Binary variable Vector of constant coefficients		11
CA	Price of distillate product	\$, €	5
C <sub>C</sub>	Unit costs for cooling in the condenser	\$/kW	11
C <sub>F</sub>	Price of feed	\$, €	5
$C_{fix,k}$	Annualized fixed charge cost of column k	\$/a	11
Сн	Unit costs for heating in the reboiler	\$/kW	11
Ci	Coefficient in Antoine's equation for component i	K, °C	4
$C_k$	Annualized cost of column k	\$/a	11

(continued)

Symbol	Explanation	Unit	Chapter
С	Parameter in the VTPR equation of	m <sup>3</sup> /mol	2
	state		
С	Constant/vector of constant		11
_	coefficients	mol/m <sup>3</sup>	10
C	molar concentration		10
Ср	Molar heat capacity at constant pressure	J/(mol K)	2
C <sub>pL</sub>	Liquid heat capacity at constant pressure	J/K	4
C <sub>pLi</sub>	Liquid heat capacity of component i at constant pressure	J/K	4
$C_{pV}$	Vapor heat capacity at constant pressure	J/K	4
d	generalized driving force, Eq. (10-30)	1/m	10
D	Distillate flow rate	mol/s, kmol/s, kg/s	4, 5, 8, 10, 1
$D_{AB}$	binary diffusion coefficient	m <sup>2</sup> /s	10
$D_{ax}$	axial dispersion coefficient	m <sup>2</sup> /s	10
$D_i$	effective diffusion coefficient of component <i>i</i>	m <sup>2</sup> /s	10
Dij	Driving Force		9
Đ <sub>ij</sub>	Maxwell-Stefan diffusion coefficient	m <sup>2</sup> /s	10
DT	Total molar distillate flow rate	kmol/s	11
E	Entrainer flow rate	kmol/s	5, 8
E <sub>MV</sub>	Murphree vapor efficiency	=	4
Eo	Overall tray/stage efficiency	_	4
E <sub>OL</sub>	Murphree efficiency for the liquid	_	10
LOL	phase	_ ,	10
$E_{OV}$	Murphree efficiency for the vapor phase	_	10
Ex	Exergy	W, W/K	6
F	Feed flow rate	mol/s, kmol/s, kg/s	4, 5, 8, 10,
FT	Total molar feed flow rate	kmol/s	11
f	Vaporized fraction of the feed	_	4
f(·)	Scalar function		11
121	Fugacity of component i	Pa	2
f <sub>i</sub>		ı a	2, 5
f <sub>obj</sub> (⋅) G <sup>E</sup>	Objective function	. î	
	Total excess Gibbs energy	J	2, 8
G <sub>ij</sub>	NRTL parameter		2
$g(\cdot)$	Equality constraints Scalar/vector functions		5 11
aE		I/mol	
g <sup>E</sup>	Molar excess Gibbs energy	J/mol	2
Δg <sub>ij</sub>	Interaction parameter between component i and j	K	2

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Symbol	Explanation	Unit	Chapter
Н	Enthalpy	W, W/K	6
h	partial molar enthalpy	J/mol	10
$H_A$	Amount of distillate	mole	5
H <sub>F</sub>	Amount of feed	mole	5
$H_{i,j}$	Henry constant of component i in j	Pa	2
$\Delta H_{vap}$	Molar heat of vaporization	J/mol	4
h	Specific enthalpy	J/kg, J/mol	4, 8, 11
h(∙)	Inequality constraints Scalar/vector functions		5 11
Δhv	Enthalpy of vaporization	J/mol	2
h <sup>E</sup>	Molar excess enthalpy	J/mol	2
HETP	height equivalent to a theoretical plate	m	10
HTU	height of a transfer unit	m	10
$H_c$	column height	m	10
J	diffusion flux	mol/(m <sup>2</sup> s)	10
J	column vector consisting of $J_i$	mol/(m <sup>2</sup> s)	10
Ki	Chemical equilibrium constant of component i	-	2
K <sub>i</sub>	Distribution coefficient/K-factor of component i	_ ,	2, 4, 8, 11
K <sub>k</sub>	Relation between feed and heat flow (Andrecovich & Westerberg model)	-	11
k <sub>ij</sub>	Binary parameter in cubic equations of state	-	2
Keq	vapor-liquid equilibrium constant	_	10
K <sub>OL</sub>	overal mass transfer coefficient in terms of the liquid phase	mol/(m <sup>2</sup> s)	10
K <sub>OV</sub>	overal mass transfer coefficient in terms of the vapor phase	mol/(m <sup>2</sup> s)	10
L	Liquid flow rate	kmol/s, kg/s	4, 8, 11
Ld	Reflux flow rate returned to the column	kmol/s	11
L <sub>R</sub>	Liquid flow rate in a rectifying column section	kmol/s	11
L <sub>S</sub>	Liquid flow rate in a stripping column section	kmol/s	11
1	axial coordinate directed from column top to bottom	m	10
L	liquid molar flow rate	mol/s	10
M	Scalar (Big M parameter)		11
m	slope of the operating line, Eq. (10-A2)	<u></u>	10

-cont'd

Symbol	Explanation	Unit	Chapter
N	Content dependent Number of trays/stages Number of components	-	4, 6, 8, 11
$N_R$	Number of trays/stages in the rectifying section	=	4, 8, 11
$N_S$	Number of trays/stages in the stripping section	-	4, 8, 11
VT	Total number of trays in column section	-	4
NF	Feed tray location	mole	4
1	Number of moles		2
nc	Number of components	=	8
7	number of mixture components	=	10
V	Content dependent molar flux	mol/(m <sup>2</sup> s)	10
NTU	number of transfer units	_	10
$O_i$	Offcuts	_	5
0	Hourly profitability	profit/hr	5
<b>D</b>	Product cuts	_	5
<sup>D</sup> oy <sub>i</sub>	Poynting factor of component i		2
0	Pressure	Pa (or bar, atm)	2, 4, 8, 11
$O_{0,i}^{LV}$	Vapor pressure of component i	Pa	4
ob <sub>i</sub>	Individual flow rate of the bottom product	kmol/s, kg/s	11
O <sub>i</sub>	Partial pressure of component i	Pa (or bar, atm)	4
oti	Individual flow rate of the top product	kmol/s, kg/s	11
$Q_{EX}$	Exchanged heat	kJ	11
Ż	Duty	W	4, 5, 6, 8, 1
Q <sub>flash</sub>	Energy added or removed in the flash drum	W	4
Q <sub>ht</sub>	Heat transfer duty	W	6
Q <sub>hx</sub>	Energy added or removed in the heat exchanger	W	4
Q <sub>k</sub>	Heat duty for column k	W	11
Q <sub>B</sub> /Q <sub>R</sub>	reboiler/boilup heat duty	_	8
7	Energy to convert one mol of feed to saturated vapor at dew point divided by the molar heat of vaporization	-	4
ALS	Liquid fraction of a stream	mol/mol	11
7	liquid molar fraction in the feed stream	-	10
2	heat flux	W/m <sup>2</sup>	10
3	Gas constant	J/mol·K	2

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Symbol	Explanation	Unit	Chapter
R	Boolean variable		11
$R_{min}$	Reflux ratio	_	4, 5, 6, 8, 1
r	Content dependent Binary variable Interest rate Scalar function		11
rec	Component recovery		11
R	gas constant	8.3144 J/(mol K)	10
$R_b$	reboil ratio	-	10
$R_f$	reflux ratio	-	10
S	Stripping factor	_	11
S	Entropy	W, W/K	6
S	Side stream flow rate	kmol/s, kg/s	4
Se	Effective stripping factor (Group methods)	_	11
S <sub>ij</sub>	Selectivity	_	2, 8
S	Renewal frequency, parameter of the surface renewal model	1/s	10
T	Absolute temperature	K	2, 4, 6, 8, 1
T <sub>bp</sub>	Boiling temperature	K, (°C)	4, 5
To	Reference temperature	K	6
T <sub>min,ea</sub>	Minimum exchanger approach temperature	K	11
T <sub>st</sub>	Steam temperature	K	11
$\Delta T_{lm}$	Logarithmic mean temperature difference	K	6
t	Time	S	5,10
t <sub>f</sub>	Total operating/final time	S	5
t <sub>e</sub>	exposure time, parameter of the penetration model	S	10
T	temperature	K	10
U	Overall heat transfer coefficient	W/m <sup>2</sup> K	6
U	Big M Parameter		11
u	Control variables		5
$u_L$	liquid-phase velocity	m/s	10
U	length-specific molar holdup	mol/m	10
V	Vapor flow rate	kmol/s, kg/s	4, 8, 11
V <sub>R</sub>	Vapor flow rate in a rectifying column section	kmol/s	11
Vr	Reboil flow rate returned to the column	kmol/s	11

(continued)

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Symbol	Explanation	Unit	Chapter
V <sub>S</sub>	Vapor flow rate in a stripping column section	kmol/s	11
V	Molar volume	cm <sup>3</sup> /mol, m <sup>3</sup> /mol	2
V	Design variables		5
V	vapor molar flow rate	mol/s	10
W	Still holdup in differential distillation	mole	4, 5
W	Boolean variable		11
W <sub>ideal</sub>	Ideal compression power demand	W	6
WC	Boolean variable (determine if a condenser exists)		11
WR	Boolean variable (determine if a reboiler exists)		11
W	Binary variable		11
X	Parameter in the Gilliland graphical correlation		- 11
×	Vector of real variables		11
X	liquid mole fraction	mol/mol	10
x	liquid-phase composition vector	mol/mol	10
×i	Mole fraction of component i in the liquid phase	mol/mol	2, 4, 5, 8, 1
Υ	Content dependent Parameter in the Gilliland graphical correlation Boolean variable		11
У	Algebraic variable		5, 11
Уi	Mole fraction of component i in the vapor phase	mol/mol	2, 4, 5, 8, 1
У	vapor mole fraction	mol/mol	10
y	vapor-phase composition vector	mol/mol	10
Z	Content dependent Boolean variable Objective variable in optimization problems	-	11
Z	Boolean variable		11
Z	Compressibility factor	-	2
Z <sub>i</sub>	Mole fraction of component i	mol/mol	2, 4, 8, 11
Z	film coordinate; transformed liquid-phase concentration, Eq. (10-A11)	m -	10
z	liquid-phase composition vector consisting of $z_i$	-	10

## **Greek Symbols**

Symbol	Explanation	Unit	Chapter
α	Relative volatility	=	2, 4, 5, 10, 1
α	relative volatility vector consisting of $\alpha_i$	-	10
$\alpha^T$	heat transfer coefficient	$W/(m^2 K)$	10
$lpha_{ij}$	Non-randomness parameter in the NRTL equation $(\alpha_{ij} = \alpha_{ji})$	-	2
$\beta_{k}$	Size factor for column k (Andrecovich & Westerberg model)		11
$\beta, \beta_{ik}$	binary mass transfer coefficient	mol/(m <sup>2</sup> s)	10
$[\beta]$	matrix of mass transfer coefficients	mol/(m <sup>2</sup> s)	10
$\gamma_i$	Activity coefficient of component i	=	2, 4
γ	component net interstage flow, Eq. (10-A3)	_	10
Υ	component net interstage flow vector consisting of $\gamma_i$	-	10
Γ	Group activity coefficient	=	2
$[\Gamma]$	matrix of thermodynamic correction factors	=	10
δ	film thickness	m	10
ζ	Split fraction	_	11
λ	Eigenvalue	_	8
ρ	Density	kg/m, mol/m <sup>3</sup>	2
$\nu_{k}$	Number of structural groups in the mixture	_	2
$v_k^{(i)}$	Number of structural groups in pure solvent	_	2
$\phi$	Liquid phase ratio	-	8
$\phi_{A}$	Recovery factor for absorption section	-	11
$\phi_{i}$	Recovery factor for component i	-	11
$\phi_{R}$	Underwood root	_	11
$\phi_{\rm S}$	Recovery factor for stripping section	-	11
φ	Fugacity coefficient	_	2
$\varphi_{FB}$	Fischer-Burmeister function		11
φ	volumetric holdup	$m^3/m^3$	10
μ	chemical potential	J/mol	10
$\theta$	root of Underwood's equation	=	10
θ	vector of roots of Underwood's equation	_	10
τ	transformed time parameter, Eq. (10-1)	_	10
Ų	Recovery fraction	_	11
9	Temperature	°C	2
τ	Dimensionless time	_	8
τij	NRTL parameter	_	2
ξ	Dimensionless time scale	_	2
$\Omega(\cdot)$	Boolean function		11
ω	Acentric factor	_	2