John A. Goldak Mehdi Akhlaghi

# COMPUTATIONAL WELDING MECHANICS



## COMPUTATIONAL WELDING MECHANICS

by

#### John A. Goldak

Professor of Mechanical & Aerospace Engineering Carleton University, Ottawa Canada

#### Mehdi Akhlaghi

Associate Professor of Mechanical Engineering Amirkabir University of Technology, Tehran Iran Visiting Professor at Carleton University, Ottawa Canada



Library of Congress Cataloging-in-Publication Data

A C.I.P. Catalogue record for this book is available from the Library of Congress.

ISBN-10: 0-387-23287-7

e-ISBN 0-387-23288-5

Printed on acid-free paper.

ISBN-13: 978-0387-23287-4

© 2005 Springer Science+Business Media, Inc.

All rights reserved. This work may not be translated or copied in whole or in part without the written permission of the publisher (Springer Science+Business Media, Inc., 233 Spring Street, New York, NY 10013, USA), except for brief excerpts in connection with reviews or scholarly analysis. Use in connection with any form of information storage and retrieval, electronic adaptation, computer software, or by similar or dissimilar methodology now know or hereafter developed is forbidden.

The use in this publication of trade names, trademarks, service marks and similar terms, even if the are not identified as such, is not to be taken as an expression of opinion as to whether or not they are subject to proprietary rights.

Printed in the United States of America.

987654321

SPIN 11054023

springeronline.com

#### **Preface**

The presentation of this book emphasizes an exposition of the computational principles and the application of computational welding mechanics to practice.

The objective in Computational Welding Mechanics is to extend the capability to analyze the evolution of temperature, stress and strain in welded structures together with the evolution of microstructure. Distortion caused by volumetric strains due to thermal expansion and phase transformations are a dominate load in the stress analysis. The microstructure evolution influences the constitutive equations. In particular, as the temperature changes from above the melting point to room temperature, the stress-strain relationship changes from linear viscous, to visco-plastic to rate independent plasticity. In high strength steels, transformation plasticity can have a major affect in reducing the longitudinal residual stress in welds.

In the past twenty years the capability to analyze short single pass welds including the above physics has been developed. The software engineering to develop codes to solve these coupled problems has tended to be near the limit of what users and software developer can manage. The complexity has been too great to develop codes to deal with long multipass welds in complex structures. To deal with this problem, new software engineering methods and strategies have been developed, that are able to automatically create initial conditions, boundary conditions, adaptive mesh generation and manage time stepping. The input is a functional specification of the problem that includes a weld procedure, a weld path and a structure to be welded. The weld procedure contains weld parameters for each weld pass in a weld joint.

By giving designers the capability to predict distortion and residual stress in welds and welded structures, they will be able to create safer, more reliable and lower cost structures.

In the next ten years, we predict that computational weld mechanics will be used routinely in the welding industry. We believe that adequate solutions now exist to solve the problems related to managing the complexity now exist of software and the ease of use of the software.

There are some longer term issues that will require further research. One issue will be obtaining values (preferably functions) for the temperature and history dependent material properties of base metal and weld metal. Another issue will be obtaining sensor data characterizing welds and welded structures. We anticipate that real-time computational weld mechanics will lead to computer controlled welding systems that utilize a model not just of the weld pool but of the structure being welded. We also expect that this will lead to archiving huge amounts of data characterizing the welding process of constructing large structures such as a ship or submarine. Some of these archives will be public and some will be corporate. With such archives, data mining will be used to optimize processes and designs. In all of these endeavors, computational weld mechanics will play an essential role. In that role, the fundamental principles upon which computational weld mechanics is based will not change.

It is our hope that this book will help the reader to learn, understand and apply computational weld mechanics to problems in industry.

John A. Goldak and Mehdi Akhlaghi

#### Units

Currently changes are being made in the use of units from the English system to the *SI* system (le System international d'Unites). However, many articles referred to in this book use the English system and many readers of this book are still accustomed to the English system.

Below is a conversion table for units frequently used in this book.

To convert from	to	multiply by
inch (in.)	meter (m)	$2.54 \times 10^{-2}$
foot (ft)	meter	$3.048\times10^{-1}$
lbm/foot <sup>3</sup>	kilogram/meter3	1.601×10
Btu	joule (J)	$1.055 \times 10^{3}$
Calorie	joule	4.19
lbf (pound force)	Newton (N)	4.448
pound mass (lbm)	kilogram (kg)	$4.535\times10^{-1}$
Lbf/inch² (psi)	Newton/meter <sup>2</sup>	$6.894 \times 10^3$
kgf/meter <sup>2</sup>	Newton/meter <sup>2</sup>	9.806
Fahrenheit $(t_F)$	Celcius $(t_C)$	$t_C = (5/9)(t_F - 32)$

#### **Notations**

Efforts were made to use the same notation symbols, as much as possible, to express various quantities throughout the entire book. However, the authors have found that it is almost impossible to use a single, unified system of notation throughout the entire book because:

- 1. The book covers many different subjects.
- 2. The book refers to works done by many investigators who have used different notations.

Efforts were made to provide sufficient explanations whenever symbols are used.

#### **Table of Contents**

#### **Chapter I: Introduction**

1.1	Introduction and Synopsis	1
1.2	Brief history of computational welding mechanics	5
1.3	Mechanical behavior of welds	8
1.4	Major objective of this book	11
1.5	References	11
Chap	oter II: Computer Simulation of Welding Processes	
2.1	Introduction and Synopsis	16
2.2	The Computing Environment	18
	Computational Geometry	18
2.2.2	Models for Welding Heat Sources	22
	Theoretical Formulations	22
	Model Considerations	24
	Gaussian Surface Flux Distribution	26
	Hemi-spherical Power Density Distribution	30
	Ellipsoidal Power Density Distribution	30
	Double Ellipsoidal Power Density Distribution	32
2.2.3	Kinematic Models for Welding Heat Transfer	35
	Evaluation of the Double Ellipsoid Model	43
2.2.5	Modeling Thermal Stresses and Distortions in Welds	51
2.2.6	Microstructure Modeling in Heat Affected Zone (HAZ)	59
2.2.7	Spatial Integration Schemes	63
2.3	References	64
Chap	oter III: Thermal Analysis of Welds	
3.1	Introduction and Synopsis	71
3.2	Heat Transfer Theory	74
3.3	Weld Heat Source	76
3.3.1	Data to characterize a Weld Heat Source	77

3.3.2	Modeling a Weld Heat Source	79
	First Generation Weld Heat Source Models	80
	Second Generation Weld Heat Source Models	81
	Distributed Heat Source Models	83
	Prescribed Temperature Heat Source Models	83
	Third Generation Weld Heat Source Models	84
	Fourth Generation Weld Heat Source Models	85
	Fifth Generation Weld Heat Source Model	86
	Hierarchical Weld Process Models	87
3.4	Heat Transfer in Welds	87
3.4.1	Power Input	89
3.4.2	Implementation of prescribed temperature model	93
3.4.3	Starting Transient	94
	Boundary Conditions	95
3.4.5	Finite Element Solutions with Prescribed Temperature	98
3.4.6	Computational Results	100
	Complex Weld Pool Shape	100
	Welds with Filler Metal Addition	108
3.5	References	115
	oter IV: Evolution of Microstructure Depending On	
Tem	perature	
4.1	Introduction and Synopsis	119
4.2	Microstructure Model	124
4.2.1	Data Structures	131
	Flow lines	131
	Functionality of the Data Structure	132
	Layered tree description	132
	Locating elements	135
	Creating flow lines	136
4.2.2	Test Problems and Results	138
	Steady State Temperature Field	140
	Clipped transient temperature field	143
4.3	Hardness Calculation of the HAZ	148
4.4	References	149

### **Chapter V: Evolution of Microstructure Depending On Deformations**

5.1	Introduction and Synopsis	153
5.2	Properties for Modeling	158
5.2.1	Stresses, Strains and Deformations	162
5.2.2	Rate Independent Isotropic Plasticity	168
	Steady-State Formulation	169
	Deformation	172
	Strain Increment Measurement	174
	Numerical Results	176
5.2.3	Linear Viscous Isotropic Plasticity around melting pt	183
5.2.4	Rate dependent isotropic plasticity (General case)	184
5.2.5	Changing Constitutive Equations in Time and Space	185
5.2.6	Numerical Experiments and Results	186
5.3	References	195
Chap	oter VI: Carburized and Hydrogen Diffusion Analysi	is
6.1	Introduction and Synopsis	199
6.2	Carburization; Theory and Numerical Methods	203
6.2.1	Thermal, Microstructure and Stress Analysis	210
	Thermal Analysis	210
	Microstructure Analysis	211
	Thermal Stress Analysis	211
	Coupling Thermal, Microstructure and Stress Analysis	212
	Test	212
	Task Sequence	213
	Structure and Materials	214
	Deposition of Welds	214
	FEM Mesh	215
	Results and Discussion	217
6.3	Hydrogen Diffusion in Welds	226
6.3.1	Fundamental Equation	228
6.3.2	Preheat prediction	232
6.3.3	Computational Analysis	238
6.4	References	244

<b>Chapter VII: Welded Structures and Applications of Welding in Industrial Fields</b>			
7.1	Introduction and Synopsis	247	
	Weld Procedure	249	
7.3	Weld Joint	251	
	Analysis of a Weld Structure	252	
7.5	Real-Time for CWM	266	
7.5.1	Current Performance for CWM	269	
7.5.2	Implications of real-time CWM	271	
7.6	References	273	
Chap	oter VIII: Fracture Mechanics		
8.1	Introduction and Synopsis	277	
8.2	Review and Model Development	283	
8.3	Discussion	300	
8.4	References	302	
Chap	oter IX: Input Data for Computational Welding	g Mechanics	
9.1	Introduction and Synopsis	305	
9.2	Structure to be Welded	305	
9.3	Weld Procedure	307	
9.4	Thermal Analysis Outside the Weld Pool	308	
9.5	Microstructure Evolution	308	
9.6	Thermal Stress Analysis Outside the Weld Pool	309	
9.7	Weld Pool Solver	310	
9.8	Material Properties Summary	311	
9.9	Visualization	312	
9.10	Fracture Mechanics of Welded Structures	312	
Index		315	

#### Chapter I

#### Introduction

#### 1.1 Introduction and Synopsis

Welding as a fabrication technique presents a number of difficult problems to the design and manufacturing community. Nowhere is this more evident than in the aerospace industry with its emphasis on performance and reliability and yet where materials are seldom selected for their weldability.

Developments in calculating the thermal cycle and elastoplastic stress-strain cycle have been slow because of the inherent complexity of the geometry, boundary conditions and the nonlinearity of material properties in welding.

However, the exponential growth in computer performance combined with equally rapid developments in numerical methods and geometric modeling have enabled computational weld mechanics to reach the stage where it can solve an increasing number of problems that interest the industry specially in pipelines, power plants, refineries and pressure vessels, nuclear reactors, building and bridges, automotive, trucks and trains, ships, offshore structures, aerospace structures, micro electronics and many others.

Although the ability to perform such analyses is important, the real justification for computational weld mechanics is that it is becoming cheaper, faster and more accurate to perform computer simulations than to do laboratory experiments. Taken to the extreme all relevant decisions would become based on computer simulations. For example since nuclear testing in the atmosphere has been banned, this has actually occurred in nuclear weapons design, a field at least as complex as welding. It is unlikely that computational weld mechanics will eliminate all experiments in welding. Instead, computational weld mechanics is likely to increase the demand for accurate constitutive data, particularly at high temperatures, and to include the effect of changes in microstructure. Also it will not eliminate the need for experiments that simulate or prototype processes and products. However, it will dramatically reduce the number and cost of such experiments and greatly enhance the accuracy and significance of the data obtained for each experiment. In the automotive industry, *CAE* (Computer Aided Engineering) is said to have reduced the number of prototypes required from a dozen to one or two.

In the next few years, digital data collection of not only welding experiments but of production welding will be coupled to computer models. The computer models will use the experimental data to adjust the parameters in the computer model. The experiment and production system will use predictions from the computer model to control the process. The mathematics of this is called a Kalmann filter. In this case, the computer model and experiment are tightly connected. Neither could exist without the other. At this point religious wars between experimentalists and theorists will become meaningless.

Furthermore, models can be examined to provide insight that could never be obtained by experiment. For example, it is well known that work piece distortion caused by welding austenitic stainless steel is some three times greater than that caused by welding carbon steel. By analyzing models in which each property is varied separately, the sensitivity of the distortion to each property can be computed. This would provide the knowledge needed to understand the greater distortion in austenitic steel. Of course, this is not possible experimentally.

In its narrowest sense computational weld mechanics is concerned with the analysis of temperatures, displacements, strains and stresses in welded structures, Figure 1-1.

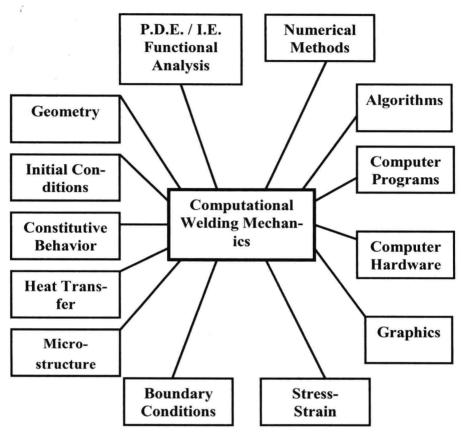


Figure 1.1: Computational welding mechanics draws on the disciplines shown above to compute the temperature, microstructure, stress and strain in welds. (PDE/IE-stands for Partial Differential Equations/ Integral Equations)

In its broadest context, it is an important element of Computer Aided Design (CAD) and Computer Aided Manufacturing (CAM). Computer modeling, in general provides the capability of storing vast amounts of data; of organizing and storing relations between data in databases or knowledge bases; and of using these data to compute or predict the behavior of products, processes or systems in the real world. On one hand, it can be viewed as a set of analytical tools for determining the mechanical response of a work piece to a given welding procedure. On the other hand, it can be viewed as a

design tool for predicting the quality of a weld and the deformation, Figure 1-2.

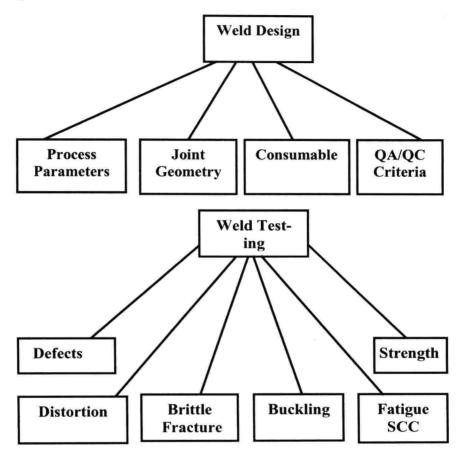


Figure 1-2: The important issues in design and testing of welds are shown schematically. (QA/QC is Quality Assurance, Quality Control and SCC is Stress Corrosion Cracking)

It is necessary at the outset to clearly fix the relationships of computer methods to experimental investigation, Figure 1-3.

Introduction 5

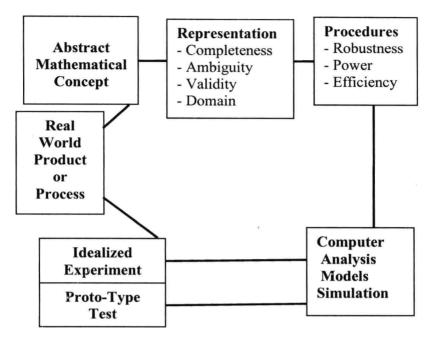


Figure 1-3: The relationships between the real world, experiments, mathematical abstraction and computer analysis.

Experiments tend to fall into two broad categories. Some are based on clearly understood theory where a strong attempt is made to exclude extraneous factors. Measurement of Young's modulus or thermal conductivity of a particular alloy fall into this category. On the other hand, when experiments deal with complex phenomena that do not have a clearly understood theory, a strong attempt is made to include any factor that may be relevant. Developing a narrow gap welding process is an example of this second category.

#### 1.2 Brief History of Computational Welding Mechanics

Historically, arc welding began shortly after electrical power became available in the late 1800s. Serious scientific studies date from at least the 1930s. The failure of welded bridges in Europe in the

1930s and the American Liberty ships in World War II did much to stimulate research in welding in the 1940s.

In the *USA*, the greatest attention was focused on developing fracture mechanics and fracture toughness tests. This could be interpreted as a belief that welding was too complex to analyze and therefore they chose an experimental approach that relied heavily on metallurgical and fracture toughness tests. The steady state heat transfer analysis of Rosenthal was an exception [3].

Russia took a different approach. The books of Okerblom [4] and Vinokurov [5] are a rich record of the analysis of welded structures including multi-pass welds and complex structures.

Over time the main techniques for solving heat transfer problems were changing with growing computer capacity. The strategy for analyzing welds and numerical methods (finite difference and finite element analysis) began in the 1960s with the pioneering work of Hibbitt and Marcal [6], Friedman [7], Westby [2], Masubuchi [8] and Andersson [9]. Marcal [11] made an early summary of experiences from welding simulation. Chihoski sought a theory to explain why welds cracked under certain conditions but not others [51, 52 and 53]. Basically, he imaged that the weld was divided into longitudinal strips and into transverse strips. He then computed the thermal expansion and contraction in each of these strips due to the temperature field of edge and butt welds. He concluded that a small intense biaxial compression stress field exists near the weld pool. Ahead of the compression field there may be a gap or a tensile stress field. Behind the compression field a tensile field or a crack can appear. The startling aspect of Chihoski's theory was that by varying the welding procedure, the position of this compress refield could be controlled. To support this theory, Chihoski developed a Moire' fringing technique to measure displacements during edge and butt weld. Chihoski used his theory to understand and solve a number of common problems: cracks and microcracks, forward gapping, upset and part distortion, sudden changes in current demand and unexpected responses to welding gaps. He considered the position and pressure of hold down fingers; the influence of localized heating or cooling; and the effects of gaps. He argued that these parameters could be optimized to obtain crack free welds.

Introduction 7

These authors consider Chihoski's papers to be among the most important in computational welding mechanics because he combined experience in production welds with an insight into weld mechanics that enabled him to conceive a theory that rationalized his observations and predicted solutions to his problems.

The reviews by Karlsson [12 and 13], Smith [17], Radaj [18 and 19] and Goldak [1, 14, 15, and 16] include references to simulations performed up to 1992. The research in Japan is reviewed by Ueda [20 and 21] and Yurioka and Koseki [22]. But Finite Element Analysis (FEA) methods gained a wide acceptance only over the last decade [10, 23, 24, 25, and 46].

The Moire'fringing technique of Chihoski is today one of the most powerful means of assessing *FEA* of stress and strain in welds (also see Johnson [55] for more on Moire' fringing methods for measuring strain in welds.).

The use of finite difference methods is more a transition between analytical and finite element methods. The main advantage of the finite difference method is that it is rather simple and easily understandable physically [10 and 26].

The finite element method has achieved considerable progress and powerful techniques of solving thermal-mechanical manufacturing process such as welding [1, 27, 28, 29 and 30]. Runnemalm presents in a dissertation thesis [24] the development of methods, methodologies and tools for efficient finite element modeling and simulation of welding. The recently published dissertation of Pilipenko [10] presents the development of an experimental, numerical and analytical approach to the analysis of weldability.