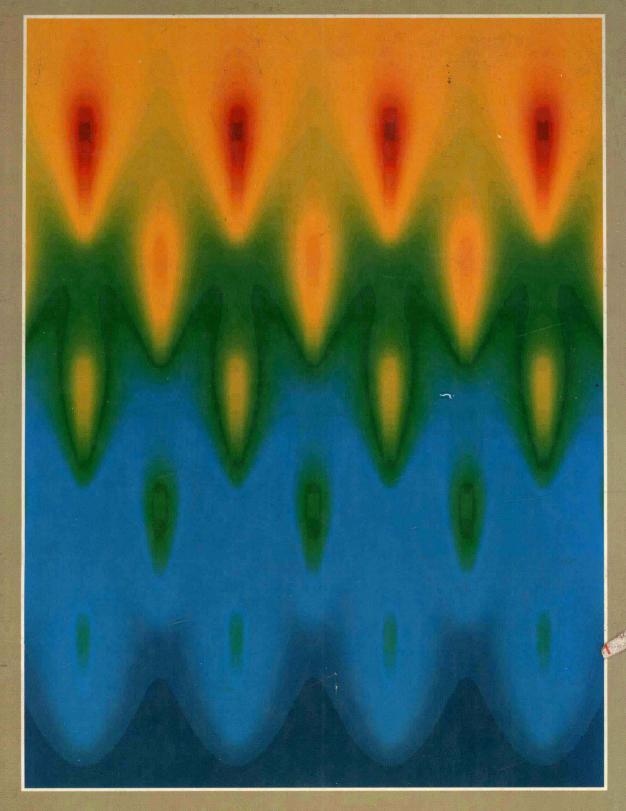
HEAT TRANSFER



ADRIAN BEJAN

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Adrian Bejan

J.A. Jones Professor of Mechanical Engineering Duke University



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Other books by Adrian Bejan:

Entropy Generation through Heat and Fluid Flow, Wiley, 1982, 248 pages. (Solutions Manual, Wiley, 1984, 50 pages, available from the author.)

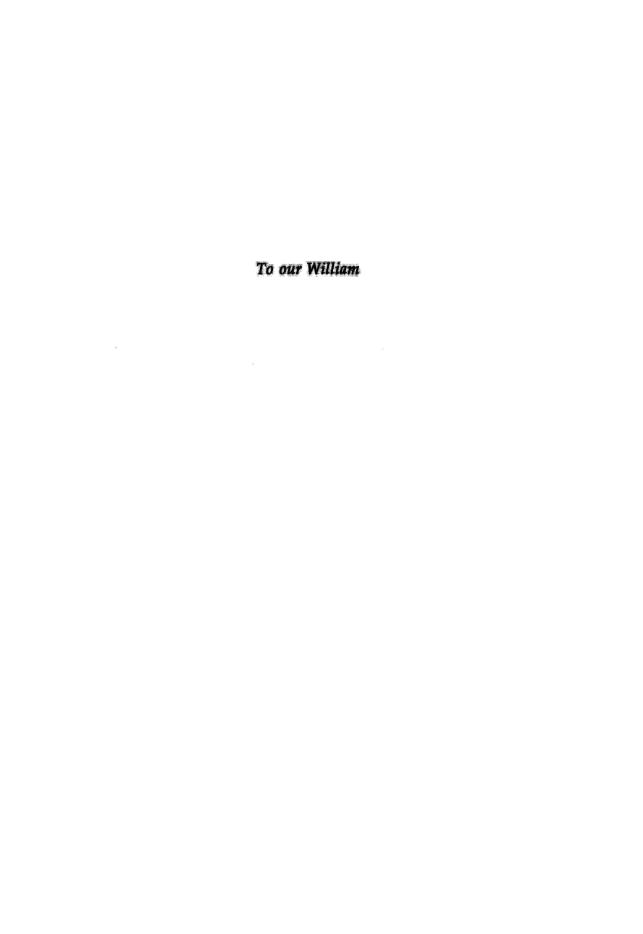
Convection Heat Transfer, Wiley, 1984, 477 pages.

(Solutions Manual, Wiley, 1984, 218 pages, available from the publisher and from the author.)

Advanced Engineering Thermodynamics, Wiley, 1988, 759 pages.

(Solutions Manual, Wiley, 1988, 153 pages, available from the publisher and from the author.)

Convection in Porous Media, with D. A. Nield, Springer-Verlag, 1992, 425 pages.



PREFACE

The principal objective in writing this textbook for a first course in heat transfer is to present a rigorous and refreshing treatment of the subject, and to relate heat transfer to other disciplines, in particular, thermodynamics and fluid mechanics. This book is about "modern" heat transfer, that is, it is intended to reflect the changes currently taking place in the engineering profession and in engineering education.

Engineering Design

Engineering work and research are driven not only by human curiosity but also by the real needs of our society. For this reason, this book emphasizes design, or the synthesizing of two or more issues (i.e., engineering disciplines) into an answer with a practical meaning. The student is called on to recognize that there is more than one way in which to design a heat transfer apparatus—and to understand that knowing the worst design (the greatest pitfall, or trap) is often as important as knowing the optimal solution and all of the other options in between.

Design questions are drawn from many diverse areas. They include, for instance, insulations for walls with nonuniform temperature, insulations that must provide mechanical rigidity and support, the safe disposal of hot ash, the stabilization of superconductors, optimal packing of fibrous insulation, fins subjected to material constraint, and several applications covering the packaging and cooling of integrated electronic circuits. Each design question is presented in a fundamental way, so that (1) the answer can be used in more than one application, and (2) the work of arriving at the answer has the greater educational value.

Interdisciplinary Approach

This book teaches heat transfer as a discipline that works hand-in-hand with other disciplines in the evolution of a process, or in the successful performance of a device. Throughout its discussion emphasizes that real applications tend to be interdisciplinary, and that good work requires a solid foundation in all of the compartments of engineering education. The material presented in the chapter discussions and in the problems at the end of each chapter illustrates extensively the interfaces between heat transfer and other disciplines, such as metallurgy, structural mechanics, tribology, electrical engineering, superconductivity, cryogenics, and solar and geothermal energy production.

The emphasis of this book on the interdisciplinary character of real-life thermal engineering, however, does not detract from the teaching of heat transfer first as a self-standing *discipline*, that is, a field with its own scope, language, and rules. Interdisciplinary engineering can only be practiced by the engineer who is solidly grounded in the fundamentals of each discipline. To gloss over the fundamentals in the quick and currently popular pursuit of "interdisciplinary" topics would be to promote shallowness in the name of erudition and modernism.

Student Oriented

Early in my career, I discerned a need to present a course that treats each student as an intelligent human being, regardless of his or her background or aspirations. In this book, my goal is to reach simultaneously the curious, who are attuned to asking more questions, and the pragmatic, who prefer to get on with their calculations based on well-defined formulas.

Relationship to Fluid Mechanics, Thermodynamics, and History of Engineering

The book stresses the importance of fluid mechanics as a prerequisite for heat transfer analysis. To understand the flow configuration and its regime (laminar versus turbulent) is tremendously important not only in convection heat transfer calculations but also in *conjugate* situations in which convection is accompanied by conduction and radiation.

The role of thermodynamics in heat transfer is presented with great care. This begins with the calorimetric terminology, which is shared by both disciplines, and continues with the thermodynamic meaning of heat transfer engineering concepts, such as natural ("free") convection, heat exchanger pressure drop, and solar collector optimization.

Throughout the book I explain where each concept and formula comes from. In many instances, I provide the history of the concept and, sometimes, even the origin of the words that are used to name that concept.

Scale Analysis

This book makes a strong case for the use of simple and approximate analyses. Special emphasis is placed on order-of-magnitude calculations, or "scale analysis." I previously used this method in my graduate text on *Convection Heat Transfer* (Wiley, 1984). Since then, I have found that scale analysis can play an even greater role in a first course on heat transfer, where it can be used to solve

conduction problems in addition to those of convection. Approximate methods, such as scale analysis and integral analysis, are emphasized because of their high rate of "return on investment." This has always been a central objective in engineering practice.

Problem-Solving Material

The emphasis on physical understanding and the freedom to choose between exact and approximate calculations is reflected also in the problem-solving material included in this course. The simplest problems are presented in the text as worked out *examples*, whereas the more challenging ones are proposed as *problems* at the end of each chapter. In later chapters, the *projects* that follow the problems require more time to solve. These projects usually have greater design content, and may be developed by the instructor into homework of longer duration.

It is always a good idea to begin solving a problem by executing a *good drawing*, and I have tried to demonstrate this to the student. Making a good drawing requires the student to explain to himself or herself the physics of the problem. Learning to take this preliminary step will be a benefit in the student's future career in engineering. The *Solutions Manual* that accompanies this book reflects the same care for problem solving (explanations, details, graphics) that is exhibited throughout the text. I wrote the solutions manual myself, as a "second book" in both content and appearance.

Looking Back at the Last Four Years

I am extremely fortunate to be and work at Duke University, which has provided me with a very friendly and supportive environment and, above all, freedom. It is a rare privilege to be allowed the freedom to think one's own thoughts.

Mary, my wife, was once again my chief collaborator and counselor. I owe every bit of my progress to her. Our family was also very supportive and a steady reminder of what is really important. I am deeply indebted to my parents-in-law, Terry Riordan and the late Bill Riordan, who actively supported my work, laboratory, and students.

Linda Hayes typed the entire manuscript while improving its English and organization. She also prepared the *Solutions Manual* on the word processor so that the manual, too, has a professional appearance. Her exquisite work is an important part of this finished project. I am very grateful to her for all of her help.

Several of my colleagues and students helped me during various stages of this project. I thank Katherine McKinney, Kathy Vickers, Dianne Himler, Eric Smith, Stoian Petrescu, Peter Jany, Dimos Poulikakos, John Georgiadis, Ira Katz, Michael Kazmierczak, P.V. Kadaba, Ab Hashemi, M. V. Vazquez, Ulrich Gösele, Sang W. Lee, Sung J. Kim, Jose Lage, Jong Lim, Alexandru Morega, and Alex Fowler. I treasure their support. I also appeal to the readers to communicate to me any errors that may persist in this final version.

Adrian Bejan Durham, North Carolina May 1992

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A. B.

ABOUT THE AUTHOR

Adrian Bejan received his B.S. (1972, Honors Course), M.S. (1972, Honors Course), and Ph.D. (1975) degrees in mechanical engineering, all from the Massachusetts Institute of Technology. From 1976 until 1978, he was a Fellow of the Miller Institute for Basic Research in Science, at the University of California, Berkeley. Before coming to Duke as a full professor in 1984, he taught at the University of Colorado, Boulder.

Professor Bejan is the author of three graduate-level textbooks, Entropy Generation through Heat and Fluid Flow, Convection Heat Transfer, and Advanced Engineering Thermodynamics, and is coauthor of a research monograph on Convection in Porous Media. In addition, he has written 190 technical articles on a variety of topics, including natural convection, combined heat and mass transfer, convection through porous media, transition to turbulence, second-law analysis and design, solar energy conversion, melting and solidification, condensation, cryogenics, applied superconductivity, and tribology.

Adrian Bejan is the 1990 recipient of the thermodynamics award of the American Society of Mechanical Engineers (ASME), the James Harry Potter Gold Medal. He also received the Gustus L. Larson Memorial Award of the ASME in 1988, and was elected Fellow of the ASME in 1987. He was awarded the J. A. Jones chair at Duke in 1989.

LIST OF SYMBOLS

a_i	impurity-scattering resistivity coefficient (m·K²/W), eq. (1.30)	b_n	dimensionless characteristic values, Table 4.1
a_n	dimensionless characteristic values, eq. (3.43) and Table 3.1	В	cross-section shape number, eq. (6.30)
a_p	phonon-scattering resistivity coefficient (m/W·K), eq. (1.30)	В	driving parameter for film condensation, eq. (8.26)
Α	area (m²)	Bi	Biot number, eq. (2.63)
A_c	cross-sectional area (m²)	Bo_v	Boussinesq number, $Bo_v = Ra_v Pr$
A_c	minimum free-flow area (m²), eq. (9.65)	с	specific heat of incompressible substance (J/kg·K)
$A_{\rm exp}$	fin surface exposed to the fluid (m^2)	с	speed of light in vacuum, Appendix A
A_f	finned area (m ²), contributed by the exposed surfaces of the fins,	c_v	specific heat at constant volume (J/kg·K)
A_{fr}	Chapter 9 frontal area (m²), eq. (9.65)	C_{P}	specific heat at constant pressure $(J/kg \cdot K)$
A_n	normal or projected area (m2)	С	capacity rate (W/K), or $\dot{m}c_P$
A_u	unfinned area (portions) of the wall (m ²), Chapter 9	C_c	correction factor, Fig. 10.27
A_0	bare surface, projected surface (m²), Fig. 2.10	C_i	molar concentration of species i (kmol/m ³)
$A_{0,f}$	finned portion of bare surface	C_D	drag coefficient, eq. (5.138)
0,j	(m ²), Fig. 2.10	$C_{f,x}$	local skin friction coefficient, eq.
$A_{0,u}$	unfinned portion of bare surface	=	(5.39)
_	(m ²), Fig. 2.10	$\overline{C}_{f,x}$	average skin friction coefficient, eq. (5.55)
b	thermal stratification parameter,	C_{sf}	• • •
h h	eq. (7.71)	℃ _{sf}	empirical constant for liquid – surface combination, Table 8.1
b, b _T	transversal length scales (m), eqs. (5.148)–(5.149)	C_w	correction factor, Fig. 10.29

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d	diameter (m)	G	total irradiation (W/m²)
D	diameter (m)	Gr_y	Grashof number based on
D	mass diffusivity, diffusion	,	temperature difference and height y,
	coefficient, or diffusion constant		$Gr_y = g\beta y^3 \Delta T/v^2 = Ra_y/Pr$
	(m^2/s)	Gz	Graetz number, eq. (6.53)
D_h	hydraulic diameter (m), eq. (6.28)	$G_{\mathcal{L}}$	constant, Table 7.1
D_i	inner diameter (m)	G_{λ}	monochromatic irradiation
D_o	outer diameter (m)		$(W/m^2 \cdot m)$
D_{12}	mass diffusivity of species 1 into species 2 (m ² /s)	h	heat transfer coefficient for external flow $(W/m^2 \cdot K)$, eq. (1.54)
e	specific internal energy (J/kg), eq. (5.12)	h	heat transfer coefficient for internal flow $(W/m^2 \cdot K)$, eq. (1.55)
E	energy (J)	h	Planck's constant (J·s), Appendix
Ε	modulus of elasticity (N/m²)		A
E	total hemispherical emissive	h	specific enthalpy (J/kg)
	power (W/m²)	h_e	effective heat transfer coefficient
E_b	total hemispherical blackbody		(W/m ² ·K), eq. (9.7)
	emissive power (W/m²)	h_f	specific enthalpy of saturated
$E_{b,\lambda}$	monochromatic hemispherical		liquid (J/kg)
	blackbody emissive power	h_{fg}	latent heat of condensation
г.	(W/m⋅m²)		(J/kg) , $h_g - h_f$
Ec	Eckert number, Appendix A	h_{fg}'	augmented latent heat of
E_{λ}	monochromatic hemispherical		condensation (J/kg), eqs. (8.10)
	emissive power (W/m·m²)	L "	and (8.17)
f	factor, Figs. 9.37–9.38	h_{fg}''	augmented latent heat of
f	friction factor, eq. (6.24)	h_g	condensation (J/kg), eq. (8.41)
f_v	vortex shedding frequency (s^{-1}), eqs. (5.137) and (F.9)		specific enthalpy of saturated vapor (J/kg)
f_v	fire pulsating frequency, eq. (F. 10)	h_m	local mass transfer coefficient
F	correction factor, Figs. 9.16-9.20		(m/s), eq. (11.57)
F	force (N)	h_s	specific enthalpy of saturated
F	similarity streamfunction profile, eq. (7.45)	h_{sf}	solid (J/kg) latent heat of melting, or of
F_D	drag force (N)		solidification (J/kg), $h_f - h_s$
F_n	normal force (N)	h_x	local heat transfer coefficient
Fo	Fourier number (dimensionless	_	$(W/m^2 \cdot K)$ at position x
F_r , F_θ ,	time), eqs. (4.63)	\overline{h}_x	average heat transfer coefficient $(W/m^2 \cdot K)$ averaged over length x
F_z	body forces per unit volume	\overline{h}_D	heat transfer coefficient
	(N/m^3) , Table 5.2		(W/m2·K) averaged over cylinder
F_r , F_{ϕ} ,			or sphere of diameter D
F_{θ}	body forces per unit volume	Н	enthalpy (J)
	(N/m^3) , Table 5.3	Н	enthalpy flowrate per unit length
F_t	tangential force (N)		(W/m), eq. (8.5)
F_{12}	geometric view factor, eq. (10.33)	H	height (m)
8	gravitational acceleration (m/s2)	H	Henry's constant (bar), Table 11.5
G	mass velocity (kg/m2·s), eq. (9.58)	i	specific enthalpy (J/kg), eq. (5.16)
G	similarity vertical velocity profile,	I_b	total intensity of blackbody
	eq. (7.43)	·	radiation (W/m ² ·sr)

		_	
$I_{b,\lambda}$	intensity of monochromatic blackbody radiation (W/m³·sr)	L_0	Lorentz constant, 2.45×10^{-8} $(V/K)^2$
I_{λ}	intensity of monochromatic radiation (W/m³·sr)	m	fin parameter (m^{-1}), eq. (2.92) integer
;	Colburn j_H factor, eq. (9.75)	m	mass (kg)
Јн :	diffusion mass flux of species i	m 	100 - 100 -
Ji	(kg/m ² ·s)	ṁ ṁ'	mass flowrate (kg/s)
\hat{j}_i	diffusion molar flux of species i	m	mass flowrate per unit length (kg/s·m)
	(kmol/m²·s)	m''	mass flux (kg/m²·s)
J	electric current density (A/m ²)	$\dot{m}_i^{\prime\prime\prime}$	volumetric rate of species i
J	radiosity (W/m²)		generation (kg/ $m^3 \cdot s$), eq. (11.2)
Ja	Jakob number, eq. (8.19)	M	dimensionless factor, eq. (6.84)
J_0	zeroth-order Bessel function of	M	molar mass of mixture (kg/kmol)
	the first kind, Fig. 3.6 and	M_i	molar mass of species i (kg/kmol)
1000	Appendix E	n	direction normal to the boundary
J_1	first-order Bessel function of the		(m), Table 3.2
•	first kind, eq. (3.63)	n	integer
k	Boltzmann's constant, Appendix A	N	number of moles in mixture
k	thermal conductivity (W/m·K)		sample (kmol)
$k_{ extbf{avg}}$	average thermal conductivity $(W/m \cdot K)$, eq. (2.55)	N_i	number of moles of species <i>i</i> (kmol)
k _e	thermal conductivity due to	NTU	number of heat transfer units, eq.
	conduction electrons (W/m·K)	1114	(9.27)
k_l	thermal conductivity due to	\dot{N}	molar flowrate (kmol/s)
	lattice vibrations (W/m·K)	Ń'	molar flowrate per unit length
k_i^{-1}	thermal resistivity due to impurity scattering (m·K/W)		(kmol/m·s)
k_p^{-1}	thermal resistivity due to phonon	Nu_x	Nusselt number based on the
,	scattering (m·K/W)	\overline{Nu}_D	local heat transfer coefficient $h_x x/k$ overall Nusselt number based on
k_s	sand roughness scale (mm), Fig.	Nu_D	the surface-averaged heat transfer
	6.14		coefficient $\bar{h}_D D/k$, where D is the
K	constant coefficient		diameter
K	permeability (cm ²), Appendix B	$\overline{Nu}^0_{\mathcal{L}}$	constant, Table 7.1
K _c	contraction loss coefficient, Figs.	\overline{Nu}_{x}	overall Nusselt number based on
	9.30 and 9.31	-	the x-averaged heat transfer
Ke	enlargement loss coefficient, Figs.		coefficient $h_x x/k$
	9.30 and 9.31	p	number of iterations, Chapter 3
1	equivalent length (m), eq. (7.84)	p	perimeter (m)
1	length (m)	p	perimeter of contact with fluid
ı	mixing length (m), eq. (5.109)		(wetted perimeter) (m)
L	characteristic length (m), eq. (7.76)	P	dimensionless parameter, Figs.
L	length (m)	n	9.16-9.20
\mathcal{L}	equivalent length (m), eqs. (5.140)	P	pressure (Pa or N/m²)
2	and (7.85)	P	mechanical power (W)
Le	Lewis number, Le = Sc/Pr =	Pe_D	Peclet number based on diameter,
	α/D , Table 11.7	Do	$U_{\infty}D/\alpha$, UD/α Peclet number based on
L_c	corrected fin length (m), eq. (2.112)	Pe_x	longitudinal length, $U_{\infty}x/\alpha$
L _e	equivalent length (m), Table 10.5	Pr	Prandtl number, $Pr = v/\alpha$
-e	-1 mon 101.0 (11)/ 14010 1010		

\Pr_t	turbulent Prandtl number, $Pr_t = \varepsilon_M / \varepsilon_H$	Re	Reynolds number $V_{\text{max}}D_h/v$, eq. (9.70)
P_{i}	partial pressure of component i (N/m^2)	Re_D	Reynolds number based on diameter, $U_{\infty}D/v$, UD/v
q	heat transfer rate (W)	Re_{l}	local Reynolds number, Appendix
q_b	total heat transfer rate through		F
	the fin (W)	Re_x	Reynolds number based on
$q_{ m tip}$	heat transfer through the tip of the fin (W)	D _o	longitudinal length, $U_{\infty}x/v$
q'	heat transfer rate per unit length	Re_y	condensate film Reynolds number, $4\Gamma(y)/\mu_i$, eq. (8.22)
4	(W/m)	R_{i}	internal radiation resistance
q''	heat flux (W/m²)		(m ⁻²), eq. (10.78)
ġ	volumetric rate of internal heat generation (W/m^3)	R_{r}	radition thermal resistance (m^{-2}) , eq. (10.45)
$q_{w,x}^{"}$	local wall heat flux (W/m²)	R_t	thermal resistance (K/W), eq. (2.8)
$\overline{q}_{w,x}^{"}$	x-averaged wall heat flux	s	empirical constant, Table 8.1
	(W/m^2) , eq. (5.80)	s_n	dimensionless characteristic
$q_{1\rightarrow 2}$	one-way heat current (W) from 1		values, Table 4.2
_	to 2	S	conduction shape factor, eq.
91-2	net heat current (W) from 1 to 2	S	(3.33) and the header of Table 3.3
Q Q'	heat transfer (J)	S	entropy (J/K) solubility coefficient
Q	heat transfer interaction per unit length (J/m)	5	(kmol/m³·bar), Table 11.6
Q''	heat transfer interaction per unit	Sc	Schmidt number, $Sc = v/D$
	area (J/m²)	Sh_x	local Sherwood number, eq.
r	radial coordinate (m), Figs. 1.8	77001	(11.65)
	and 1.9	St	x-independent Stanton number
r_i	inner radius (m)	Ste	h/pc _p U Stofan number of (4.110)
r_o	outer radius (m)	St _m	Stefan number, eq. (4.119) local mass transfer Stanton
$r_{o,c}$	critical outer radius (m), eqs. (2.44) and (2.47)		number, eq. (11.85)
r_s	thermal resistance of the scale	St _x	local Stanton number $h_x/\rho c_p U_\infty$
_	$(m^2 \cdot K/W)$, eq. (9.5)	t	thickness (m)
R	dimensionless parameter, Figs.	t	time (s)
R	9.16–9.20	t_c T	transition time scale (s), eq. (4.9)
R	radius (m)	1	temperature (K or °C), eqs. (1.5) and Fig. 1.2
R	function of r only, Chapter 3	T_{b}	base temperature in fin analysis
K	ideal gas constant (kJ/kg·K), Appendix D		(K), Chapter 2
\overline{R}	universal ideal gas constant, Appendix A	T_b	bulk, or mean temperature (K or °C)
$Ra_{m,y}$	mass transfer Rayleigh number,	T_c	center temperature (K), Chapter 4
	eq. (11.102)	T_{i}	initial temperature (K)
Ra _y	Rayleigh number based on temperature difference and height y , $Ra_y = g\beta y^3 \Delta T/\alpha v$	$T_{i,j}$	temperature of the control volume surrounding the node (<i>i</i> , <i>j</i>), Chapter 3
Ra_y^*	Rayleigh number based on heat flux and height <i>y</i> ,	T_m	mean, or bulk temperature (K), eq. (6.33)
	$Ra_y^* = g\beta q_w^* y^4 / \alpha v k$	T_m	melting point temperature (K)

T_{sat}	saturation temperature (K)	x	Cartesian coordinate (m), Fig. 1.7
T_w	wall temperature (K or °C)	x_i	mole fraction
T_{0}	surface temperature (K), Chapter 4	x_{tr}	transition length (m)
T_{0}	reference temperature (K or °C)	X	flow entrance length (m), eqs.
T_{∞}	free-stream or reservoir		(6.4') and (6.65)
	temperature (K or °C)	X	function of x only, Chapter 3
и	specific internal energy (J/kg)	X_{C}	concentration entrance length
и	velocity component in the x		(m), eq. (11.93)
	direction (m/s)	X_{l}	longitudinal pitch (m)
U	average longitudinal velocity (m/s)	X_t	transversal pitch (m)
И	internal energy (J)	X_T	thermal entrance length, eqs.
U	mean velocity (m/s), eq. (6.1)		(6.32) and (6.65)
И	overall heat transfer coefficient (W/m ² ·K)	X_l^{\bullet}	dimensionless longitudinal pitch X_1/D
U_{∞}	free stream velocity (m/s)	X_t^{\bullet}	dimensionless transversal pitch
v	specific volume (m³/kg)		X_t/D
v	velocity in the y direction (m/s)	X, Y, Z	body forces per unit volume
v_n	normal velocity (m/s)		(N/m^3) , Table 5.1
\boldsymbol{V}	mean longitudinal velocity (m/s)	y	Cartesian coordinate (m), Fig. 1.7
\boldsymbol{V}	volume (m³)	Y	function of y only, Chapter 3
V	volume (m³), Chapter 9	Y_0	zeroth-order Bessel function of the second kind, Fig. 3.6
w	mechanical transfer rate, or power (W)	z	axial position in cylindrical coordinates (m), Fig. 1.8
W	width (m)	~	Cartesian coordinate (m), Fig. 1.7
W	work transfer (J)	z Z	
Ŵ	work transfer rate, or power (W)	L	function of z only, Chapter 3
Greek L	etters		
α	heat transfer area density (m^2/m^3) , eq. (9.64)	δ	skin thickness, boundary layer thickness (m)
α	thermal diffusivity (m ² /s), $\alpha = k/\rho c_P$	δ	velocity boundary layer thickness (m), eq. (5.25)
α	total absorptivity	δ^{ullet}	displacement thickness (m), eq.
α	total hemispherical absorptivity		(5.58)
$lpha_0$	temperature coefficient of electrical resistivity (${}^{\circ}C^{-1}$),	δ_{s}	thickness of shear layer (m), eq. (7.38)
	Appendix B	$\delta_{\scriptscriptstyle T}$	thermal boundary layer thickness
α_{λ}	monocromatic hemispherical		(m), eq. (5.60)
	absorptivity	δ_{99}	velocity boundary layer thickness
$lpha_\lambda^\prime$	directional monochromatic	4.0	(m), eq. (5.57)
	absorptivity	ΔP	pressure drop (N/m^2) , eq. (6.27)

(K), eqs. (6.105) and (9.22) β_c composition expansion coefficient (m^3/kg) , eq. (11.99) $\Delta\epsilon$ correction term, Fig. 10.30 Γ condensate mass flowrate per convergence criterion, eq. (3.99) ϵ unit length (kg/s·m), eq. (8.4) ϵ heat exchanger effectiveness, eq. δ film thickness (m), Chapter 8 (9.29)

coefficient of volumetric thermal expansion (K^{-1}) , eq. (5.18)

β

 ΔT

 ΔT_{lm}

temperature difference (K)

log-mean temperature difference

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ϵ ϵ ϵ_f ϵ_H	overall surface efficiency, eq. (9.4) total hemispherical emissivity fin effectiveness, eq. (2.118) thermal eddy diffusivity (m ² /s), eq. (5.100) momentum eddy diffusivity (m ² /s), eq. (5.99)	ν ν Π ρ	frequency (s ⁻¹) kinematic viscosity (m ² /s), $v = \mu/\rho$ pressure drop number, $\Pi = \Delta P \cdot L^2/\mu\alpha$ density (kg/m ³) total reflectivity
ϵ_0	overall projected-surface effectiveness, eq. (2.79) monochromatic hemispherical	$ \rho_e $ $ \sigma $	electrical resistivity (W·m/A²) contraction ratio, eq. (9.53)
ϵ_{λ}	emissivity directional monochromatic	σ	Stefan-Boltzmann constant, Appendix A surface tension (N/m), Table 8.2
η	emissivity fin efficiency, eq. (2.115)	σ_{xx}	normal stress (N/m^2) , eq. (5.8)
η	similarity variable compressor isentropic efficiency	τ	angle of enclosure inclination (rad), Fig. 7.23
η_c η_p	pump isentropic efficiency	$ au_{w,x}$	total transmissivity local wall shear stress (N/m²)
θ	angular coordinate (rad), Figs. 1.8 and 1.9	$\overline{ au}_{w,x}$	x-averaged wall shear stress (N/m^2) , eq. (5.54)
heta heta	excess temperature (K), eq. (2.88) momentum thickness (m), eq. (5.59)	$ au_{xy} \ au_{\lambda} \ \phi$	tangential stress (N/m ²), eq. (5.8) monochromatic transmissivity angle of wall inclination (rad),
θ	similarity temperature profile, eq. (7.46)	ϕ	Fig. 7.10 angular coordinate (rad), Fig. 1.9
θ	thermal potential function (W/m), eq. (2.51)	ϕ	dimensionless temperature profile, eq. (6.45)
$ heta_b$	excess temperature of fin base (K) von Karman's constant, eq. (5.112)	ϕ	relative humidity, Appendix D porosity, Appendix B
κ_{λ}	monochromatic extinction coefficient (m ⁻¹)	φ .	viscous dissipation function (s^{-2}), eq. (5.15)
λ	characteristic value, Chapter 3	Φ_i	mass fraction ρ_i/ρ
λ	dimensionless parameter in the Stefan solution, eq. (4.118)	χ Ψ	correction factor, Figs. 9.37–9.38 streamfunction (m ² /s), eq. (5.45)
λ	wavelength (m)	ω	solid angle (sr)
μ	characteristic value, Chapter 3 viscosity (kg/s·m), eq. (5.10)	ω	specific humidity, or humidity ratio, Appendix D

Subscripts

() _a	absorbed, Chapter 10	() _c	centerline, center, midplane
() _a	air, Chapter 11	() _c	cold
() _{acc}	acceleration	() _c	compressor
() _{app}	apparent	() _{eddy}	eddy transport
() _{avg}	average	() _f	fluid
() _b	base of the fin, Chapter 2	()8	gas, Chapter 10
() _b	black, Chapter 10) _h	hot
() _b	bulk, mean	($)_i$	initial
(),	carbon dioxide, Chapter 10	(),	inner