

Porous Media

Fluid Transport and Pore Structure

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To my friend and colleague Howard Brenner for his encouragement and inspiration

Preface

The unique property of a porous medium, the one that distinguishes it from other solid bodies on the one hand, and from simple conduits on the other, is its complicated pore structure. The vast majority of porous media contain an interconnected three-dimensional network of capillary channels of nonuniform sizes and shapes, commonly referred to as "pores."

Fluid flow, diffusion, and electrical conduction in porous media take place within extremely complicated microscopic boundaries that make any rigorous solution of the equations of change in the capillary network practically impossible. This is one reason why some of the brilliant and successful practitioners in the field of "flow through porous media" have tried, as much as possible, to stick with the continuum approach in which no attention is paid to pores or pore structure. The other reason is that the continuum approach is often adequate for the phenomenological description of macroscopic transport processes in porous media. The continuum approach fails to provide a clue to help explain any of a multitude of observations that depend on the properties of the microscopic channels and the behavior of the fluids on the microscopic scale. The desire of scientists and engineers to be able to understand and then explain their observations has always been a powerful driving force for progress. Therefore there have been numerous attempts over the past fifty years or so to explain the flow phenomena in terms of the microscopic structure as accurately as possible. The results have

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seldom been entirely satisfactory, but with every step a further penetration into an immensely complicated territory has been achieved. There is a great deal of information available in the technical literature on the role played by pore structure in determining transport phenomena in pore spaces.

This book has been written with the primary purpose of presenting in an organized manner the most pertinent information available on the role of pore structure and then putting it to use in the interpretation of experimental data and the results of model calculations.

Pore structure is inseparable from the convective, diffusive, and interfacial effects that take place in the pores; these effects are all interrelated so that there is little point in trying to evaluate their relative merits with the aim of deciding which of them is most important.

Existing books on "flow through porous media" have been written with an emphasis on the fluid mechanical aspects. Interfacial effects, such as interfacial tension and wettability, have been under intensive and productive investigation for quite some time. In this book the author has made an attempt to show that there are benefits to be gained by trying to think about the phenomena in porous media in terms of interactions among the three main factors, i.e., transport phenomena, interfacial effects, and pore structure. The book contains many examples of applications of this concept, and it is the hope of the author that many readers will find this approach useful as well as an inspiration and motivation to do more fundamental research on the role played by pore structure.

The author wishes to acknowledge an operating grant from the National Research Council of Canada. A number of persons have contributed their invaluable time and energy to the preparation of this book, and without their help it could not have been written. Therefore the author takes great pleasure in acknowledging the perfect typing and dedication of Nancy Stade; the outstanding professional artwork of Rinze Koopmans; the helpful comments offered by Professor D. R. Spink who read the Preface and the Introduction; the prompt and competent assistance of Baiba Gomes with the Bibliography; the innumerable discussions conducted with P. K. Shankar and I. Chatzis; and last but not least, the author is deeply indebted to his wife, Ruth, for putting up with him while he worked on the book and for the loving help she gave with the organization of the Bibliography.

List of Symbols

Latin Letters

a	speed of sound; edge length of cube; cross-sectional area; Turner-
	structure parameter; narrow half-width; medium dispersivity; activity
a'	dynamic medium dispersivity
a"	geometric medium dispersivity
a_{ijkl}	component of medium dispersivity tensor
a_j	$\equiv l_i/D_i$
Å	area ef plane; cross-sectional area of pore or sample; area of circle; con-
	stant parameter
A_A	fractional area of phase A in the plane of section
<i>b</i>	constant parameter; number of branches; Turner-structure parameter
В	constant parameter; hydraulic conductance of channel
c	adjustable parameter; mass concentration
C	constant parameter; connectivity; factor defined by Eq. (3.2.12)
C'	"shift factor" [Eq. (4.7.4)]
$C_{\mathbf{A}}$	molar concentration of A
$C_{\mathbf{p}}$	specific heat at constant pressure
$C_{\mathbf{p}}$ $C_{\mathbf{v}}$	specific heat at constant volume
D	pore (capillary) diameter; sphere diameter
Da	$\equiv \Delta \mathcal{P}/\alpha \mu v L$ (Darcy number)
D_{h}	bulge diameter
D'_{ct}	coefficient of hydrodynamic dispersion in a capillary
D_e	pore entry diameter
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\mathscr{D}_{\mathrm{eff}}
                               effective diffusion coefficient
  D_{\rm f}
                               fiber diameter
  D_{H}
                            \equiv 4r_{\rm H} = {\rm hydraulic\ diameter}
  D_{ii}
                               component of dispersivity tensor
  D_1
                               diameter of large capillary
  D_{n}
                               neck diameter

D_{p}

\overline{D}_{p}

\overline{D}_{p2}

                               particle diameter
                               effective average particle diameter
                               surface average sphere diameter
                               average particle diameter by weight
                           \equiv \int_{0}^{\infty} D_{p} D_{p}^{r} N(D_{p}) dD_{p} / \int_{0}^{\infty} D_{p}^{r} N(D_{p}) dD_{p}
 \bar{D}_{pr}
 D_{p50}
                               median particle diameter by weight
 D_{\rm s}
                               diameter of narrow capillary; equivalent surface diameter [Eq. (3.2.2)]
 D_{\mathsf{T}}
                               container diameter
 D_{v}
                              equivalent volume diameter [Eq. (4.2.12)]; volume average diameter of
                               periodically constricted capillary
 D_{v}^{*}
 D_2
                              length of longest intercept with three-dimensional object
 D_3
                              equivalent spherical void diameter [Eq. (3.2.51)]
 D'
                              coefficient of hydrodynamic dispersion
 D_{\rm L}'
                              dispersion coefficient in the direction of flow
                              dispersion coefficient in the transverse direction
                              hydrodynamic dispersion tensor
 \mathcal{D}_{AB}
                           \equiv \mathscr{D} = \text{molecular diffusion coefficient}
\mathcal{D}_{KA}
                              Knudsen diffusion coefficient of A
 \mathscr{D}_{\mathfrak{m}}
                              moisture diffusivity
 D
                          \equiv (1/\bar{D}_e) - (1/\bar{D}) = "structural difficulty index"
 E
                              modulus of elasticity; effective viscosity ratio [Eq. (7.3.110)]
E_{\rm D}
                              efficiency of conversion of work to creation of surface
                              separation in reverse osmosis [Eq. (5.7.10)]
f<sub>φ</sub>
f(A, 1, α)
f<sub>a</sub>
f<sub>p</sub>
f<sub>r</sub>
f<sub>r</sub>
f<sub>w</sub>
f<sub>w</sub>
                              friction factor of non-Newtonian fluid [Eq. (4.7.9)]
                              probability density of A, l, and α
                          \equiv N_{\rm d} f_2(\phi) [Eqs. (4.3.31) and (4.3.32)]
                             friction factor in porous media
                             relative frequency of pores (capillaries) of type r
                             friction factor [Eq. (4.4.3)]
                             fractional flow function [Eq. (6.4.43)]
f(\phi)
                             porosity function
f(k)
                             probability density of k
f(R)
                             probability density distribution of pore volume by pore radius
                             formation or resistivity factor; bulk flow portion of molar flux
F_{\rm e}
                             effective formation factor at partial saturation
F_{\mathbf{w}}
                          \equiv |Q_{\mathbf{w}}/Q_{\mathbf{T}}| = \text{fractional flow}
F(D_2)
                             probability density function of number of objects of diameter D<sub>2</sub>
F(t)
                             effect of surface forces of pore walls on thermodynamic potential of
                             adsorbed multilayer
F(\tau_{\phi})
                          \equiv 2v/\phi D_{\rm H} [{\rm Eq.} (4.7.2)]
F(\tau_{\mathbf{w}})
                         \equiv 2v/D [Eq. (4.7.1)]
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g		acceleration due to gravity
$g(r^*)$		probability density of r*
$g(\delta; \theta, \phi, \Omega, D_2)$		shape function, i.e., relationship between distance z, measured from the
		plane section characterized by $\delta_{\rm max}$, and δ for various orientations
		(θ, ϕ, Ω) of an object of diameter D_2
$\bar{g}(\delta)$		shape function averaged over all orientations of object
G		Gibbs free energy; genus; molar flow rate
G_{m}		mass flow rate
h		height (measured upward); pressure head; half-width of channel
h_c	=	$\psi \equiv -(P_{\rm w}/\rho_{\rm w}g) = { m capillary \ pressure \ head \ or \ moisture \ tension \ or \ suc-$
		tion head
Н		heterogeneity factor
\overline{H}		mean tangent height or mean caliper diameter
I	=	$F_{\rm e}/F$ = resistivity index
$J(S_{\mathbf{w}})$		Leverett J function
$\vec{J_i^{\rm v}}$		mass flux of i with respect to volume average velocity
k		specific permeability or "permeability"
k'		Kozeny constant
\bar{k}		permeability tensor
k _{CK}		permeability defined by Eq. (4.2.9)
$k_{\rm D}$		permeability used in gas permeametry [Eq. (4.6.3)]
	=	$\mathcal{D}_{\text{eff}} = \text{diffusive permeability coefficient}$
k_{ei}		effective permeability of i
$k_{\tau i}$		relative permeability of i
k _H		hydraulic conductivity
 k _M	=	$\mathscr{D}K_{\mathbf{H}}$ = permeability coefficient used with membranes
k_{ij}		component of permeability tensor
k'_n, k''_n		directional permeabilities
k_0		shape factor; permeability of infinitely dilute bed
k_{1}, k_{2}, k_{3}		"principal" permeabilities
k_1, k_2, k_3, k_4, k_5		constant parameters
k		"pure water permeability constant" [Eq. (5.7.15)]
k	=	$\mathcal{D}/l = \text{mass transfer coefficient}$
K		numerical constant; K factor [Eq. (7.3.10)]
$K_{\mathbf{H}}$		Henry's law constant
1		length; length of capillary; length of a straight line; length of a step in
		random walk; directional cosine of channel axis
l_{ij}		cumulative length of segments of diameter D_i in cell i
l_1		length of a large capillary
$l_{\rm s}$		length of a narrow capillary
<i>l</i> *	=	l/L = dimensionless ratio
L		length of sample; chord or intercept length; greatest pore length in sample
L_{A}		length of chords in a plane per unit test area
.,		average effective path length of fluid
L_{e}		mixing length
$L_{\rm m}$	_	$DL_{\rm m}/2R^2u_{\rm m} = {\rm dimensionless\ mixing\ length}$
L_{m}'	_	lineal fraction of chords contained within two-dimensional features in
$L_{\mathtt{L}}$		the section plane
ı		length of chords in space per unit test volume
$L_{\mathbf{v}}$		length of chords in space per unit test volume

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L(R)	probability density of total length of pores of radius R in the sample
\bar{L}_3	$\equiv 4V/S = \text{mean intercept length}$
$(L_3)_i$	chord length from a random penetration of a three-dimensional object
	by a straight test line
m	mass; cementation exponent; mobility ratio = $k_{2r}\mu_1/k_{1r}\mu_2$
M	molecular weight; Mach number
$M(\phi)$	"effective viscosity" [Eq. (4.5.3)]
n	number of parallel lines crossing unit area; number of moles; number
	of nodes; total number of pores in model; mass flux w.r.t. stationary
	coordinates; adjustable parameter; number of steps taken; number
	of particles per unit volume
n_i	number of repeating capillary units in cell i
n	outward unit normal vector; unit vector
n(D)	photomicrographically determined probability density of pore sizes
	expressed as equivalent sphere diameters
$n(D_p)$	probability density of particle diameters
n'(D)	photomicrographically determined probability density of pore sizes
	expressed as equivalent cylinder diameters
n(L)	probability density of chord length L per unit area of test section
$n(\delta)$	probability density of two-dimensional features of size δ per unit area
	of plane section
N	Avogadro number; index denoting mixing cell; number of intervals;
	rate of transport [Eq. (5.2.14)]
$N_{\mathbf{A}}$	number of two-dimensional features per unit area of section plane;
	molar diffusion flux of A
$N_{\mathbf{B}}$	molar diffusion flux of B
-	
N_{Ca}	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma =$ "capillary number"
N_{Ca} N_{AS}	$\equiv \mu_{\rm w} v_{\rm w} / \phi \sigma =$ "capillary number" diffusion flux of A based on cross section of sample
N_{Ca} N_{AS} N_{d}	$\equiv \mu_{\rm w} v_{\rm w} / \phi \sigma =$ "capillary number" diffusion flux of A based on cross section of sample "deflection number"
N_{Ca} N_{AS} N_{d} N_{e}	$\equiv \mu_{\rm w} v_{\rm w}/\phi \sigma =$ "capillary number" diffusion flux of A based on cross section of sample "deflection number" effective pore number
N_{Ca} N_{AS} N_{d} N_{e} N_{j}	$\equiv \mu_{\rm w} v_{\rm w}/\phi \sigma =$ "capillary number" diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j
N_{Ca} N_{AS} N_{d} N_{e} N_{j} N_{p}	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma =$ "capillary number" diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter
N_{Ca} N_{AS} N_{d} N_{e} N_{j}	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma =$ "capillary number" diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the
N_{Ca} N_{AS} N_{d} N_{e} N_{j} N_{p} N_{L}	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma =$ "capillary number" diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section
N_{Ca} N_{AS} N_{d} N_{e} N_{j} N_{p} N_{L}	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma = \text{``capillary number''}$ diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section $\equiv \text{Re}_{\mathbf{p}}/(1-\phi) = \text{Reynolds number}$
N_{Ca} N_{AS} N_{d} N_{e} N_{j} N_{p} N_{L} N_{Re}	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma = \text{``capillary number''}$ diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section $\equiv \text{Re}_{\mathbf{p}}/(1-\phi) = \text{Reynolds number}$ Reynolds number for non-Newtonian fluids [Eq. (4.7.11)]
N_{Ca} N_{AS} N_{d} N_{e} N_{j} N_{p} N_{L} N_{Re} N_{Ke} N_{S}	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma = \text{``capillary number''}$ diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section $\equiv \text{Re}_{\mathbf{p}}/(1-\phi) = \text{Reynolds number}$ Reynolds number for non-Newtonian fluids [Eq. (4.7.11)] number of spheres per unit volume of bed
N_{Ca} N_{AS} N_{d} N_{e} N_{j} N_{p} N_{L} N_{Re} N_{Ke} N_{SAA}	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma = \text{``capillary number''}$ diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section $\equiv \text{Re}_{\mathbf{p}}/(1-\phi) = \text{Reynolds number}$ Reynolds number for non-Newtonian fluids [Eq. (4.7.11)] number of spheres per unit volume of bed "tertiary oil recovery number" [Eq. (6.4.64)]
N_{Ca} N_{AS} N_{d} N_{e} N_{j} N_{p} N_{L} N_{Re} N_{Ke} N_{SAA} N_{T}	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma = \text{``capillary number''}$ diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section $\equiv \text{Re}_{\mathbf{p}}/(1-\phi) = \text{Reynolds number}$ Reynolds number for non-Newtonian fluids [Eq. (4.7.11)] number of spheres per unit volume of bed "tertiary oil recovery number" [Eq. (6.4.64)] total molar flux
N_{Ca} N_{AS} N_{d} N_{e} N_{j} N_{p} N_{L} N_{Re} N_{Ke} N_{SAA}	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma = \text{``capillary number''}$ diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section $\equiv \text{Re}_{\mathbf{p}}/(1-\phi) = \text{Reynolds number}$ Reynolds number for non-Newtonian fluids [Eq. (4.7.11)] number of spheres per unit volume of bed "tertiary oil recovery number" [Eq. (6.4.64)] total molar flux number of three-dimensional objects per unit test volume; volume flux
$\begin{array}{c} N_{\rm Ca} \\ N_{\rm AS} \\ N_{\rm d} \\ N_{\rm e} \\ N_{\rm j} \\ N_{\rm p} \\ N_{\rm L} \\ \\ N_{\rm Re} \\ N_{\rm Ke} \\ N_{\rm S} \\ N_{\rm SAA} \\ N_{\rm T} \\ N_{\rm v} \end{array}$	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma = \text{``capillary number''}$ diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section $\equiv \text{Re}_p / (1 - \phi) = \text{Reynolds number}$ Reynolds number for non-Newtonian fluids [Eq. (4.7.11)] number of spheres per unit volume of bed "tertiary oil recovery number" [Eq. (6.4.64)] total molar flux number of three-dimensional objects per unit test volume; volume flux relative to membrane [Eq. (5.2.1)]
$\begin{array}{l} N_{Ca} \\ N_{AS} \\ N_{d} \\ N_{e} \\ N_{j} \\ N_{p} \\ N_{L} \\ \\ N_{Re} \\ N_{Ke} \\ N_{S} \\ N_{SAA} \\ N_{T} \\ N_{v} \\ \\ N(D) \end{array}$	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma = \text{``capillary number''}$ diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section $\equiv \text{Re}_{\mathbf{p}}/(1-\phi) = \text{Reynolds number}$ Reynolds number for non-Newtonian fluids [Eq. (4.7.11)] number of spheres per unit volume of bed "tertiary oil recovery number" [Eq. (6.4.64)] total molar flux number of three-dimensional objects per unit test volume; volume flux relative to membrane [Eq. (5.2.1)] $\equiv N(D_{\mathbf{p}}) = \text{probability density of sphere or particle diameters}$
$\begin{array}{c} N_{\rm Ca} \\ N_{\rm AS} \\ N_{\rm d} \\ N_{\rm e} \\ N_{\rm j} \\ N_{\rm p} \\ N_{\rm L} \\ \\ N_{\rm Re} \\ N_{\rm Ke} \\ N_{\rm S} \\ N_{\rm SAA} \\ N_{\rm T} \\ N_{\rm v} \end{array}$	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma = \text{``capillary number''}$ diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section $\equiv \text{Re}_{\mathbf{p}}/(1-\phi) = \text{Reynolds number}$ Reynolds number for non-Newtonian fluids [Eq. (4.7.11)] number of spheres per unit volume of bed "tertiary oil recovery number" [Eq. (6.4.64)] total molar flux number of three-dimensional objects per unit test volume; volume flux relative to membrane [Eq. (5.2.1)] $\equiv N(D_{\mathbf{p}}) = \text{probability density of sphere or particle diameters}$ photomicrographically determined fraction of pores with diameters
$\begin{array}{l} N_{Ca} \\ N_{AS} \\ N_{d} \\ N_{e} \\ N_{j} \\ N_{p} \\ N_{L} \\ \\ N_{Re} \\ N_{Ke} \\ N_{S} \\ N_{SAA} \\ N_{T} \\ N_{v} \\ \\ N(D) \\ N(D_{k}) \end{array}$	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma = \text{``capillary number''}$ diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section $\equiv \text{Re}_{\mathbf{p}}/(1-\phi) = \text{Reynolds number}$ Reynolds number for non-Newtonian fluids [Eq. (4.7.11)] number of spheres per unit volume of bed "tertiary oil recovery number" [Eq. (6.4.64)] total molar flux number of three-dimensional objects per unit test volume; volume flux relative to membrane [Eq. (5.2.1)] $\equiv N(D_{\mathbf{p}}) = \text{probability density of sphere or particle diameters}$ photomicrographically determined fraction of pores with diameters $D \geq D_k$
N_{Ca} N_{AS} N_{d} N_{e} N_{j} N_{p} N_{L} N_{Re} N'_{Ke} N_{S} N_{SAA} N_{T} N_{v} $N(D)$ $N(D_{k})$	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma = \text{``capillary number''}$ diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section $\equiv \text{Re}_p / (1 - \phi) = \text{Reynolds number}$ Reynolds number for non-Newtonian fluids [Eq. (4.7.11)] number of spheres per unit volume of bed "tertiary oil recovery number" [Eq. (6.4.64)] total molar flux number of three-dimensional objects per unit test volume; volume flux relative to membrane [Eq. (5.2.1)] $\equiv N(D_p) = \text{probability density of sphere or particle diameters}$ photomicrographically determined fraction of pores with diameters $D \geq D_k$ probability; probability density of tube radius distribution
$\begin{array}{l} N_{Ca} \\ N_{AS} \\ N_{d} \\ N_{e} \\ N_{j} \\ N_{p} \\ N_{L} \\ \\ N_{Re} \\ N_{Ke} \\ N_{S} \\ N_{SAA} \\ N_{T} \\ N_{v} \\ \\ N(D) \\ N(D_{k}) \\ \\ p \\ \tilde{p} \end{array}$	$\equiv \mu_{\mathbf{w}} v_{\mathbf{w}} / \phi \sigma = \text{``capillary number''}$ diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section $\equiv \operatorname{Re}_p/(1-\phi) = \operatorname{Reynolds number}$ Reynolds number for non-Newtonian fluids [Eq. (4.7.11)] number of spheres per unit volume of bed "tertiary oil recovery number" [Eq. (6.4.64)] total molar flux number of three-dimensional objects per unit test volume; volume flux relative to membrane [Eq. (5.2.1)] $\equiv N(D_p) = \operatorname{probability density of sphere or particle diameters}$ photomicrographically determined fraction of pores with diameters $D \geq D_k$ probability; probability density of tube radius distribution random variable [Eq. (7.3.58)]
N_{Ca} N_{AS} N_{d} N_{e} N_{j} N_{p} N_{L} N_{Re} N'_{Ke} N_{S} N_{SAA} N_{T} N_{v} $N(D)$ $N(D_{k})$	≡ $\mu_{\mathbf{w}}v_{\mathbf{w}}/\phi\sigma$ = "capillary number" diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section ≡ $\mathrm{Re_p}/(1-\phi)$ = Reynolds number Reynolds number for non-Newtonian fluids [Eq. (4.7.11)] number of spheres per unit volume of bed "tertiary oil recovery number" [Eq. (6.4.64)] total molar flux number of three-dimensional objects per unit test volume; volume flux relative to membrane [Eq. (5.2.1)] ≡ $N(D_p)$ = probability density of sphere or particle diameters photomicrographically determined fraction of pores with diameters $D \ge D_k$ probability; probability density of tube radius distribution random variable [Eq. (7.3.58)] fraction of capillaries with diameters $D \ge D_k$ in network model, i.e.,
$\begin{array}{l} N_{Ca} \\ N_{AS} \\ N_{d} \\ N_{e} \\ N_{j} \\ N_{p} \\ N_{L} \\ \\ N_{Re} \\ N_{Ke} \\ N_{S} \\ N_{SAA} \\ N_{T} \\ N_{v} \\ \\ N(D) \\ N(D_{k}) \\ \\ p \\ \tilde{p} \end{array}$	≡ $\mu_{\mathbf{w}}v_{\mathbf{w}}/\phi\sigma$ = "capillary number" diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section $ = \mathbf{Re_p}/(1-\phi) = \mathbf{Reynolds} \text{ number} $ Reynolds number for non-Newtonian fluids [Eq. (4.7.11)] number of spheres per unit volume of bed "tertiary oil recovery number" [Eq. (6.4.64)] total molar flux number of three-dimensional objects per unit test volume; volume flux relative to membrane [Eq. (5.2.1)] $ = N(D_p) = \text{probability density of sphere or particle diameters } D \ge D_k $ probability; probability density of tube radius distribution random variable [Eq. (7.3.58)] fraction of capillaries with diameters $D \ge D_k$ in network model, i.e., probability that a randomly chosen capillary will have diameter greater
$\begin{array}{l} N_{Ca} \\ N_{AS} \\ N_{d} \\ N_{e} \\ N_{j} \\ N_{p} \\ N_{L} \\ \\ N_{Re} \\ N_{Ke} \\ N_{S} \\ N_{SAA} \\ N_{T} \\ N_{v} \\ \\ N(D) \\ N(D_{k}) \\ \\ p \\ \tilde{p} \end{array}$	≡ $\mu_{\mathbf{w}}v_{\mathbf{w}}/\phi\sigma$ = "capillary number" diffusion flux of A based on cross section of sample "deflection number" effective pore number number of capillaries of size j number of pores per unit section of filter number of interceptions of features per unit length of test line in the plane of section ≡ $\mathrm{Re_p}/(1-\phi)$ = Reynolds number Reynolds number for non-Newtonian fluids [Eq. (4.7.11)] number of spheres per unit volume of bed "tertiary oil recovery number" [Eq. (6.4.64)] total molar flux number of three-dimensional objects per unit test volume; volume flux relative to membrane [Eq. (5.2.1)] ≡ $N(D_p)$ = probability density of sphere or particle diameters photomicrographically determined fraction of pores with diameters $D \ge D_k$ probability; probability density of tube radius distribution random variable [Eq. (7.3.58)] fraction of capillaries with diameters $D \ge D_k$ in network model, i.e.,

$p(u, t/u_0, t_0)$	probability that a molecule has a velocity u at time t , if it had a velocity
	u_0 at time t_0
P	hydrostatic pressure; fraction of pore space which is accessible through
	pores with diameters less than or equal to a given value
Pe	$\equiv \tilde{v}_{p} \overline{D}_{p} / D = \text{Peclet number}$
Pe'	$\equiv \bar{v}_p \bar{D}_p / D' = \text{dynamic Peclet number}$
Pe_{ct}	Peclet number in a capillary [Eqs. (7.2.6) and (7.2.7)]
Pe _{fT}	Peclet number [Eq. (7.3.55)]
$P_{\rm c}$	capillary pressure
P_{cb}	breakthrough capillary pressure or bubbling pressure
P'_{cb}	$\equiv P_{\rm cb}/4\sigma\cos\theta = { m reduced}$ breakthrough capillary
$P_{\rm m}$	arithmetic mean pressure
P_0	vapor pressure over plane surface; hydrostatic pressure at the datum
* 0	level
P_{p}	$\equiv P_o/P_T$ = fractional point count
P*	$\equiv 1/r^*$ = dimensionless capillary pressure
P'' _r	vapor pressure over hemispherical meniscus of radius of curvature r
<i>p</i> *	$\equiv \mathscr{P}/\rho v^2 \text{ or } \equiv \mathscr{P}/\rho v_0^2 = \text{dimensionless group}$
<i>P'</i>	absolute value of the macroscopic pressure gradient
$P_{\mathbf{A}}$	number of points (intersections) generated per unit area of section plane
1 A	with lines in space
$P_{ m L}$	number of points (intersections) generated per unit length of test line
L	with traces of surfaces in the section plane
D	total number of grid points
$P_{\mathbf{T}}$	number of points of intersection between surfaces and lines per unit test
$P_{\mathbf{V}}$	volume
P_{α}	number of grid points falling over phase α
P P	piezometric pressure
_	probability that a randomly chosen pore will not exceed a given size, i.e.,
q	number fraction of pores smaller than a given size; volume flow in a tube;
	$\equiv l/t \text{ (velocity of particle along a step)}$
a	ith size distribution parameter
q_i	fraction of "pseudo-dead-end capillaries" in network model when D_k is
q_k	the diameter of the smallest penetrated capillary
-(D D()	probability density of volume flow rates [Eq. (4.3.15)]
$q(D_{\rm e},D_{\rm e}')$	volume flow rate or discharge
Q	radial coordinate or distance; radius of capillary or pore; number of
r	dimensions used in averaging particle diameters; rate of production;
	ratio of true to apparent surface area; dimensionless distance between
	centers of spheres
	mean radius of curvature
$r_{\rm m}$	hydraulic radius
<i>r</i> _H →	
r*	$\equiv r/R$ = dimensionless ratio principal radii of curvature of surface, inner and outer radius of rotation,
r_1, r_2	respectively; smallest and largest radius, respectively, or periodically
	constricted tube
$rD_{\mathbf{p}}$	interparticle distance
r(c, t)	rate of production per unit volume of solution
R	resistivity; greatest pore radius in sample; radius of capillary or grain;
	electrical resistance of network; universal gas constant

```
R
                          force resisting motion [Eq. (4.9.29)]
R_{\rm p}
                          cumulative oil recovery in pore volume units
Re
                       \equiv \rho v \sqrt{k/\mu} = \text{Reynold's number}
Re"
                       \equiv \beta \rho v / \alpha \mu = \text{Reynolds number}
                       \equiv D_{\rm f} v_{\rm p} \rho / \mu = \text{Reynolds number}
Re<sub>c</sub>
                       \equiv D_{\rm f} v \rho / \mu = "superficial" Reynolds number for fibrous beds
Ref
                       \equiv v_{\rm DF} \sqrt{k}/v = \text{Reynolds number}
Re
                       \equiv D_{p}v\rho/\mu = "superficial" or "particle" Reynolds number
Re<sub>p</sub>
                       \equiv D_{\rm v}v_{\rm m}/v = {\rm Reynolds\ number}
Re<sub>v</sub>
Re,
                       \equiv \lambda v_0/v = \text{Reynolds number}
                       \equiv D_{p50}v_{DF}/v = \text{Reynolds number}
Reso
                          radius defined by Eq. (3.2.10)
R,
                          resistivity of saturated sample
R_{\rm o}
R_w
                          resistivity of electrolyte solution
R_{i}
                          constriction radius
                          bulge radius
R_2
R_1, R_2
                          radii of curvature of surface
R_1^*
                       \equiv R_1/\lambda
R_2^*
                       \equiv R_2/\lambda
                          length measured along axis of channel
S
                          photomicrographically determined volume fraction of capillaries of
s_i
                          diameter D_i
S
                          spreading coefficient; saturation; surface; specific surface per unit mass
                          of sample; standard deviation
Sc
                       \equiv v/D = Schmidt number
S_i
                          fraction of pore volume occupied by capillaries in cell i; saturation of
                          saturation with respect to a nonwetting phase, predicted by network
S_{k}
                          analysis, when D_k is the diameter of the smallest penetrated capillary
S_0
                          specific surface per unit volume of solids
                          particle surface area; pore surface area
                          specific surface area based on Eq. (3.2.20)
                          surface area contained in unit test volume or surface area per unit bulk
                          volume
S_{\text{BET}}
                          specific surface area based on BET method
                          "constrictedness factor" [Eq. (4.9.25)]
S(D_k)
                          photomicrographically determined volume fraction of pores with diam-
                          eters D \ge D_k (cumulative pore size distribution)
                          time: multilayer thickness; duration of a step in random walk
T
                          absolute temperature; "tortuosity"; time it takes to collect one pore
                          volume of effluent; length of a time interval
T'. T''
                          correction factors
                          "tortuosity tensors"
\mathcal{F}_{ij} and \mathcal{F}_{ij}
                          r velocity component of microscopic point velocity
                          z velocity component of microscopic point velocity
u_z
                          microscopic point velocity
u*
                       \equiv u/v = \text{dimensionless velocity}
и,*
                       \equiv u_r/v_0, or \equiv u_r/v = dimensionless velocity component
                       \equiv u_z/v_0 = dimensionless velocity component
u*
U
                          velocity component of a marked particle relative to coordinate axes
                          moving with the mean velocity [Eq. (7.3.75)]
                       \equiv (\delta Q/\delta A)\mathbf{n} = filter velocity; specific discharge or superficial velocity
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List of Symbols xvii

	AQUID?
$v_{\mathbf{m}}$	$\equiv 4Q/\pi D_{\rm v}^2 = \text{volumetric mean velocity}$
v_0	mean velocity at the entrance of a periodically constricted tube
$v_{\mathbf{p}}$	"pore velocity" [Eqs. (4.3.14) or (4.3.24)]
$v_{\mathtt{pn}}$	pore velocity in a pore parallel to macroscopic pressure gradient
$v_{ m DF}$	$\equiv v/\phi$ = average pore velocity according to Dupuit-Forchheimer assump-
	tion
$ar{v}$	mean molecular speed
$v_{\mathbf{D}}$	random part of velocity due to dispersion process
$ar{v}_{\mathtt{p}}$	average pore velocity; interstitial velocity or "seepage" velocity
v*	mass-averaged velocity [Eq. (4.9.29)]
v ^v	$\equiv v_{DF} = volume$ average velocity of mixture with respect to the solid
	matrix
V	volume; volume of vapor adsorbed; velocity component of marked
	particle in the transverse direction
$V_{\mathtt{a}}$	adsorbed volume of adsorbate as ATP gas per gram of adsorbent
V_{f}	fluid volume
$V_{ m m}$	STP volume of gas adsorbed at complete monolayer point
V_0	STP number (22.414 liters)
$V_{ m p}$	particle volume; pore volume
$V_{ m s}$	volume of absorbate at saturation vapor pressure
$V_{\mathbf{v}}$	fractional volume of a phase
V_{ij}	$\equiv V(D_e, D) \times 100 = \text{percent pore volume contributed by pores of diam-}$
	eter D_j such that they are accessible through pores of diameter D_i
$V_{_{ m B}}$	bulk volume
$V_{\mathbf{T}}$	total pore volume
V(D)	volume of a capillary (pore) characterized by diameter D
$V(D_e, D)$	probability density of pore volume by pore diameters D_e and D (bivariate
	pore size distribution: BPSD)
V'	molar volume of liquid
V''	molar volume of vapor
V_i	partial molar volume of i
x	x coordinate; mole fraction; dimensionless ratios $\equiv P''/P$; or $\equiv D_1/D_s$
x'	moving x coordinate
X	distance measured from center of a sphere; electrical torguosity factor;
	x coordinate of displacement of a marked particle
y	y coordinate; dimensionless ratios $\equiv v_l/v_s$, or $\equiv l_l/l_s$; mole fraction in
	gas phase
y_k	number-based saturation with respect to nonwetting phase capillaries in
	network such that $D > D_k$, when D_k is the smallest penetrated capillary
	diameter
Y	y coordinate of displacement of marked particle
Y_k	number-based saturation of network with respect to wetting phase when
	D_k is smallest penetrated capillary diameter
z	z coordinate; distance measured vertically upward; $\equiv g(\delta; \theta, \phi, \Omega, D_2)$
\boldsymbol{Z}	coordination number; z coordinate of displacement of marked particle

Greek Letters

α	angle; reciprocal of "permeability"; $\equiv 1 + N_B/N_A$
$\alpha(D)$	probability density function of pore volume by pore diameters according
	to the bundle of capillary tubes model

$\alpha(D_e)$	probability density function of pore volume by pore entry diameters
α	orientation vector
$\alpha(t; D)$	probability density of number of chords obtained by intercepting spheres
o.	of diameter D per unit length of test line
β	layer spacing parameter; angle; "inertia parameter"; parameter of
	second-order memory fluid; constant parameter; inverse compaction
$\beta D_{_{\mathbf{p}}}$	factor [Eq. (5.1.4)]
βD_{p} $\beta(\delta; D)$	layer spacing
p(v, D)	probability density of number of circle diameters δ per unit area of plane of section obtained by intersecting spheres of diameter D
$\beta(\delta; D_2)$	probability density of number of features of size δ per unit area of sec-
p(+, -2)	tioning plane, obtained by intersecting objects of diameter D_2
γ	ratio of specific heats; constant parameter
$\stackrel{\prime}{\Delta}$	difference of two quantities
δ	Dirac delta function; circle diameter; longest intercept with two-dimen-
	sional feature in the y direction
\mathfrak{F}	$\equiv \overline{R}/\overline{l}$ = ratio of average channel radius to average channel length
$arepsilon_i$	$\equiv (v_{\rm DF})_i / v_{\rm DF} [\rm Eq. (7.3.107)]$
heta	contact angle; polar angle; dip angle
κ	$\equiv R_0/R_i = \text{dimensionless ratio}$
λ	mean-free path; "wave length" of periodically constricted tube; constant
	parameter; "pore size distribution index" [Eq. (6.3.13)]
Λ	characteristic length
μ	chemical potential; viscosity
μ_{jk}	number of capillaries of diameter D_j penetrated in the network by the
	nonwetting phase when D_k is the diameter of the smallest penetrated
	capillary
μ_{ϕ}	Darcy viscosity kinematic viscosity
$v_{\rm l}$	number of large capillaries
v _p	number of pore volumes
v _s	number of pore volumes
v _{jk}	number of "pseudo dead-end capillaries" of diameter D_j when D_k is the
<i>J</i> *	diameter of the smallest penetrated capillaries
ξ	constant parameter
ξ_i	statistical weight; local coordinates
π	$\equiv \sigma/\mu v = \text{dimensionless group}; \text{ osmotic pressure}$
ho	radius; density; electrical resistance of individual resistor
γ	angle; constant parameter [Eq. (4.4.15)]; $\equiv b/a = \text{dimensionless ratio}$
$\gamma(D_{\mathbf{e}})$	probability density function of pore entry diameters
Γ	shear rate
$(\Sigma m)_r$	number of pores connected to a pore of type r
σ	surface tension; standard deviation; length along streamline; retention
•	[Eq. (5.1.1)]
σ^0	area of a molecular site
τ	$\equiv tD/R^2$ = dimensionless time; shear stress; tortuosity vector; $\equiv V/Q$ =
	residence time
τ.,	wall shear stress in capillary
τ_{ϕ}	wall shear stress in packed bed

List of Symbols xix

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φ
                          porosity; angle: azimuthal angle; half-angle of cone; piezometric head;
                          volume fraction
                       \equiv z + \frac{P_{\rm w}}{o...a} \equiv z - h_{\rm c} = {\rm capillary\ head}
\phi_{c}
\phi_{\mathrm{e}}
                         effective porosity [Eq. (4.2.23)]
\phi_0
                          overall porosity corresponding to a given D_p/D_T
\phi_{\rm s}
                          "sphericity," i.e., the ratio of surface area of the hypothetical sphere of
                          the same volume as the particle to the actual surface area of the particle
φ′
                          local porosity
\bar{\phi}
                         local mean porosity relative to a reference point or plane
                         local area porosity
                         capillary pressure head; arbitrary point function; "viscosity level
                         parameter"
\psi_i
                         ith particle shape parameter
Ω
                         angle of rotation about an axis
ω
                         angular velocity
η
                         apparent viscosity of non-Newtonian fluid in "Poiseuille flow" [Eq.
                         (4.7.8)]; collection efficiency of an individual fiber [Eq. (5.1.9)]
\eta_{\phi}
                         "Darcy viscosity" of non-Newtonian fluid [Eq. (4.7.9)]
```

Subscripts

a apparent; air; adsorbate; adsorption brance A advancing h breakthrough; bulge В bulk BET refers to Brunauer, Emmet, and Teller capillary ct capillary tube c, cr critical d desorption branch e entry; equilibrium eff effective f front

g gas
h hysteresis function (= functional)
i irreducible; inner; initial
i refers to cell i; refers to capillary i
f refers to capillary j

k refers to smallest penetrated capillary

liquidlongitudinal

m mean value; monolayer; molar

max maximum min minimum mt multilayer

n neck; narrow, smallest pore or capillary

nwr residual nonwetting phase

nw nonwetting

o saturated; initial; outer

p pore

P constant pressure

r residual
r r type of pore
R receding

s solid; saturation; solvent

s.s. steady state

t refers to t curve

T transverse; total; constant temperature

v vapor

w wetting; water; wide electrolyte solution

 w
 electrolyte solution

 wi
 irreducible water

 x
 x component

Superscripts and Overlines

reduced; on the convex side of interface; moving coordinate; distin-

guished mark

refers to tracer

on the concave side of the interface

positive direction from the xy plane
reduced macroscopic variable
negative direction from xy plane

= tensor

-- ensemble average

i "in" o "out"

Special Symbols

∇ "del" or "nabla" operator

 ∇^* $D\nabla$

 ∇^{*^2} $D^2\nabla^2$

 δ denotes a small quantity