Mandbook[®]
Ninth Edition
Volume 15
Casting

Metals Handbook[®] Ninth Edition

Volume 15 Casting

Prepared under the direction of the ASM INTERNATIONAL Handbook Committee

D.M. Stefanescu, Chairman

Joseph R. Davis, Senior Editor
James D. Destefani, Technical Editor
Theodore B. Zorc, Technical Editor
Heather J. Frissell, Editorial Supervisor
George M. Crankovic, Assistant Editor
Alice W. Ronke, Assistant Editor
Diane M. Jenkins, Word Processing Specialist
Karen Lynn O'Keefe, Word Processing Specialist

Robert L. Stedfeld, Director of Reference Publications Kathleen M. Mills, Manager of Editorial Operations

> Editorial Assistance Lois A. Abel Robert T. Kiepura Penelope Thomas Nikki D. Wheaton



Copyright © 1988 by ASM INTERNATIONAL All rights reserved

No part of this book may be reproduced, stored in a retrieval system, or transmitted, in any form or by any means, electronic, mechanical, photocopying, recording, or otherwise, without the written permission of the copyright owner.

First printing, September 1988

Metals Handbook is a collective effort involving thousands of technical specialists. It brings together in one book a wealth of information from world-wide sources to help scientists, engineers, and technicians solve current and long-range problems.

Great care is taken in the compilation and production of this volume, but it should be made clear that no warranties, express or implied, are given in connection with the accuracy or completeness of this publication, and no responsibility can be taken for any claims that may arise.

Nothing contained in the Metals Handbook shall be construed as a grant of any right of manufacture, sale, use, or reproduction, in connection with any method, process, apparatus, product, composition, or system, whether or not covered by letters patent, copyright, or trademark, and nothing contained in the Metals Handbook shall be construed as a defense against any alleged infringement of letters patent, copyright, or trademark, or as a defense against liability for such infringement.

Comments, criticisms, and suggestions are invited, and should be forwarded to ASM INTERNATIONAL.

Library of Congress Cataloging-in-Publication Data

ASM INTERNATIONAL

Metals handbook.

Includes bibliographies and indexes.

Contents: v. 1. Properties and selection—[etc.]—
v. 13 Corrosion—[etc.]—
v. 15. Casting.

I. Metals—Handbooks, manuals, etc. I. ASM INTERNATIONAL. Handbook Committee. TA459.M43 1978 669 78-14934 ISBN 0-87170-007-7 (v. 1) SAN 204-7586

Printed in the United States of America

Foreword

The subject of metal casting was covered--along with forging--in Volume 5 of the 8th Edition of Metals Handbook. Volume 15 of the 9th Edition, a stand-alone volume on the subject, is evidence of the strong commitment of ASM INTERNATIONAL to

the advancement of casting technology

The decision to devote an entire Handbook to the subject of casting was based on the veritable explosion of improved or entirely new molding, melting, metal treatment, and casting processes that has occurred in the 18 years since the publication of Volume 5. New casting materials, such as cast metal-matrix composites, also have been developed in that time, and computers are being used increasingly by the foundry industry. An entire section of this Handbook is devoted to the application of computers to metal casting, in particular to the study of phenomena associated with the solidification of molten metals.

Coverage of the depth and scope provided in Volume 15 is made possible only by the collective efforts of many individuals. In this case, the effort was an international one, with participants in 12 nations. The driving force behind the entire project was volume chairman Doru M. Stefanescu of the University of Alabama, who along with his section chairmen recruited more than 200 of the leading experts in the world to author articles for this Handbook. We are indebted to all of them, as well as to the members of the ASM Handbook Committee and the Handbook editorial staff. Their hard work and dedication has culminated in the publication of this, the most comprehensive single-volume reference on casting technology yet published.

> William G. Wood President, ASM INTERNATIONAL

> Edward L. Langer Managing Director. **ASM INTERNATIONAL**

The Ninth Edition of Metals Handbook is dedicated to the memory of TAYLOR LYMAN, A.B. (Eng.), S.M., Ph.D. (1917-1973) Editor, Metals Handbook, 1945-1973

Preface

The story of metal casting is as glamorous as it is ancient, beginning with the dawn of human civilization and interwoven with legends of fantastic weapons and exquisite artworks made of precious metals. It was and is involved in the two main activities of humans since they began walking the earth: producing and defending wealth. Civilization as we know it would not have been possible without metal casting. Metal casting must have emerged from the darkness of antiquity first as magic, later to evolve as an art,

then as a technology, and finally as a complex, interdisciplinary science.

As with most other industries, the body of knowledge in metal casting has doubled over the last ten years. A modern text on the subject should discuss not only the new developments in the field but also the applications of some fundamental sciences such as physical chemistry, heat transfer, and fluid flow in metal casting. The task of reviewing such an extensive amount of information and of documenting the knowledge currently involved in the various branches of this manufacturing industry is almost impossible. Nevertheless, this is the goal of this Volume. For such an endeavor to succeed, only one avenue was possible—to involve in the preparation of the manuscripts as well as in the review process the top metal casting engineers and scientists in the international community. Indeed, nearly 350 dedicated experts from industry and academe worldwide contributed to this Handbook. This magnificent pool of talent was instrumental in putting together what I believe to be the most

complete text on metal casting available in the English language today.

The Handbook is structured in ten Sections, along with a Glossary of Terms. The reader is first introduced to the historical development of metal casting, as well as to the advantages of castings over parts produced by other manufacturing processes, their applications, and the current market size of the industry. Then, the thermodynamic relationships and properties of liquid metals and the physical chemistry of gases and impurities in liquid metals are discussed. A rather extensive Section reviews the fundamentals of the science of solidification as applied to cast alloys, including nucleation kinetics, fundamentals of growth, and the more practical subject of interpretation of cooling curves. Traditional subjects such as patterns, molding and casting processes, foundry equipment, and processing and design considerations are extensively covered in the following Sections. Considerable attention has been paid to new and emerging processes, such as the Hitchiner process, directional solidification, squeeze casting, and semisolid metal forming. The metallurgy of ferrous and nonferrous alloys is extensively covered in two separate Sections. Finally, there is detailed information on the most modern approach to metal casting, namely, computer applications. The basic principles of modeling of heat transfer, fluid flow, and microstructural evolution are discussed, and typical examples are given.

It is hoped that the reader can find in this Handbook not only the technical information that he or she may seek, but also the prevailing message that the metal casting industry is mature but not aging. It is part of human civilization and will remain so for centuries to come. Make no mistake. A country cannot hold its own in the international marketplace without a modern, competitive metal casting industry.

It is a great pleasure to acknowledge the collective effort of the many contributors to this Handbook. The chairmen of the ten Sections and the authors of the articles are easily acknowledged, since their names are duly listed throughout the Volume. Less obvious but of tremendous importance in maintaining a uniform, high-quality text is the contribution of the reviewers. The Handbook staff of ASM INTERNATIONAL must also be commended for their dauntless and painstaking efforts in making this Volume not only accurate but also beautiful. Last but not least, I would like to acknowledge the precious assistance of my secretary, Mrs. Donna Snow, who had the patience to cope gracefully with the many tasks involved in such a complex project.

Prof. D.M. Stefanescu Volume Chairman

Officers and Trustees of ASM INTERNATIONAL

William G. Wood
President and Trustee
Kolene Corporation

Richard K. Pitler
Vice President and Trustee
Allegheny Ludlum Corporation
(retired)

Raymond F. Decker
Immediate Past President and Trustee
University Science Partners, Inc.

Frank J. Waldeck
Treasurer
Lindberg Corporation

Trustees

Stephen M. Copley University of Southern California

Herbert S. Kalish
Adamas Carbide Corporation

H. Joseph Klein
Haynes International, Inc.

William P. Koster
Metcut Research Associates, Inc.

Robert E. Luetje Kolene Corporation Gunvant N. Maniar
Carpenter Technology Corporation

Larry A. Morris
Falconbridge Limited

William E. Quist
Boeing Commercial Airplane Company

Daniel S. Zamborsky Aerobraze Corporation

Edward L. Langer Managing Director

Members of the ASM Handbook Committee (1987-1988)

Dennis D. Huffman (Chairman 1986—; Member 1983—) The Timken Company

Roger J. Austin (1984-)
Astro Met Associates, Inc.

Roy G. Baggerly (1987-) Kenworth Truck Company

Peter Beardmore (1986-) Ford Motor Company

Robert D. Caligiuri (1986-)
Failure Analysis Associates

Richard S. Cremisio (1986-) Rescorp International, Inc. Thomas A. Freitag (1985–1988)
The Aerospace Corporation

Charles David Himmelblau (1985–1988) Lockheed Missiles & Space Company, Inc.

J. Ernesto Indacochea (1987-) University of Illinois at Chicago

Ell Levy (1987-)
The De Havilland Aircraft Company
of Canada

Arnold R. Marder (1987-) Lehigh University

L.E. Roy Meade (1986-) Lockheed-Georgia Company Merrill L. Minges (1986–)
Air Force Wright Aeronautical Laboratories

David V. Neff (1986-) Metaullics Systems

David LeRoy Olson (1982-1988) Colorado School of Mines

Ned W. Polan (1987-) Olin Corporation

Paul E. Rempes (1986-) Williams International

E. Scala (1986-) Cortland Cable Company, Inc.

David A. Thomas (1986--) Lehigh University

Previous Chairmen of the ASM Handbook Committee

R.S. Archer (1940–1942) (Member, 1937–1942)

L.B. Case (1931-1933) (Member, 1927-1933)

T.D. Cooper (1984–1986) (Member, 1981–1986)

E.O. Dixon (1952-1954) (Member, 1947-1955)

R.L. Dowdell (1938–1939) (Member, 1935–1939)

J.P. Gill (1937) (Member: 1934-1937)

J.D. Graham (1966-1968) (Member, 1961-1970)

J.F. Harper (1923–1926) (Member, 1923–1926)

C.H. Herty, Jr. (1934–1936) (Member, 1930–1936)

J.B. Johnson (1948–1951) (Member, 1944–1951)

L.J. Korb (1983) (Member, 1978–1983)

R.W.E. Leiter (1962–1963) (Member, 1955–1958, 1960–1964)

G.V. Luerssen (1943–1947) (Member, 1942–1947)

G.N. Maniar (1979–1980) (Member, 1974–1980)

J.L. McCall (1982) (Member, 1977-1982) W.J. Merten (1927-1930) (Member, 1923-1933)

N.E. Promisel (1955–1961) (Member, 1954–1963)

G.J. Shubat (1973–1975) (Member, 1966–1975)

W.A. Stadtler (1969–1972) (Member, 1962–1972)

R. Ward (1976–1978) (Member, 1972–1978)

M.G.H. Wells (1981) (Member, 1976–1981)

D.J. Wright (1964–1965) (Member, 1959–1967)

Policy on Units of Measure

By a resolution of its Board of Trustees, ASM INTERNATION-AL has adopted the practice of publishing data in both metric and customary U.S. units of measure. In preparing this Handbook, the editors have attempted to present data in metric units based primarily on Système International d'Unités (SI), with secondary mention of the corresponding values in customary U.S. units. The decision to use SI as the primary system of units was based on the aforementioned resolution of the Board of Trustees and the widespread use of metric units throughout the world.

For the most part, numerical engineering data in the text and in tables are presented in SI-based units with the customary U.S. equivalents in parentheses (text) or adjoining columns (tables). For example, pressure, stress, and strength are shown both in SI units, which are pascals (Pa) with a suitable prefix, and in customary U.S. units, which are pounds per square inch (psi). To save space, large values of psi have been converted to kips per square inch (ksi), where 1 ksi = 1000 psi. The metric ton (kg \times 10³) has been shown in megagrams (Mg). Some strictly scientific data are presented in SI units only. For example, the solubility of a gas in a metal is given only in milliliters per 100 grams of metal (mL/100 g).

To clarify some illustrations, only one set of units is presented on artwork. References in the accompanying text to data in the illustrations are presented in both SI-based and customary U.S. units. On graphs and charts, grids corresponding to SI-based units appear along the left and bottom edges. Where appropriate, corresponding customary U.S. units appear along the top and right edges.

Data pertaining to a specification published by a specificationwriting group may be given in only the units used in that specification or in dual units, depending on the nature of the data. For example, the typical yield strength of aluminum sheet made to a specification written in customary U.S. units would be presented in dual units, but the sheet thickness specified in that specification might be presented only in inches.

Data obtained according to standardized test methods for which the standard recommends a particular system of units are presented in the units of that system. Wherever feasible, equivalent units are

also presented.

Conversions and rounding have been done in accordance with ASTM Standard E 380, with attention given to the number of significant digits in the original data. For example, an annealing temperature of 1570 °F contains three significant digits. In this case, the equivalent temperature would be given as 855 °C; the exact conversion to 854.44 °C would not be appropriate. For an invariant physical phenomenon that occurs at a precise temperature (such as the melting of pure silver), it would be appropriate to report the temperature as 961.93 °C or 1763.5 °F. In some instances (especially in tables and data compilations), temperature values in °C and °F are alternatives rather than conversions.

The policy on units of measure in this Handbook contains several exceptions to strict conformance to ASTM E 380; in each instance, the exception has been made in an effort to improve the clarity of the Handbook. The most notable exception is the use of g/cm³ rather than kg/m³ as the unit of measure for density (mass per unit volume).

SI practice requires that only one virgule (diagonal) appear in units formed by combination of several basic units. Therefore, all of the units preceding the virgule are in the numerator and all units following the virgule are in the denominator of the expression; no parentheses are required to prevent ambiguity.

Authors and Reviewers

G. J. Abbaschian University of Florida Harvey Abramowitz

Purdue University R. Agarwal

General Motors Technical Center Mark J. Alcini

Williams International

Robert I. Allen Deere & Company Richard L. Anderson

Arnold Engineering Company John Andrews

Camden Castings Center James J. Archibald

Ashland Chemical Company

Shigeo Asai Nagoya University (Japan)

William H. Bailey

Cleveland Pneumatic Company Leo J. Baran

American Foundrymen's Society, Inc. W.J. Barice

Precision Castparts Corporation Charles E. Bates

Southern Research Institute Robert J. Bayuzick

Vanderbilt University

J. Beech University of Sheffield (Great Britain)

V.G. Behal Dofasco Inc. (Canada)

P. Belding Columbia Steel Casting Company

John T. Berry University of Alabama

Leybold AG (West Germany)

Gopal K. Bhat Bhat Technology International, Inc.

Yves Bienvenu Ecole des Mines de Paris (France)

Reynolds Metals Company

Reynolds Aluminum Charles R. Bird

Stainless Steel Foundry & Engineering Inc K.E. Blazek

Inland Steel Company William J. Boettinger

National Bureau of Standards M.A. Bohlmann

I.G. Technologies, Inc. Charles B. Bover

Battelle Columbus Division

Jose R. Branco

Colorado School of Mines

R. Brink

Leybold AG (West Germany)

William Brouse

Carpenter Technology Corporation

Roger B. Brown

Disamatic, Inc. Francis Brozo

Hitchcock Industries, Inc.

Robert S. Buck

International Magnesium Consultants, Inc.

I. Bukowski

General Motors Technical Center

Wilhelm Burgmann

Leybold AG (West Germany)

H.I. Burrier

The Timken Company

Michael Byrne

Homer Research Laboratories

S.L. Camacho

Plasma Energy Corporation Paul G. Campbell

ALUMAX of South Carolina

James A. Capadona Signicast Corporation

C. Carisson Asea Brown Boveri, Inc.

James H. Carpenter Pangborn Corporation

Sam F. Carter Carter Consultants, Inc.

Dixon Chandley Metal Casting Technology, Inc.

K.K. Chawla New Mexico Institute of Technology

Dianne Chong McDonnell Douglas Astronautics

Company A. Choudhury

Leybold AG (West Germany)

Richard J. Choulet

Steelmaking Consultant

Yeou-Li Chu

The Ohio State University

Dwight Clark

Baltimore Specialty Steels

Steve Clark

R.H. Sheppard Company, Inc.

Byron B. Clow

International Magnesium Consultants, Inc.

Arthur Cohen

Copper Development Association, Inc.

B. Cole

Fort Wayne Foundry Corporation

H.H. Cornell

Niobium Products Company, Inc.

James A. Courtois

ALUMAX Engineered Metal Processes. Inc

Jim Cox

Hatch Associates Ltd.

D.B. Craig

Elkem Metals Company

Alan W. Cramb

Carnegie Mellon University

R. Creese

West Virginia University

T.J. Crowley

Microwave Processing Systems

Milford Cunningham

Stahl Specialty Company

Peter A. Curreri

NASA Marshall Space Flight Center

Michael J. Cusick

Colorado School of Mines

Johnathan A. Dantzig

University of Illinois at Urbana-Champaign

C.V. Darragh

The Timken Company

A.S. Davis

ESCO Corporation

Jackson A. Dean

Cardinal Service Company

Prateen V. Desai

Georgia Institute of Technology

B.K. Dhindaw

IIT Kharagpur (India)

W. Dietrich

Leybold AG (West Germany)

George Di Sylvestro

American Colloid Company

R.L. Dobson

The Centrifugal Casting Machine Company

George J. Dooley, III

United States Department of the Interior

J.L. Dorcic

IIT Research Institute

R. Doremus

Rensselaer Polytechnic Institute

G. Doughman

Casting Design and Services

B. Duca

Duca Remanufacturing Inc. I. DuPlessis

Crucible Magnetics Division

F. Durand

Centre National de la Recherche Scientifique

Polytechnique de Grenoble (France)

William B. Elsen Crucible Compaction Metals Nagy El-Kaddah University of Alabama R. Elliott University of Manchester (Great Britain) John M. Eridon Howmet Corporation R.C. Eschenbach Retech, Inc. N. Eustathopoulos Institut National Polytechnique de Grenoble (France) M. Evans Cytemp Specialty Steels Robert D. Evans ALUMAX Engineered Metal Processes, Inc. Daniel Evl vn University of Dayton H.E. Exner Max-Planck-Institut für Metallforschung (West Germany) Gilbert M. Farrior ALUM.\X Engineered Metal Processes, Inc J. Feroe G.H. Hensley Industries Inc. J. Feinman Tech..ical Consultant Merton C. Flemings Massachusetts Institute of Technology S.C. Flood Alcan International Ltd. (Great Britain) Victor K. Forsberg Quancx Robert C Fovle Herman-Sinto V-Process Corporation H. Frederiksson The Royal Institute of Technology (Sweden) Richard J. Fruehan Carnegie Mellon University B. Gabrielsson Elwood Uddeholm Steel Company D.R. Gaskell Purdue University William Gavin Hitchcock Industries, Inc. H. Gave Technical Consultant M. Geiger Asea Brown Boveri, Inc.

L. Gonano

George Good

P. Gouwens

National Forge Company

Ford Motor Company

Taussig Associates, Inc.

Smithsonian Institution

CMI Novacast Inc.

George M. Goodrich

Martha Goodway

J. Grach Cominco Metals L.D. Graham -**PCC Airfoils** E.J. Grandy H. Kramer & Company Douglas A. Granger Alcoa Technical Center C.V. Grosse Howmet Corporation R.E. Grote Missouri Precision Castings Daniel B. Groteke Metcast Associates, Inc. Thomas E. Grubach Aluminum Company of America J.E. Gruzieski McGill University (Canada) Richard B. Gundlach Climax Research Services T.B. Gurganus Alcoa Technical Center Alex M. Gymarty SKW Metals & Alloys, Inc. David Hale Ervin Industries, Inc. T.C. Hansen Trane Company Michael J. Hanslits Precision Castparts Corporation Howard R. Harker A. Johnson Metals Corporation Ron Harrison Cameron Forge Company Richard Helbling Northern Castings H. Henein Carnegie Mellon University D.G. Hennessy The Timken Company John J. Henrich United States Pipe and Foundry Company W. Herman Quanex **Edwin Hodge** Degussa Electronics Inc. D. Hoffman National Forge Company George B. Hood United Technologies Pratt & Whitney M.J. Hornung Elkem Metals Company Robert A. Horton PCC Airfoils, Inc. Daryl F. Hoyt Wedron Silica Company I.C.H. Hughes **BCIRA International Centre for Cast**

James Hunt Southern Aluminum Company J.D. Hunt University of Oxford (Great Britain) W.-S. Hwang National Cheng Kung University (Taiwan) J.E. Indacochea University of Illinois Carnegie Mellon University K.A. Jackson AT&T Bell Laboratories J.D. Jackson Pratt & Whitney N. Janco Technical Consultant H. Jones University of Sheffield (Great Britain) M. Jones Duriron Company, Inc. J.L. Jorstad Reynolds Aluminum David P. Kanicki American Foundrymen's Society Seymour Katz General Motors Research Laboratories T.L. Kaveney Technical Consultant Avery Kearney Avery Kearney & Company H. Kemmer Leybold AG (West Germany) Malachi P. Kenney ALUMAX Engineered Metal Processes, Inc. Gerhard Kienel Leybold AG (West Germany) Dan Kihlstadius Oregon Metallurgical Corporation Franklin L. Küskila Williams International Ken Kirgin Technical Consultant David H. Kirkwood University of Sheffield (Great Britain) F. Knell Leybold AG (West Germany) Allan A. Koch ALUMAX Engineered Metal Processes, Inc. G.J.W. Kor The Timken Company D.J. Kotecki Teledyne McKay Ronald M. Kotschi Kotschi's Software & Services, Inc. Ezra L. Kotzin American Foundrymen's Society R.W. Kraft Lehigh University

Metals Technology (Great Britain)

Austrian Foundry Research Institute

R. Hurmer

(Austria)

W. Kurz

Swiss Federal Institute of Technology (Switzerland)

Curtis P. Kyonka

ALUMAX Engineered Metal Processes,

John B. Lambert Fansteel

Craig F. Landefeld

General Motors Research Laboratories

Eugene Langner

American Cast Iron Pipe Company

A. Laporte

National Forge Company

David J. Larson, Jr.

Grumman Corporation

John P. Laughlin

Oregon Metallurgical Corporation

Franklin D. Lemkey

United Technologies Research Center

G. Lesoult

Ecole des Mines de Nancy (France)

Colin Lewis

Hitchcock Industries, Inc.

Don Lewis

Aluminum Smelt & Refining

Ronald L. Lewis

The Ohio State University

R. Lindsay, III Newport News Shipbuilding

R.D. Lindsay

Plasma Energy Corporation

Stephen Liu

Colorado School of Mines

Roy Lobenhofer

American Foundrymen's Society

C.A. Loong

Noranda Research Centre (Canada)

Carl Lundin

University of Tennessee

Norris Luther

Luther & Associates

Alvin F. Maloit

Consulting Metallurgist

P. Magnin

Swiss Federal Institute of Technology (Switzerland)

William L. Mankins

Inco Alloys International, Inc.

P.W. Marshall

Technical Consultant

Ian F. Masterson

Union Carbide Corporation

Linde Division

Gene J. Maurer, Jr.

United States Industries

D. Mayton

Urick Foundry

T.K. McCluhan Elken Metals Company

J. McDonough

Technical Consultant

J.P. McKenna

Lindberg Division

Unit of General Signal Corporation -

W. McNeish

Teledyne All-Vac

Ravi Menon

Teledyne McKay

Thomas'N. Meyer

Aluminum Company of America

William Mihaichuk

Eastern Alloys, Inc.

David P. Miller

The Timken Company

A. Mitchell

The University of British Columbia (Canada)

S. Mizoguchi

Nippon Steel Corporation (Japan)

G. Monzo

Elwood Uddeholm Steel Company

P. Moroz

Armco Inc.

F. Müller

Leybold AG (West Germany)

Frederick A. Morrow

TFI Corporation

C. Nagy

Union Carbide Corporation

N.E. Nannina

Cast Masters Division of Latrobe Steel

R.L. Naro

Ashland Chemical Company

E. Nechtelberger

Austrian Foundry Research Institute (Austria)

David V. Neff

Metaullics Systems

Charles D. Nelson

Morris Bean and Company

Dale C.H. Nevison

Zinc Information Center, Ltd.

Jeremy R. Newman

Titech International Inc.

Roger A. Nichting

Colorado School of Mines

Osaka University (Japan)

Patrick O'Meara

Intermet Foundries Inc.

B. Ozturk

Carnegie Mellon University

K.V. Pagalthivarthi

GIW Industries, Inc.

H. Pannen

Leybold AG (West Germany)

J. Parks

ME International

Murray Patz

Lost Foam Technologies, Inc.

Walter J. Peck

Central Foundry Division General Motors Corporation

Robert D. Pehlke

University of Michigan

J.H. Perepezko

University of Wisconsin-Madison

Ralph Y. Perkul

Asea Brown Boveri, Inc.

Art Piechowski

Grede Foundries, Inc.

Larry J. Pionke

McDonnell Douglas Astronautics Company

Thomas S. Piwonka

University of Alabama

Lee A. Plutshack

Foseco, Inc.

D.R. Poirier

University of Arizona

J.R. Ponteri

Lester B. Knight & Associates, Inc.

Richard L. Poole

Aluminum Company of America

William Powell

Waupaca Foundry

Henry Proffitt

Haley Industries Ltd. (Canada)

William Provis

Modern Equipment Company

Timothy J. Pruitt

Zimmer, Inc.

John D. Puckett

Nelson Metal Products Corporation

Christopher W. Ramsey

Colorado School of Mines

V. Rangarajan

Colorado School of Mines

M. Rappaz

Swiss Federal Institute of Technology (Switzerland)

Garland W. Reese

Leybold-Heraeus Technologies Inc.

J.E. Rehder

University of Toronto (Canada) H. Rice

Atlas Specialty Steel Division (Canada)

J.E. Roberts

Huntington Alloys

C.E. Rodaitis

The Timken Company

Lynn Rogers

Ervin Industries, Inc.

Pradeep Rohatgi University of Wisconsin-Milwaukee

Elwin L. Rooy Aluminum Company of America

Mervin T. Rowley

Technical Consultant

Alain Royer

Pont-A-Mousson S.A. (France) Ronald W. Ruddle

Ronald W. Ruddle & Associates

Gary F. Ruff

CMI-International

Peter R. Sahm Giesserei-Institut der RWTH

(West Germany)

Mahi Sahoo Canadian Centre for Minerals and

Robert F. Schmidt Colonial Metals Company

Energy Technology (Canada)

Richard Schaefer FWS, Inc. Donald G. Schmidt R. Lavin & Sons, Inc. T.E. Schmidt Mercury Marine Division of Brunswick Corporation Robert A. Schmucker, Jr. Thomas & Skinner, Inc. Rainer Schumann Leybold Technologies Inc. D.M. Schuster **Dural Aluminum Composites Corporation** William Seaton Seaton-SSK Engineering, Inc. R. Shebuski

Outboard Marine Corporation W. Shulof

General Motors Corporation

Leybold AG (West Germany) Geoffrey K. Sigworth

Reading Foundry Products H. Sims

Vulcan Engineering Company J. Slaughter Southern Alloy Corporation

Lawrence E. Smiley Reliable Castings Corporation

Cyril Stanley Smith Technical Consultant

Richard L. Smith Ashland Chemical Company

John D. Sommerville University of Toronto (Canada)

Warren Spear Technical Consultant T. Spence

Duriron Company, Inc.

A. Spengler **Technical Consultant** D.M. Stefanescu

The University of Alabama S. Stefanidis

I. Schumann & Company H. Stephan

Leybold AG (West Germany) T. Stevens

Wollaston Alloys, Inc. D. Stickle

Duriron Company, Inc.

Stephen C. Stocks
Oregon Metallurgical Corporation

R.A. Stoehr University of Pittsburgh C.W. Storey High Tech Castings

The Ohio State University

George R. St. Pierre

R. Russell Stratton

Investment Casting Institute

Ken Strausbaugh

Ashland Chemical Company

Lionel J.D. Sully

Edison Industrial Systems Center

Anthony L. Suschil Foseco, Inc.

Koreaki Suzuki

Hiroshima Junior College (Japan)

John M. Svoboda

Steel Founders' Society of America

Julian Szekely

Massachusetts Institute of Technology

Jack Thielke Asea Brown Boveri, Inc.

Gary L. Thoe

Waupaca Foundry, Inc. John K. Thorne

Precision Castparts Corporation

Basant L. Tiwari General Motors Research Laboratories

Judith A. Todd

University of Southern California R. Trivedi

Iowa State University Paul K. Trojan

University of Michigan-Dearborn D. Trudell

Aluminum Company of Ámerica D.H. Turner

Timet Inc. B.L. Tuttle

GMI Engineering & Management Institute

Daniel Twarog American Foundrymen's Society

Derek Tyler Olin Corporation A.E. Umble

Bethlehem Steel Corporation G. Uren

Electrical Metallurgy Company Stella Vassenr

Pont-A-Mausson (France) John D. Verhoeven

Ames Laboratory S.K. Verma

IIT Research Institute Robert Voigt

"University of Kansas

Vernon F. Voigt Giddings & Lewis Machine Tool

Company Vaughan Voller

University of Minnesota P. Voorhees

Northwestern University

Terry Waitt Maynard Steel Casting Company

J. Wallace Case Western Reserve University

Charles F. Walton Technical Consultant

A. Wavne Ward Ward & Associates Claude Watts

Technical Consultant Daniel F. Weaver Pontiac Foundry, Inc.

E. Weingärtner Leybold AG (West Germany)

D. Wells **Huntington Alloys**

Charles E. West Aluminum Company of America

J.H. Westbrook Sci-Tech Knowledge Systems, Inc.

Kenneth Whaler Stahl Specialties Company

Charles V. White GMI Engineering & Management Institute

Eldon Whiteside U.S. Gypsum

P. Wieser Technical Consultant

W.R. Wilcox Clarkson University

Larson E. Wile Consultant J.L. Wilkoff

S. Wilkoff & Sons Company

R. Williams Air Force Wright Aeronautical

Laboratories Frank T. Worzala

University of Wisconsin-Madison Nick Wukovich

Foseco, Inc. R.A. Wright Technical Consultant

Michael Wrysch Detroit Diesel Allison Division

General Motors Corporation R. Youmans

Modern Equipment Company, Inc. Kenneth P. Young

AMAX Research and Development

Center

William B. Young Dana Corporation **Engine Products Division** Michael Zatkoff Sandtechnik, Inc.

Contents

Glossary of Terms	1	Aggregate Molding Materials	. 20
Introduction and Historical Development		Bonds Formed in Molding Aggregates	21
Section Chairman: Joseph R. Davis, ASM International	13	Resin Binder Processes	21
		Sand Molding	22
History of Casting	15	Bonded Sand Molds	22
Development of Foundry Technology in the United States.		Unbonded Sand Molds	23
Casting Advantages, Applications, and Market Size	. 24	Coremaking	22
		Plaster Molding	. 24
Principles of Liquid Metal Processing	. 47	Ceramic Molding	. 24
Section Chairman, Seymour Katz, General Motors		Investment Casting .	. 25
Research Laboratories		Replicast Process	. 276
Introduction	40	Rammed Graphite Molds	. '27',
Principles of Physical Chemistry	50	Permanent Mold Casting	27:
I nermodynamic Properties of Aluminum-Rase and		Die Casting	286
Copper-Base Alloys	. 55	Centrifugal Casting Horizontal Centrifugal Casting	296
Helmodynamic Properties of Iron-Base Alloys	61	Vertical Centrifugal Casting	296
Composition Control	71	Continuous Casting	300
Gases in Metals	83	New and Emerging Processes	308
Inclusion-Forming Reactions	. 88	Counter-Gravity Low-Pressure Casting	317
		Directional and Monocrystal Solidification	317 319
Principles of Solidification	. 99	Squeeze Casting	212
Section Chairmen: W Kurz, Swiss Federal Institute of		Semisolid Metal Casting and Forging	323
Technology; D.M. Stefanescu, The University of Alabama		and Longing	321
Nucleation Kinetics	101	Foundry Fauinment and Processing	
Fundamentals of Growth	109	Foundry Equipment and Processing	339
Basic Concepts in Crystal Growth and Solidification	109	occion Chairman. Inomas Fruena, CMI International	
Solidification of Single-Phase Alloys	114	Sand Processing	341
Solidification of Eutectics	119	Green Sand Molding Equipment and Processing	3/11
Appendix 1: Simplified Theory of Eutectic Growth	124	Sand Reclamation	351
Appendix 2: Eutectic Growth at Very High		Melting Furnaces	356
Solidification Rates	125	Electric Arc Furnaces	356
Solidification of Peritectics	125	Induction Furnaces	368
Columnar to Equiaxed Transition	130	Reverberatory Furnaces and Crucible Furnaces	374
Microsegregation and Macrosegregation Behavior of Insoluble Particles at the	136	Cupolas	383
Solid/Liquid Interface		Vacuum Melting and Remelting Processes	393
Low-Gravity Effects During Solidification	142	Vacuum Induction Melting (VIM)	393
Solidification of Eutectic Alloys	147 159	Vacuum Induction Remelting and Shape Casting	399
Aluminum-Silicon Alloys	159	Electroslag Remelting (ESR)	401
Cast Iron	168	Vacuum Arc Remelting (VAR)	406
Interpretation and Use of Cooling Curves	100	Vacuum Arc Skull Melting and Casting	409
(Thermal Analysis) ,	182	Electron Beam Melting and Casting	410
		Plasma Melting and Casting .	419
atterns	187	Degassing Processes (Converter Metallurgy)	426
ection Chairman: Robert Voigt, The University of Kansas		Argon Oxygen Decarburization (AOD)	426
		Vacuum Oxygen Decarburization (VODC) Degassing Processes (Ladie Metallurgy)	429
Patterns and Patternmaking	189	Vacuum Ladle Degreeing (VD)	432
		Vacuum Ladle Degassing (VD) Vacuum Oxygen Decarburization (VOD)	432
folding and Casting Processes'.	201	Ladle Furnace and Vacuum Arc Degassing	434
ection Chairman: Thomas S. Piwonka, The University of Alabama		(LF/VD-VAD)	435
		Vacuum Induction Degassing (VID)	433
Classification of Processes and Flow Chart of		Plasma Heating and Degassing	440
Foundry Operations	203	Nonferrous Molten Metal Processes	445

Automatic Pouring Systems	497 502 502	Nonferrous Casting Alloys	741
Blast Cleaning of Castings	506 520 538 544 561 566	Aluminum and Aluminum Alloys Copper and Copper Alloys Zinc and Zinc Alloys Magnesium and Magnesium Alloys Cobalt-Base Alloys Nickel and Nickel Alloys	771 786 798
Design Considerations Riser Design Gating Design Casting Design	575 577 589 598	Titanium and Titanium Alloys	836
Dimensional Tolerances and Allowances	614 625	Computer Applications in Metal Casting Section Chairmen: John T. Berry, The University of Alabama; Robert D. Pehlke, The University of Michigan Introduction	857
Classification of Ferrous Casting Alloys	627 629 647	Modeling of Solidification Heat Transfer Modeling of Fluid Flow Modeling of Combined Fluid Flow and Heat/Mass	867
Compacted Graphite Irons	667 678 686	Transfer	883
High-Alloy Graphitic Irons Plain Carbon Steels Low-Alloy Steels	698 702 715	Metric Conversion Guide	
High-Alloy Steels	722 736	Index	899

Glossary of Terms

acid. A term applied to slags, refractories, and minerals containing a high percentage

acidity. The degree to which a material is acid. Furnace refractories are ranked by their acidity.

acid process. A steelmaking method using an acid refractory-lined furnace. Neither sulfur nor phosphorus is removed.

acid refractory. Siliceous ceramic materials of a high melting temperature, such as silica brick, used for metallurgical furnace linings. Compare with basic refractory.

addition agent. (1) Any material added to a charge of molten metal in a bath or ladle to bring the alloy to specifications. (2) Reagent added to plating bath.

additive. Any material added to molding sand for reasons other than bonding, for example, seacoal, pitch, graphite, cereals.

aerate. To fluff up molding sand to reduce its density.

airblasting. See blasting or blast cleaning. air channel. A groove or hole that carries the vent from a core to the outside of a

air dried. Refers to the air drying of a core or mold without the application of heat.

air-dried strength. Strength (compressive, shear, or tensile) of a refractory (sand) mixture after being air dried at room temperature.

air furnace. Reverberatory-type furnace in which metal is melted by heat from fuel burning at one end of the hearth, passing over the bath toward the stack at the other end. Heat is also reflected from the roof and sidewalls. See also reverberatorv furnace

air hole. A hole in a casting caused by air or gas trapped in the metal during solidification

air setting. The characteristic of some materials, such as refractory cements, core pastes, binders, and plastics, to take permanent set at normal air temperatures.

allowance. In a foundry, the specified clearance. The difference in limiting sizes, such as minimum clearance or maximum interference between mating parts, as computed arithmetically. See also tolerance.

alpha process. A shell molding and coremaking method in which a thin resinbonded shell is baked with a less expensive, highly permeable material.

alumina. The mineral aluminum oxide (Al₂O₃) with a high melting point (refractory) that is sometimes used as a molding sand.

angularity. The angular relationship of one surface to another. Specifically, the dimensional tolerance associated with such features on a casting.

arbitration bar. A test bar, cast with a heat of material, used to determine chemical composition, hardness, tensile strength, and deflection and strength under transverse loading in order to establish the state of acceptability of the casting.

arbor. A metal shape embedded in and used to support green or dry sand cores in the mold.

arc furnace. A furnace in which metal is melted either streetly by an electric arc between an electrode and the work or indirectly by an arc between two electrodes adjacent to the metal.

arc melting. Melting metal in an electric arc furnace

as-cast condition. Castings as removed from the mold without subsequent heat treat-

atmospheric riser. A riser that uses atmospheric pressure to aid feeding. Essentially, a blind riser into which a small core or rod protrudes; the function of the core or rod is to provide an open passage so that the molten interior of the riser will not be under a partial vacuum when metal is withdrawn to feed the casting but will always be under atmospheric pressure.

austenite. A solid solution of one or more elements in face-centered cubic iron (gamma iron). Unless otherwise designated (such as nickel austenite), the solute is generally assumed to be carbon.

back draft. A reverse taper that prevents removal of a pattern from a mold or a core from a core box.

backing board (backing plate). A second bottom board on which molds are opened. backup coat. The ceramic slurry of dip coat that is applied in multiple layers to provide a ceramic shell of the desired thickness and strength for use as a mold.

bake. Heating in an oven to a low controlled temperature to remove gases or to harden a binder.

baked core. A core that has been heated through sufficient time and temperature

to produce the desired physical properties attainable from its oxidizing or thermal-setting binders.

bank sand. Sedimentary deposits, usually containing less than 5% clay, occurring in banks or pits, used in coremaking and in synthetic molding sands. See sand.

basic refractory. A lime- or magnesia-base ceramic material of high melting temperature used for furnace linings. Compare with acid refractory.

hatch. An amount of core or mold sand or other material prepared at one time.

bath. Molten metal on the hearth of a furnace, in a crucible, or in a ladle.

bead. (1) Half-round cavity in a mold, or half-round projection or molding on a casting. (2) A single deposit of weld metal produced by fusion.

bedding. Sinking a pattern down into the sand to the desired position and ramming the sand around it.

bedding a core. Placing an irregularly shaped core on a bed of sand for drying.

bench molding. Making sand molds by hand tamping loose or production patterns at a bench without the assistance of air or hydraulic action.

bentonite. A colloidal claylike substance derived from the decomposition of volcanic ash composed chiefly of the minerals of the montmorillonite family. It is used for bonding molding sand.

bimetal. A casting made of two different metals, usually produced by centrifugal casting.

binder. A material used to hold the grains of sand together in molds or cores. It may be cereal, oil, clay, or natural or organic

blacking. Carbonaceous materials, such as graphite or powdered carbon, usually mixed with a binder and frequently carried in suspension in water or other liquid used as a thin facing applied to surfaces of molds or cores to improve casting finish.

blasting or blast cleaning. A process for cleaning or finishing metal objects with an air blast or centrifugal wheel that throws abrasive particles against the surface of the workpiece. Small, irregular particles of metal are used as the abrasive in gritblasting; sand, in sandblasting; and steel balls, in shotblasting.

bleed. Refers to molten metal oozing out of a casting. It is stripped or removed from the mold before complete solidification.

blended sand. A mixture of sands of different grain size and clay content that provides suitable characteristics for foundry use.

blind riser. A riser that does not extend

through the top of the mold.

blister. A defect in metal, on or near the surface, resulting from the expansion of gas in a subsurface zone. It is characterized by a smooth bump on the surface of the casting and a hole inside the casting directly below the bump.

blow. A term that describes the trapping of gas in castings, causing voids in the met-

blowhole. A void or large pore that may occur because of entrapped air, gas, or s' rinkage; usually evident in heavy sections.

blow holes. Holes in the head plate or blow plate of a core blowing machine through which sand is blown from the reservoir into the core box.

bond clay. Any clay suitable for use as a bonding agent in molding sand.

bond strength. The degree of cohesiveness that the bonding agent exhibits in holding sand grains together.

bondi .g agent. Any material other than water that, when added to foundry sands, imparts strength either in the green, dry, or fired state.

boss. A relatively short protrusion or projection from the surface of a forging or casting, often cylindrical in shape. Usually intended for drilling and tapping for attaching parts. See also locating boss.

bottom board. A flat base for holding the

flask in making sand molds.

bottom-pour ladle. A ladle from which metal, usually steel, flows through a nozzle located at the bottom.

bottom running or pouring. Filling of the mold cavity from the bottom by means of

gates from the runner.

bridging. (1) Premature solidification of metal across a mold section before the metal below or beyond solidifies. (2) Solidification of slag within a cupola at or just above the tuyeres.

buckle. (1) Bulging of a large, flat face of a casting; in investment casting, caused by dip coat peeling from the pattern. (2) An indentation in a casting, resulting from expansion of the sand, can be termed the start of an expansion defect.

bumper. A machine used for packing molding sand in a flask by repeated jarring or jolting. See also jolt ramming.

burned-in sand. A defect consisting of a mixture of sand and metal cohering to the surface of a casting.

burned-on sand. A misnomer usually indicating metal penetration into sand resulting in a mixture of sand and metal adhering to the surface of a casting. See also metal penetration.

burnout. Firing a mold at a high temperature to remove pattern material residue.

burned sand. Sand in which the binder or bond has been removed or impaired by contact with molten metal.

calcium silicon. An alloy of calcium, silicon, and iron containing 28 to 35% Ca, 60 to 65% Si, and 6% Fe (max), used as a deoxidizer and degasser for steel and cast iron; sometimes called calcium silicide.

carbonaceous. A material that contains carbon in any or all of its several allotropic

carbon dioxide process (sodium silicate/ CO₂). A process for hardening molds or cores in which carbon dioxide gas is blown through dry clay-free silica sand to precipitate silica in the form of a gel from the sodium silicate binder.

carbon refractory. A manufactured refractory comprised substantially or entirely of

carbon (including graphite).

castability. (1) A complex combination of liquid-metal properties and solidification characteristics that promotes accurate and sound final castings. (2) The relative ease with which a molten metal flows through a mold or casting die.

castable. A combination of refractory grain and suitable bonding agent that, after the addition of a proper liquid, is generally poured into place to form a refractory shape or structure that becomes rigid

because of chemical action.

casting. (1) Metal object cast to the required shape by pouring or injecting liquid metal into a mold, as distinct from one shapeo by a mechanical process. (2) Pouring molten metal into a mold to produce an object of desired shape.

casting defect. Any imperfection in a casting that does not satisfy one or more of the required design or quality specifications. This term is often used in a limited sense for those flaws formed by improper cast-

ing solidification.

casting section thickness. The wall thickness of the casting. Because the casting may not have a uniform thickness, the section thickness may be specified at a specific place on the casting. Also, it is sometimes useful to use the average, minimum, or typical wall thickness to describe a casting.

casting shrinkage. The amount of dimensional change per unit length of the casting as it solidifies in the mold or die and cools to room temperature after removal from the mold or die. There are three distinct types of casting shrinkage. Liquid shrinkage refers to the reduction in volume of liquid metal as it cools to the liquidus. Solidification shrinkage is the reduction in volume of metal from the beginning to the end of solidification. Solid shrinkage involves the reduction in volume of metal from the solidus to room temperature.

casting stresses. Stresses set up in a casting because of geometry and casting shrinkage. casting thickness. See casting section thickness.

casting volume. The total cubic units (mm³ or in.3) of cast metal in the casting

casting yield. The weight of a casting(s) civided by the total weight of metal poured into the mold, expressed as a percentage.

cast iron. A generic term for a large family of cast ferrous alloys in which the carbon content exceeds the solubility of carbon in austenite at the eutectic temperature. Most cast irons contain at least 2% C. plus silicon and sulfur, and may or may not contain other alloying elements. For the various forms, the word cast is often left out, resulting in compacted graphite iron, gray iron, white iron, malleable iron, and ductile iron.

cast structure. The internal physical structure of a casting evidenced by the shape and orientation of crystals and the segre-

gation of impurities.

cavity. The mold or die impression that gives a casting its external shape.

cementite. A very hard and brittle compound of iron and caroon corresponding to the empirical formula Fe₃C, commonly known as iron carbide.

centerline shrinkage. Shrinkage or porosity occurring along the central plane or axis

of a cast part.

centrifugal casting. The process of filling molds by (1) pouring metal into a sand or permanent mold that is revolving about either its horizontal or its vertical axis or (2) pouring metal into a mold that is subsequently revolved before solidification of the metal is complete. See also centrifuge casting.

centrifuge casting. A casting technique in which mold cavities are spaced symmetrically about a vertical axial common downgate. The entire assembly is rotated about that axis during pouring and solidification.

ceramic. Material of a nonmetallic nature, usually refractory, made from fused, sintered, or cemented metallic oxides.

ceramic molding. A precision casting process that employs permanent patterns and fine-grain slurry for making molds. Unlike monolithic investment molds, which are similar in composition, ceramic molds consist of a cope and a-drag or, if the casting shape permits, a drag only.

CG iron. Same as compacted graphite iron. chaplet. Metal support that holds a core in place within a mold; molten metal solidifies around a chaplet and fuses it into the finished casting.

charge. (1) The materials placed in a melting furnace. (2) Castings placed in a heattreating furnace.

check. A minute crack in the surface of a casting caused by unequal expansion or contraction during cooling.

- chill. (1) A metal or graphite insert embeaded in the surface of a sand mold or core or placed in a mold cavity to increase the cooling rate at that point. (2) White iron occurring on a gray or ductile iron casting, such as the chill in the wedge test. See also chilled iron. Compare with inverse chill.
- chill coating. Applying a coating to a chill that, forms part of the mold cavity so that the metal does not adhere to it, or applying a special coating to the sand surface of the mold that causes the iron to undercool.

chilled iron. Cast iron that is poured into a metal mold or against a mold insert so as to cause the rapid solidification that often tends to produce a white iron structure in the casting.

clay. A natural, earthy, fine-g, ain material that develops plasticity when mixed with a limited amount of water. Foundry clays, which consist essentially of hydrous silicates of alumina, are used in

molds and cores.

CO₂ process. See carbon dioxide process. coming. (1) The process of straightening and sizing castings by die pressing. (2) A press metalworking operation that establishes accurate dimensions of flat surfaces or depressions under predominantly compressive loading.

coke. A porous, gray, infusible product resulting from the dry distillation of bituminous coal, petroleum, o. coal tar pitch that drives off most of the volatile matter. Used as a fuel in cupola melting.

coke bed. The first layer of coke placed in the cupola. Also the coke used as the foundation in constructing a large mold in a flask or pit.

coke breeze. Fines from coke screenings, used in blacking mixes after grinding; also briquetted for cupola use.

coke furnace. Type of pot or crucible furnace that uses coke as the fuel.

cold box process. A two-part organic resin binder system mixed in conventional mixers and blown into shell or solid core shapes at room temperature. A vapor mixed with air is blown into the core, permitting instant setting and immediate pouring of metal around it.

cold chamber machine. A die casting machine with an injection system that is charged with liquid metal from a separate furnace. Compare with hot chamber ma-

chine.

cold cracking. Cracks in cold or nearly cold metal due to excessive internal stress caused by contraction. Often brought about when the mold is too hard or the casting is of unsuitable design.

cold lap. Wrinkled markings on the surface of an ingot or casting from incipient freezing of the surface and too low a casting

temperature.

cold-setting process. Any of several systems for bonding mold or core aggregates by

means of organic binders, relying on the use of catalysts rather than heat for polymerization (setting).

cold that. (1) A portion of the surface of an ingot or casting showing premature solidification; caused by splashing of molten metal onto a cold mold wall during pouring. (2) Small globule of metal embedded in, but not entirely fused with, the casting.

cold shut. (1) A discontinuity that appears on the surface of cast metal as a result of two streams of liquid meeting and failing to unite. (2) A lap on the surface of a forging or billet that was closed without fusion during deformation. (3) Freezing of the top surface of an ingot before the mold is full.

collapsibility. The tendency of a sand mixture to break down under the pressures and temperatures developed during casting.

columnar structure. A coarse structure of parallel columns of grains, that is caused by highly directional solidification resulting from sharp thermal gradients.

combination die (multiple-cavity die). In die casting, a die with two or more different

cavities for different castings.

combined carbon. Carbon in iron that is combined chemically with other elements; not in the free state as graphite or temper carbon. The difference between the total carbon and the graphite carbon analyses. Contrast with free carbon.

compacted graphite iron. Cast iron having a graphite shape intermediate between the flake form typical of gray iron and the spherical form of fully spherulitic ductile iron. Also known as CG iron or vermicular iron, compacted graphite iron is produced in a manner similar to that for ductile iron but with a technique that inhibits the formation of fully spherulitic graphite nodules.

constraint. Any restriction that limits the transverse contraction normally associated with a longitudinal tension, and therefore causes a secondary tension in the transverse direction.

consumable-electrode remelting. A process for refining metals in which an electric current passes between an electrode made of the metal to be refined and an ingot of the refined metal, which is contained in a water-cooled mold. As a result of the passage of electric current, droplets of molten metal form on the electrode and fall to the ingot. The refining action occurs from contact with the atmosphere, vacuum, or slag through which the drop falls. See electroslag remelting and vacuum arc remelting.

continuous casting. A process for forming a bar of constant cross section directly from molten metal by gradually withdrawing the bar from a die as the metal flowing into the die solidifies. contraction. The volume change that occurs in metals and alloys upon solidification and cooling to room temperature.

convection. The motion resulting in a fluid from the differences in density and the action of gravity. In heat transmission, this meaning has been extended to include both forced and natural motion or circulation.

cooling stresses. Stresses developed during cooling by the uneven contraction of metal, generally due to nonuniform cooling.

cope. The upper or topmost section of a flask, mold, or pattern.

core. (1) A specially formed material inserted in a mold to shape the interior or other part of a casting that cannot be shaped as easily by the pattern. (2) In a ferrous alloy prepared for case hardening, that portion of the alloy that is not part of the case. Typically considered to be the portion that (a) appears light on an etched cross section, (b) has an essentially unaltered chemical composition, or (c) has a hardness, after hardening, less than a speci-

core assembly. A complex core consisting of a number of sections.

fied value.

core binder. Any material used to hold the grains of core sand together.

core blow. A gas pocket in a casting adjacent to a cored cavity and caused by entrapped gases from the core.

core blower. A machine for making foundry cores using compressed air to blow and pack the sand into the core box.

core box. A wood, metal, or plastic structure containing a shaped cavity into which sand is packed to make a core.

core dryers. Supports used to hold cores in shape during baking; constructed from metal or sand for conventional baking or from plastic material for use with dielectric core-baking equipment.

core filler. Material, such as coke, cinder, and sawdust, used in place of sand in the interiors of large cores; usually added to aid collapsibility.

coring. A variable composition between the center and the surface of a unit of structure (such as a dendrite, grain, or carbide particle) resulting from the nonequilibrium growth that occurs over a range of temperature.

core knockout machine. A mechanical device for removing cores from castings.

coreless induction furnace. An electric induction furnace for melting or holding molten die casting metals that does not utilize a steel core to direct the magnetic field.

core oil. A binder for core sand that sets when baked and is destroyed by the heat from the cooling casting.

core plates. Heat-resistant plates used to support cores during baking; may be meatallic or nonmetallic, the latter being a requisite for dielectric core baking.

16