

8461212

PROCEEDINGS OF THE

THIRD INTERNATIONAL CONFERENCE ON FINITE ELEMENTS IN FLOW PROBLEMS

BANFF, ALBERTA, CANADA

10-13 JUNE, 1980



VOLUME I

TB115-2
F3
V.1
1980

TB115-2
F3
V.1
(2)

8461212
035-53
161.2
1980
V.1

PROCEEDINGS OF THE

THIRD INTERNATIONAL CONFERENCE ON FINITE ELEMENTS IN FLOW PROBLEMS

BANFF, ALBERTA, CANADA

10-13 JUNE, 1980



VOLUME I



E8461212

THIRD INTERNATIONAL CONFERENCE ON FINITE ELEMENTS IN FLOW PROBLEMS

INTERNATIONAL ORGANIZING COMMITTEE

- R. Glowinski, INRIA, Rocquencourt, France
- R. H. Gallagher, University of Arizona, USA
- M. Kawahara, Chuo University, Tokyo, Japan
- D. H. Norrie, University of Calgary, Canada (Chairman)
- J. T. Oden, University of Texas, Austin, USA
- C. Taylor, University of Wales, Swansea, United Kingdom
- O. C. Zienkiewicz, University of Wales, Swansea, United Kingdom

LOCAL ARRANGEMENTS COMMITTEE

- D. Bennion, Department of Chemical Engineering, University of Calgary
- G. de Vries, Delray Engineering, Calgary
- B. Irons, Department of Civil Engineering, University of Calgary
- D. H. Norrie, Department of Mechanical Engineering, University of Calgary
- A. Pollard, Department of Mechanical Engineering, University of Calgary
- R. Westbrook, Department of Mathematics and Statistics, University of
Calgary (Chairman)

EDITOR: D. H. NORRIE

THE THIRD INTERNATIONAL CONFERENCE ON FINITE
ELEMENTS IN FLOW PROBLEMS WAS SUPPORTED BY
THE FOLLOWING ORGANIZATIONS:

NATIONAL SCIENCES AND ENGINEERING RESEARCH
COUNCIL CANADA

THE UNIVERSITY OF CALGARY

AIR CANADA

CP AIR

CONTENTS

VOLUME I

PAGE NUMBER

INVITED LECTURES

Some Developments of the Finite Element Methods for Fluid Mechanics - <i>O. C. Zienkiewicz, R. L. Taylor</i>	1
Transonic Flow Simulations by Finite Elements and Least Square Methods - <i>M. O. Bristeau, R. Glowinski, J. Periaux, P. Perrier, O. Pironneau, G. Poirier</i>	11
Boundary Methods in Flow Problems - <i>I. Herrera</i>	30
Modeling of Environmental Hydrodynamics and Field Data Requirements - <i>R. T. Cheng</i>	43
The Utilisation of the F.E.M. in the Solution of Some Free Surface Problems - <i>C. Taylor</i>	54
Theoretical Analysis of Some Finite Element Schemes for Convective Diffusion Equations - <i>F. Kikuchi, T. Ushijima</i> .	82

NAVIER-STOKES AND NATURAL CONVECTION PROBLEMS

On the Spurious Pressures Generated by Certain GFEM Solutions of the Incompressible Navier-Stokes Equations - <i>R. L. Sani, P. M. Gresho, R. L. Lee</i>	96
A Finite Element Method for Navier-Stokes Equations - <i>J. P. Benque, B. Ibler, A. Keramsi, G. Labadie</i>	110
An Uncoupled Approach for Primitive Variable Solutions to Viscous Incompressible Flows - <i>A. N. F. Mack</i>	121
A Comparison of Various Finite Elements Schemes for the Solution of the Navier-Stokes Equations in Rotating Flow - <i>P. Bar-Yoseph</i>	132
Further Finite Element Results for the Square Cavity - <i>M. D. Olson, S-Y. Tuann</i>	143
Natural Convection in Inclined Square Enclosures at High Rayleigh Numbers - <i>J. C. Heinrich, M. Strada</i>	153
Finite Element Computations with Refined Mesh for Two-Dimensional Natural Convection in Closed Cells - <i>J. S. Lidder, P. L. Betts</i>	164

CONTENTS

	<u>PAGE NUMBER</u>
A Finite Element Analysis of Volumetrically Heated Fluids in an Axisymmetric Enclosure - <i>D. K. Gartling</i> . . .	174
Finite Element Boundary Techniques for Improved Performance in Computing Navier-Stokes and Related Heat Transfer Problems - <i>A. G. Hutton</i>	183
Finite Element Analysis of Convective Heat Transfer in a Porous Medium - <i>D. K. Gartling</i>	194
A New Finite Element for Incompressible or Boussinesq Fluids - <i>P. M. Gresho, R. L. Lee, S. T. Chan, J. M. Leone, Jr.</i>	204
A Comparison of Several Conservative Forms for Finite Element Formulations of the Incompressible Navier-Stokes or Boussinesq Equations - <i>R. L. Lee, R. P. Gresho, S. T. Chan, R. L. Santi</i>	216
 <u>POROUS MEDIA</u>	
A Finite Element in Time and Space Model for Quasi-Three-Dimensional Multiaquifer Simulation - <i>J. P. Hennart, R. Yates, I. Herrera</i>	228
A Consolidation Analysis of a Waterdrive Gas Reservoir - <i>B. A. Schrefler, R. W. Lewis</i>	237
A Comparison of Rayleigh-Ritz and Kantorovich Methods for Unsteady Porous Flow with Free Surfaces - <i>H. Rasmussen, D. Sulhani</i>	248
Galerkin Approximation of the Time-Derivative for the Problem of a Real Gas Flow Through Porous Media - <i>A. Q. Romo, M. A. Llovera-Polo</i>	256
Thermomechanically Coupled Creeping Flow of Saturated Cohesive Porous Media - <i>P. R. Dawson, P. F. Chavez</i>	268
Three-Dimensional Seepage Through a Homogeneous Dam with a Toe Drain - <i>J. P. Caffrey, J. C. Bruch, Jr.</i>	280
A Variable Domain Finite Element Analysis of Seepage From a Ditch - <i>E. Varoglu, W. D. L. Finn</i>	290

CONTENTS

	<u>PAGE NUMBER</u>
Two Phase Seepage of a Compressible Fluid in an Inhomogeneous Medium - <i>G. P. Steven, D. J. Auld</i>	300
<u>NON-NEWTONIAN FLOW</u>	
Numerical Solution of the Flow and Heat Transfer of Polymer Melts - <i>S. Nakazawa, J. F. T. Pittman, O. C. Zienkiewicz</i> .	311
A Finite Element Method for Bingham Fluid Flows - <i>M. Bercovier, M. Engelman, M. Fortin</i>	322
The Flow of a Maxwell Fluid Around a Sphere - <i>M. J. Crochet</i>	332
<u>BOUNDARY LAYERS AND TURBULENT FLOW</u>	
A Diabatic, Turbulent, Atmospheric Boundary-Layer Model - <i>E. S. Takle, R. L. Santi, L. P. Chang</i>	342
A Finite Element-Differential Method for a Class of Boundary-Layer Flows - <i>C-C. Hsu</i>	351
Two-Dimensional Finite Element Model for Turbulent Flows in Rivers, Channels and Around Obstacles - <i>M Thienpont, J. Berlamont</i>	361
<u>COMPRESSIBLE FLOW</u>	
Some Mathematical Aspects of Compressible Flow - <i>G. F. Carey</i>	374
Finite Element Methods for the Solution of Full Potential Equation in Transonic Steady and Unsteady Flow - <i>A. Eberle</i>	381
Treatment of Shocks in the Computation of Transonic Flows Using Finite Elements - <i>H. U. Akay, A. Ecer</i>	391
Optimum Design for Potential Flows - <i>F. Angrand, R. Glowinski, J. Periaux, P. Perrier, G. Poirier, O. Pironneau</i> .	400

SOME DEVELOPMENTS OF THE FINITE ELEMENT
METHODS FOR FLUID MECHANICS

by

O.C. Zienkiewicz
Professor
Civil Engineering Department
University College Swansea, U.K.
Naval Sea Systems Command
Research Professor
Naval Postgraduate School
Monterey, California

R.L. Taylor
Professor
Civil Engineering Department
University of California
Berkeley, California

ABSTRACT

The paper reviews and summarizes the developments in:

- (a) Penalty methods for enforcement of incompressibility constraints.
- (b) Galerkin-Petrov, upwind methods for concrete-diffusive problems.
- (c) Hierarchical concepts of element formulation and introduces;
- (d) new semi-explicit time stepping procedures.

INTRODUCTION

More than a decade has now elapsed since the entry of the finite element method into the arena of numerical fluid mechanics. Its unlimited potential as a unified approximation procedure is being realized today but many special developments are required to make its applications economically advantageous.

In the opening lectures of the first and second conferences of this series the first author had the privilege of introducing two developments which today have become established and widely used. The first of these, in the 1974 conference, was the introduction of penalty formulation [1],[2] for simple treatment of incompressible flow. The second, in the 1976 conference was the Petrov-Galerkin treatment of optimally "upwinded" convective terms. [3],[4],[5] At this, third, conference we shall;

- (a) survey the development of both 'upwinding' and penalty procedures;
- (b) introduce a special penalty formulation not necessitating the use of reduced integration.
- (c) draw attention to 'hierarchical' finite element concepts which have recently been introduced with success to the solid mechanics field and finally;
- (d) introduce a class of new time stepping methods which promises to improve the economics of computation.

PENALTY PROCEDURES

Many physical processes are governed by differential equations of the type

$$\begin{cases} \underline{L}u + \underline{\bar{C}}^T p = \underline{f} \\ \underline{C}u = 0 \end{cases} \quad \text{where } \underline{L}, \underline{\bar{C}} \text{ and } \underline{C} \text{ are differential operators} \\ \text{and } u, p \text{ the independent variables.} \quad (1)$$

The Navier-Stokes equations of fluid mechanics are a particular case of above with u standing for the velocities and p for the pressures. Further, in this particular case the operator

$$\underline{C} = \underline{\bar{C}} \equiv \underline{\nabla}^T \quad (2)$$

is a constraint imposing incompressibility.

In penalty formulation we first approximate equation (1) by writing

$$\begin{aligned} \underline{L}\underline{u} + \underline{\bar{C}}^T \underline{p} &= \underline{f} \\ \underline{C}\underline{u} - \frac{\underline{p}}{\alpha} &= 0 \end{aligned} \quad (2)$$

where, with $\alpha \rightarrow \infty$ the original formulation is obtained.

The device of introducing the penalty parameter, α , has the advantage of permitting the elimination of \underline{p} , either before or after discretization avoiding the difficulties associated numerically with typical, zero diagonals, of Lagrangian form.

The two alternate approaches lead to discretization which can be written either as

$$\begin{bmatrix} K_{uu} & K_{up} \\ K_{pu} & \frac{1}{\alpha} K_{pp} \end{bmatrix} \begin{Bmatrix} \underline{\bar{u}} \\ \underline{\bar{p}} \end{Bmatrix} = \begin{Bmatrix} \underline{\bar{f}} \\ 0 \end{Bmatrix} \quad (3)$$

with

$$\underline{u} = \underline{N}\underline{\bar{u}}; \underline{p} = \underline{\bar{N}}\underline{\bar{p}}$$

Equation (3) leads on elimination of $\underline{\bar{p}}$ to a form

$$\left(K_{uu} + \alpha \hat{K} \right) \underline{\bar{u}} = \underline{\bar{f}} \quad (4)$$

If alternatively \underline{p} is eliminated at the differential equation level and discretization adopted for \underline{u} alone we have a form

$$\left(K_{uu} + \alpha \hat{K} \right) \underline{\bar{u}} = \underline{\bar{f}} \quad (5)$$

where in general

$$\hat{K} \neq K$$

The evaluation of the matrix K in the first form of Eq. 4 is cumbersome and costly for C^0 continuous \underline{p} discretization. However, if the weak form of Eq. 1 permits discontinuous approximations, the parameters $\underline{\bar{p}}$ can be eliminated at element level. For particular local discretizations of this form it can be shown that formulation (4) became identical with those of (5) in which quadrature rule adopted for \underline{K} uses identical number of values as the number of parameters required for \underline{p} determination. [6]

It will be realized that the number of parameters of $\underline{\bar{p}}$ introduced (or the number of quadrature points used) is equivalent to the number of constraints of incompressibility imposed. If this number is 'm' and the number of parameters describing variation of \underline{u} is 'n' then clearly for nontrivial solutions

$$n > m$$

is needed. In Fig. 1, we show the performance of various elements on the basis of a number

$$\beta = \frac{\Delta n}{\Delta m} \quad (6)$$

for addition of a single element to a constrained field. Obviously $\beta < 1$ will lead to meaningless results.

It is readily seen why the serendipity type element originally used (1) has now been superceded by linear [7] and parabolic [8] Lagrangian elements with reduced/selective integration. Using in place of reduced integration - locally defined 3 parameter linear expansion allows us to resurrect the serendipity element as an efficient non-locking one.[9][10]

Same comments apply to three dimensional problems where again an extremely efficient, serendipity type, brick with 20 nodes has been developed using four internal constraints.

OPTIMAL, UPWINDED PETROV-GALERKIN SCHEMES

The original concepts of 'upwinding' or the use of non-symmetric weighting functions have been suggested by some equivalent finite difference ideas but have not followed the same path. Thus many objections (of excessive diffusion or inaccuracy) have been laid to rest. It has been repeatedly shown that optimally upwinded schemes not only eliminate 'wiggles' [11], but at all stages produce more accurate solutions in the steady state convective-diffusive problems than do symmetric Galerkin Bubnov type operators (even in the extreme case when both numerical solutions are 'wiggly' free).

The interest in this area of finite element approximation has found its expression in a recent conference on this subject[12]. Despite much discussion it can be concluded that the original form of upwinding for one dimensional and two dimensional elements[3][5] is still not superceded although variants in the formulation using special quadrature rules [13] or equivalent compensating diffusion[14][15] ease numerical computation.

Extension of upwinding to the Navier-Stokes equations has followed a similar path and today this is widely used in that context[16-19].

For transient, non-steady state convective-diffusion problems much yet remains to be done but clearly if such problems tend to steady state precisely the same amount of 'upwinding' will be necessary. Thus concentration of activity on reduction of 'error' in time marching schemes is of primary importance.

HIERARCHICAL CONCEPTS AND ITERATIVE SOLUTIONS

As the finite element method is an approximation process it is frequently necessary to use two or more mesh refinements to obtain an accurate solution. In the standard use of finite elements the subdivided mesh does not contain the coarser mesh shape functions and in general no use is made of the coarse mesh solution to obtain the refined one. If on the other hand, shape functions are arranged 'hierarchically' in such a manner that the refined variables (a_j) are superposed on the coarse ones (a_i) then the matrix discretized forms are

for coarse mesh

$$K_{ii} \tilde{a}_i = \tilde{f}_i \quad (7)$$

for fine mesh

$$\begin{bmatrix} \tilde{K}_{ii} & \tilde{K}_{ij} \\ \tilde{K}_{ji} & K_{jj} \end{bmatrix} \begin{bmatrix} \tilde{a}_i \\ a_j \end{bmatrix} = \begin{bmatrix} \tilde{f}_i \\ f_j \end{bmatrix} \quad (8)$$

Here not only the original (coarse mesh) matrix reappears but \tilde{a}_i , the coarse mesh solution forms a first approximation to the iterative solution of the refined variables.

Hierarchical functions arise naturally in the 'global-local' approximations of Mote [20] or in successive addition of polynomial modes to isoparametric elements[21]. The realization of the power of the process for refinement of solution by iteration can be credited independently to Wilson [22], Wachspress[23], Peano[24][25], Szabo[26]. Indeed the latter two authors and their collaborators have extended the process to self-adaptive mesh refinement procedures [viz. Babuska 27][28].

While all the applications of the hierarchical concepts have so far been made in the context of linear solid mechanics, their use in non-linear fluid mechanics area is yet to come. If we consider the fact that iterative processes are invariably necessary in such problems and that these are the major part of the cost of the operation it seems that the use of hierarchical concepts is here overdue.

In the finite difference context parallel progress has been made using so called multi-grid procedures in which acceleration of iteration by simultaneous use of coarse and fine grids together with appropriate interpolation has proved successful.[28] Clearly in finite element form where the link between successive refinements is clearer the process would be even more advantageous.

A NEW SET OF TIME STEPPING ALGORITHM (SEE) SELECTIVE EXTRAPOLATED EXPLICIT PROCESSES

The solution of unsteady state fluid mechanics problems (or indeed the use of such unsteady solutions as an interaction device to obtain steady states) necessitates the use of efficient time stepping processes. Many such processes are now known and well documented; further most of these can be developed via the application of finite element concepts to the time domain.

With 'explicit' processes the computation of each time step is trivial as no equation solving processes are involved. Unfortunately such schemes are plagued by instability and an extremely small time step is generally needed to overcome this. Unconditionally stable, implicit methods require on the other hand a full equation solution to be carried out at each computational step and thus the cost per time step is very much larger. In the finite difference context a very much economical compromise has been achieved in the so called ADI (Alternating Direction Implicit) processes [31/33] and some attempts at grafting these methods on to the finite element formulations have recently been made.[33]

Here we shall outline general partitioning/staggered processes which are similar to the ADI methods but which can in the limit be reduced to a fully explicit and unconditionally stable methods. We shall class the method under the name of SEE (Selective Extrapolated Explicit) Process.

The motivation for the methods here described comes from procedures developed for the solution of coupled physical systems by Parks and Fellipa [34],[35] the approach below assumes that we are dealing with two sets of (discretized) physical variables a_1 and a_2 which obey the coupled equations of first order

$$C_{11} \dot{a}_1 + K_{11} a_1 + [C_{12} \dot{a}_2 + K_{12} a_2] = f_1 \quad (9a)$$

$$C_{22} \dot{a}_2 + K_{22} a_2 + [C_{21} \dot{a}_1 + K_{12} a_2] = f_2 \quad (9b)$$

Considering the above system we can proceed as follows. First, by the use of some integration algorithm, solve equation (9a) for the variable a_1^{n+1} using known values of a_1^n, a_1^{n-1} etc., and extrapolated values of \dot{a}_2^x and \dot{a}_2^x . Second, apply a similar solution to Eq. (9b) for a_2^{n+1} using now the values of a_1^{n+1} computed in the first step of the operation.

Using unconditionally stable although not necessarily identical algorithms, for each stage of the operation and a suitable extrapolation procedure unconditional stability of the whole process can be assured.

Consider for instance the application of linear expansion of a_1 and a_2 and the use of suitable weighting resulting in a two point θ , algorithm [36] to Eq.(9.1) We have now, at stage 1 of the operation

$$C_{11} (\dot{a}_1^{n+1} - \dot{a}_1^n) + \Delta t K_{11} (\theta_1 a_1^{n+1} + (1-\theta_1) a_1^n) = \Delta t \bar{f}_1 - C_{12} \dot{a}_2^x - \Delta t K_{12} \bar{a}_2^x \quad (10)$$

where the extrapolation of the mean values $\dot{\bar{a}}_2^*$ and $\dot{\bar{a}}_2^*$ can proceed in a variety of ways e.g. writing

$$\dot{\bar{a}}_2^x = \beta (\bar{a}_2^n - \bar{a}_2^{n-1}) \quad (11)$$

$$\bar{a}_2^x = \theta_1 \left(\bar{a}_2^n + \alpha (\bar{a}_2^n - \bar{a}_2^{n-1}) \right) + (1 - \theta) \bar{a}_2^n$$

Once \bar{a}_1^{n+1} is evaluated from equation (10) similar time marching process applied to Eq. (9b) gives

$$\begin{aligned} \bar{c}_{22} (\bar{a}_2^{n+1} - \bar{a}_2^n) + \Delta t K_2 (\theta_2 \bar{a}_2^{n+1} + (1 - \theta_2) \bar{a}_2^n) = \\ \Delta t \bar{f}_2 - \bar{c}_{21} (\bar{a}_1^{n+1} - \bar{a}_1^n) + \Delta t K_{21} (\theta_2 \bar{a}_1^{n+1} + (1 - \theta_2) \bar{a}_1^n) \end{aligned} \quad (12)$$

The 'splitting' of the vector of the unknown variables \bar{a} can be many fold and stability conditions for 'two way' split continue to apply. Thus the variables \bar{a} can be subdivided into a series of small partitions and matrices of size K_{nn} only then require solving at each step of the computation. Indeed the splitting can be continued to the individual components of \bar{a} thus achieving a fully explicit computation.

The order in which the various partitions are dealt with can be varied at alternate steps

Experiments with the procedure are continuing but preliminary tests show that

- (a) unconditional stability is readily achieved;
- (b) accuracy of computation can vary with the order in which the splitting is carried out.

It appears that a very general and useful computations tool is now available which can be used to reduce substantially the cost of time stepping computation and, if these should be used for iterative purposes, to reduce the cost of such solutions.

The SEE method can in a similar vein be applied to second order equations and its usefulness in that context is now being studied.

If the 'splitting' process is arranged to follow a hierarchical subdivision of variables discussed in the previous section greatly improved accuracy will be achieved for reasons there mentioned.

In Fig. 2, we show the SEE procedure applied as an explicit process in the solution of a one dimensional heat diffusion equation using two alternative sequencing of the partition.

In conclusion, we should mention that the time stepping algorithm developed by Truillo though formally resembling the process described here differ in many substantial respects (in particular, omitting the extrapolation process). [36][37]

REFERENCES

1. Zienkiewicz, O. C., and P.N. Godbole, 'Viscous incompressible flow with special reference to non-Newtonian (plastic) flow,' Ch. 2 from J.T. Oden, O.C. Zienkiewicz, R.H. Gallagher, and C. Taylor (eds.), Finite Elements in Fluids, Vol. I, J. Wiley and Sons, 1975.
2. Zienkiewicz, O.C., Constrained variational principles and penalty function methods in finite elements, Conf. on Numerical Solution of Differential Equations, Dundee, 1973, Lecture Notes in Mathematics Springer, 1973.
3. Christie, I., D. F. Griffiths, A. R. Mitchell and O.C. Zienkiewicz, 'Finite element methods for second order differential equations with significant first derivatives', Int. J. Num. Meth. Eng., 10, 1389-96, 1976.
4. Zienkiewicz, O. C. J.C. Heinrich, P.S. Huyakorn and A. R. Mitchell, 'An upwind finite element scheme for two dimensional convective transport equations', Int. J. Num. Meth. Eng., 11, 131-44, 1977.
5. Zienkiewicz, O. C., and J. C. Heinrich, 'The finite element method and convection problems in fluid mechanics Ch. 1 from Finite Elements in Fluids, Vol. III, J. Wiley and Sons, 1978.
6. Malkus, D. S. and T. J. R. Hughes, Mixed finite element methods - reduced and selective integration techniques: A unification of concepts, Comp. Meth. Appl. Mech and Eng., 15, p. 63-81, 1978.
7. Hughes, T.J.R., R.L. Taylor, J.F. Levy, 'High Reynolds number, steady incompressible flows by a finite element method' Ch. from Finite Elements in Fluids, Vol. III, J. Wiley and Sons, 1978.
8. Zienkiewicz, O.C., Jain, P.C. and E. Onate, 'Flow of solids during forming and extrusion: Some aspects of numerical solutions', Int. J. Solids Structures, 14, 15-38, 1978.
9. Nagtegaal, J.C., D.M. Parks and J.R. Rice, 'On numerically accurate finite element solutions in the fully plastic range', Comp. Meth. Appl. Mech and Eng., 4, 153-178, 1974.
10. Zienkiewicz, O.C. and E. Hinton, Reduced Integration, function smoothing and non-conformity in finite element analysis, J. Franklin Inst., 302, 443-61, 1976.
11. Gresho P. and R.L. Lee, Don't suppress the wiggles - they're telling you something, see ref. 12, 37-62.
12. Hughes, T.J.R., Ed., 'Finite element methods for convection dominated flows', Am. Soc. Mech. Eng., AMD-Vol. 34, Dec. 1979.
13. Hughes, T.J.R., A simple scheme for developing 'upwind' finite element, Int. J. Num. Meth. Eng. 12, 1359-65, 1978.
14. Hughes, T.J.R., and A. Brooks, A multidimensional upwind scheme with no cross wind diffusion, p. 19-36 of ref. 12.
15. Kelly, D., S. Nakazawa, and O.C. Zienkiewicz,
Meth. Eng., 1980. to be published, Int. J. Num.

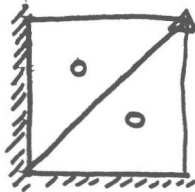
16. Zienkiewicz, O.C. and J.C. Heinrich, "A Unified Treatment of Steady-State Shallow Water and Two-Dimensional Navier-Stokes Equations. Finite Element Method Penalty Functions Approach". Comp. Meth. Appl. Mech. Eng. vol.17/18, 673-698(1979).
17. Heinrich, D.C. R.S. Marshall and O.C. Zienkiewicz, "Penalty Function Solution of Coupled Convective and Conductive Heat Transfer", Proceedings of the International Conference on Laminar and Turbulent Flow, Swansea, Wales, July 1978. Pentech Press, London (1978).
18. Bar-Yoseph, P., J.J. Blech and A. Solan, "Upwind Schemes for the Finite Element Solution of the Navier-Stokes Equations in Rotating Flow", Proceedings of the International Conference on Laminar and Turbulent Flow, Swansea, Wales, July 1978. Pentech Press, London (1978).
19. Hughes. T.J.R., W.K. Liu and A. Brooks, Finite element analysis of incompressible viscous flow by the penalty formulation, J. Comp. Physics, 1979.
20. Mote, C.D., Jr., Global-local finite element, In. J. Num. Meth. Eng. 3, 565-74, 1971.
21. Zienkiewicz, O.C., B.M. Irons, I.C. Scott and J.S. Campbell, Three Dimensional Stress Analysis, Proc. IUTAM Symp. on High Speed Computing of Elastic Structure, Liege, Belgium, 1, 413-32, 1971.
22. Wilson, E.L., Special Numerical and Computer techniques for the analysis of Finite element method Ch.1, 1-25 from Formulations and Computational algorithm in Finite Element Analysis, K.J. Bathe, J.T. Oden and W. Wunderlich editors, M.I.T. Press, 1977.
23. Wachspress, E.L. 'Two level finite element computations', Ch 31, 877-913, as ref. 22.
24. Peano, A.G., Hierarchies of conforming finite elements, Ph.D. thesis, Washington University, St. Louis, Missouri, 1975.
25. Peano, A.G., Hierarchies of conforming finite elements for plane elasticity in plate bending, Comp. and Math with Applications, 2, 211-229, 1976.
26. Szabo, B.A., Some recent developments in finite element analysis, Comp and Math with Applic., 5, 99-115, 1979.
27. Babuska, I., 'The self adaptive approach to the Finite Element Method,' from "The Mathematics of finite elements and application" II, edit, J. Whiteman, Acad. Press, 1976.
28. I. Babuska and W.C. Rheinboldt, A Posteriori error estimate for the finite element method, Tech. Rep. T.R. 581, University of Maryland, Sept. 1977.
29. Brandt, A. Multi level adaptive solution to Boundary Value problems, Math. Comp. 31, 333-91, 1977.
30. Nicolaidis, R.A., On some theoretical and practical aspects of multi-grid methods, Math. Comp., June 1979.
31. Douglas, J. and T. Dupont, Alternating direction Galerkin methods on rectangles, Proc. Symp. Num. Solution Partial Diff. Eq., ed. B. Hubbard, Acad. Press, 1971.
32. See above reference, (31), Galerkin Method for parabolic equations, SIAM J. Num. Anal. 575-626, 1970.

33. Hayes, L. J., Galerkin alternating direction methods for non-rectangular regions using patch approximations, CNA-134, Center of Numerical Analysis, Univ. of Texas, Austin, 1978.
34. Park, K.C., Partitioned Transient analysis procedure for coupled field problems to be published, J. Appl. Mech, 1980.
35. Park, K.C. and Fellippa, C.A., Partioned transient analysis procedures for Coupled field problems: Accuracy analysis, in preparation.
36. Zienkiewicz, O.C., 'The Finite Element Method, Ch. 21, Mc-Graw Hill, 1971.
37. Trujillo, D.M., An Unconditionally stable explicit algorithm for sturcture dynamics, Int. J. Num. Meth. Eng., 11, 1579-92, 1977.
38. Trujillo, D.M. and W. T. Busby, Finite element non-linear heat treatment using a stable explicit method, Paper B 2/12, SMIRT 4, San Francisco, 1977.

Performance of some 2-D elements for incompressibility⁹

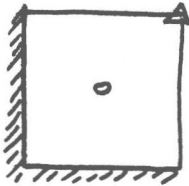
Δ 2 D.O.F For velocity

○ 1 constraint (integration point or D.O.F for p)



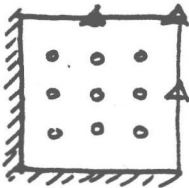
$$\beta = \frac{An}{Am} = \frac{2}{2} = 1$$

(COMPLETE LOCKING)
LINEAR TRIANGLE



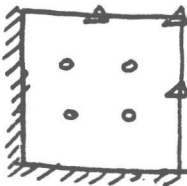
$$= \frac{2}{1} = 2$$

BILINEAR SELECTIVE
INTEGRATION



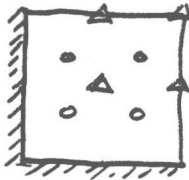
$$= \frac{3 \times 2}{9} = 0.67$$

FULLY INTEGRATED
SERENDIPITY
(COMPLETE LOCKING)



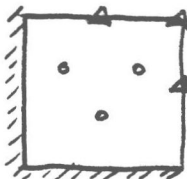
$$= \frac{3 \times 2}{9} = 1.5$$

REDUCED INTEGRATION
SERENDIPITY



$$= \frac{4 \times 2}{4} = 2.0$$

SELECTIVE INTEGRATION
LAGRANGIAN



$$= \frac{3 \times 2}{3} = 2.0$$

MIXED FORMULATION
LINEAR p

FIG 1

FIG 2. Temperature at $\frac{L}{2}$ of bar (20 linear elements)
 $x=0$ $T=1$

