

研究所・高普考叢書

單輸元送現操象作解題技巧

編著者 劉 弘 揚

曉園出版社
世界圖書出版公司



研究所·高普考叢書

單輸送現象操作解題技巧

編著者 劉 弘 揚

曉園出版社
北京·廣州·上海·西安

北京·广州·上海·西安

1992

单元操作输送现象解题技巧

刘弘扬 编

*

晓园出版社出版

世界图书出版公司北京公司重印

北京朝阳门内大街 137 号

北京中西印刷厂印刷

新华书店北京发行所发行 各地新华书店经售

*

1993 年 10 月第 一 版 开本：850×1168 1/32

1993 年 10 月第一次印刷 印张：16.75

印数：0001—500 字数：360 千字

ISBN：7-5062-1469-5/O·86

定价：11.00 元 (W_b9206/12)

世界图书出版公司 通过中华版权代理公司向晓园出版社

购得重印权

序　　言

單操輸送學為化工之基礎，亦為研究所、高考、化工技師檢覈及升技術學院之必考科目，所以想在各種考試中順利過關，單操輸送是必讀的重要科目。

坊間有關單操輸送之書籍均著重於理論之陳述，無法對解題有深一層之解說，尤其理論陳述繁雜，往往讀完後似懂非懂，遑論解題？筆者有鑒於此，特集數年來補習班教學經驗與資料，編成此書以針對各項考試之快速正確解題。

本書以歷年各項考試為準編寫而成，編列歷年各項考試中有出現之題型，並闡述解題技巧，使讀者在讀完本書後，對解題必有十足的信心，本書附有各校歷年研究所入學試題及解答，書後亦列出歷年高考試題以供參考。

筆者不佞，雖竭智窮慮，猶恐掛一漏萬，盼先進賢達不吝指正，俾作修正，以期更臻完美。

劉弘揚謹識

Contents

Part(I) Transport phenomena 1

(A) The simulation problems and solutions for momentum transfer 1

【 Example 1】 Laminar flow between two parallel flat plates 2

【 Excercise 】 Laminar flow in a narrow slit 8

【 Excercise 】 Performance of an electric dust collector 10

【 Example 2】 Laminar flow through a circular pipe 14

【 Excercise 】 Analysis of capillary flow meter 22

【 Excercise 】 Efflux time for tank with exit pipe 24

【 Example 3】 Tangential annular flow of a Newtonian fluid 26

【 Excercise 】 Velocity distribution in a stormer viscometer 28

【 Excercise 】 Velocity distribution between two rotating cylinders 28

【 Example 4】 Laminar flow an inclined plate 31

- [Excise] Drainage of liquids 34
- [Excise] Flow of a falling film with a moving boundary 36
- [Excise] Laminar flow of falling film on outside of a circular tube 38
- [Example 5] Laminar flow through an annulus 43
- [Excise] Annular flow with inner cylinder moving axially 48
- [Example 6] Radial flow between coaxial cylinder 51
- [Example 7] Acceleration effects in unsteady flow from a tank 55
- [Example 8] Momentum balance problem-jet in a pressurized tank 57
- [Example 9] Mass balance problem-unsteady state flow in a tank 60
- [Example 10] Unsteady state flow problem-two parallel plates 62
- [Excise] Flow near a wall suddenly set in motion 64
- [Example 11] Boundary layer flow problem-momentum integral equation and its application 67
- [Example 12] Ideal Flow (Potential flow) 74

(B) Simulation problems and solutions for heat transfer	87
【 Example 1】 Conduction through the hollow cylinder	87
【 Example 2】 Critical radius of insulation	89
[Excise] examine the insulation thickness on heat loss	91
【 Example 3】 Conduction with internal heat generation	92
Case (A) Heat generation in plane wall	92
Case (B) Heat generation in cylinder	94
【 Example 4】 The one-dimensional fin equation	97
[Excise] examine the fin effects	103
【 Example 5】 Two-dimensional steady state heat conduction with no heat generation	105
— solved by separation of variable method	107
【 Example 6】 Two-dimensional steady state heat conduction	109
【 Example 7】 One-dimensional unsteady state heat conduction	113
Case(1) Lumped-system analysis for $Bi \ll 0.1$	114
Case(2) Distribution -system for $Bi \gg 0.1$	117
【 Example 8】 Internal laminar forced convective flow	126
Case(1) Heat transfer in couette flow	126

Case(2) Temperature profile for laminar flow in tubes	133
【 Example 9】 External laminar forced convective flow	137
【 Example 10】 External turbulent forced convective flow	141
【 Example 11】 Heat transfer from a wall to a falling film	149
(C) Simulation problems and solutions for mass transfer 154	
1 Steady-state molecular diffusion in gas	154
【 Example 1】 Pseudo-steady-state diffusion through a stagnant gas film	158
【 Example 2】 Steady-state diffusion from a sphere	162
【 Example 3】 Diffusion from a droplet into a quiescent gas	164
【 Example 4】 Diffusion through a stagnant liquid film	166
2 Diffusion with chemical reaction	168
【 Example 5】 Diffusion with heterogeneous chemical reaction	171
【 Example 6】 Determine the rate of combustion of coal	175
【 Example 7】 Diffusion with homogeneous chemical reaction	179

【Example 8】 Effectiveness factor for thin disks	187
3 Diffusion into a falling liquid film	188
【Example 9】 Solid dissolution into a falling film	194
4 Unsteady-state molecular diffusion	199
【Example 10】 Transient diffusion in a semi-infinite medium	202
5 Mass transfer coefficient	205
【Example 11】 NH ₃ , absorption in a wetted-wall tower	207
〔Excise〕 Mass transfer in an absorption tower	208
〔Excise〕 Mass transfer in a wetted-column	210
【Example 12】 Mass transfer in a distillation tower	213
6 Mass transfer in the laminar flow	217
【Example 13】 Mass transfer in the boundary layer	219
【Example 14】 Chilton-colburn analogy problem	220
【Example 15】 Heat and mass transfer analogy	222
Part(II) Unit operation	225
(1) The calculation of heat transfer equipment-evaporator & heat exchanger	225
(2) The vapor-liquid separation process-distillation	234
(3) The gas-liquid separation process-absorption & desorption	249
(4) Liquid-solid separation process-leaching	260

- (5) Water-air separation process-humidification dehumidification **266**
- (6) Water-solid separation process-drying **280**
- (7) Particle-fluid separation process-settling **288**
- (8) Flow measurement and pump **298**

Part(III) 歷屆試題詳解 323

[台大 61 ~ 75 年單操輸送研究所入學考題及解答] **323**

[清大 63 ~ 71 年單操輸送研究所入學試題及解答] **439**

[附錄 47 ~ 72 年化工歷屆高考單操輸送考題] **509**

Part(1) Transport phenomena

(A) The Simulation Problems and Solutions for Momentum transfer

The Problem-Solving Approach :

(→) Extracting the N-S Eq method

(1) Carefully read the problem statement

(2) Choose a coordination system (rectangular, Cylindrical and Spherical)

(3) Sketch system diagam

(4) Extract the describing N-S Diff Eqs

(5) Set up BC & IC

(6) Solve the Eqs, Subject to BC & IC

(7) Analyse the Results

(↔) Shell-balance method Analysis

(1) Choose a Shell size

(2) Force Balance

(3) Shear force related to velocity gradient

(4) Velocity distribution Solved (B.C Known)

(5) Average or Max. velocity

(6) Drag force

Example 1.

Steady state of laminar flow for
Newton's Incompressible fluids between two parallel flat
plates find

1 Velocity profile ?

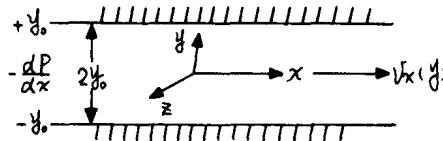
2 Pressure drop per unit length of the conduit $\frac{-dp}{dx} = ?$

3 $V_{x \max} = ?$

4. $\langle V_{x \text{ ave}} \rangle = ?$

5 $Q = ?$

¶] By Simplifying Navier-Stokes eq



from eq of continuity $\nabla \cdot \vec{v} = 0$

$$\frac{\partial V_x}{\partial x} + \frac{\partial V_y}{\partial y} + \frac{\partial V_z}{\partial z} = 0 \Rightarrow \frac{\partial V_x}{\partial x} = 0 \Rightarrow \frac{\partial^2 V_x}{\partial x^2} = 0$$

$$\rho \frac{D\vec{v}}{Dt} = -\nabla P + \rho \vec{g} + \mu \nabla^2 \vec{v}$$

$$\nabla = \frac{\partial}{\partial x} \vec{i} + \frac{\partial}{\partial y} \vec{j} + \frac{\partial}{\partial z} \vec{k}, \vec{v} = V_x \vec{i} + V_y \vec{j} + V_z \vec{k}$$

from Eq of motion x-compoment

$$\frac{\rho}{g_c} \left(\frac{\partial V_x^0}{\partial t} + V_x \frac{\partial V_x^0}{\partial x} + V_y \frac{\partial V_x^0}{\partial y} + V_z \frac{\partial V_x^0}{\partial z} \right) = -\frac{\partial P}{\partial x}$$

$$\mu \left(\frac{\partial^2 V_x^0}{\partial x^2} + \frac{\partial^2 V_x^0}{\partial y^2} + \frac{\partial^2 V_x^0}{\partial z^2} \right) + \frac{\rho}{g_c} g_x$$

$$\Rightarrow \frac{\partial P}{\partial x} = \mu \frac{\partial^2 V_x}{\partial y^2} \Rightarrow \frac{dP}{dx} = \mu \frac{d^2 V_x}{dy^2} = \text{const}$$

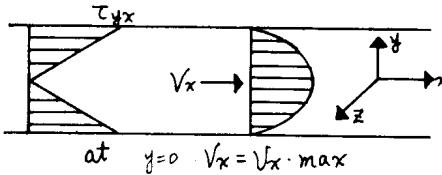
$$\text{B.C} \begin{cases} (1) y = \pm y_0 & , V_x = 0 \\ (2) y = 0 & V_x = \text{finite} \Rightarrow \frac{dV_x}{dy} = 0 \end{cases}$$

$$\frac{dv_x}{dy} = \frac{1}{\mu} \frac{dP}{dx} y + C_1 \quad \text{with } B \cdot C(2) \Rightarrow C_1 = 0$$

$$\frac{dv_x}{dy} = \frac{1}{\mu} \frac{dP}{dx} y \Rightarrow \text{integrate} \Rightarrow V_x = \frac{1}{\mu} \frac{dP}{dx} \cdot \frac{1}{2} y^2 + C_2$$

$$\text{using } B \cdot C(1) \Rightarrow C_2 = -\frac{1}{\mu} \frac{dP}{dx} \cdot \frac{1}{2} \cdot y_0^2$$

1 $\Rightarrow V_x = \frac{1}{\mu} \frac{dP}{dx} \cdot \frac{1}{2} (y^2 - y_0^2) \leftarrow V_x \text{ 對 } y \text{ 為一拋物線}$



at $y=0 \quad V_x = V_{x \max}$

$$2 \Rightarrow V_{x \max} = \frac{1}{-2 \mu} \frac{dP}{dx} y_0^2$$

$$\Rightarrow V_x = \frac{1}{-2 \mu} \frac{dP}{dx} y_0^2 [1 - (\frac{y}{y_0})^2]$$

$$= V_{x \max} [1 - (\frac{y}{y_0})^2]$$

$$3 \langle V_{x \text{ ave}} \rangle = \frac{\int_{-y_0}^{y_0} \int_0^w V_x dy dz}{\int_{-y_0}^{y_0} \int_0^w dy dz} = \frac{Q}{A}$$

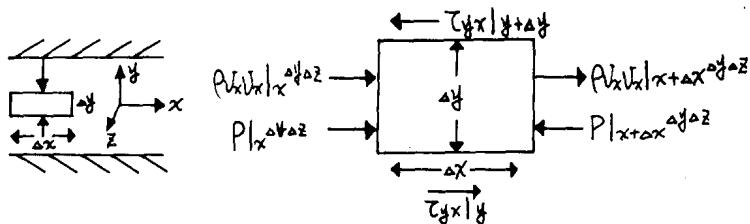
$$4. Q = \int dQ = \int V_x dA = \int_{-y_0}^{y_0} V_{x \max} [1 - (\frac{y}{y_0})^2] dy \text{ (per unit width)}$$

$$= \frac{1}{-2 \mu} \frac{dP}{dx} \int_{-y_0}^{y_0} (y_0^2 - y^2) dy = \frac{1}{-2 \mu} \frac{dP}{dx} \frac{4}{3} y_0^3$$

$$= \frac{-2}{3 \mu} \frac{dP}{dx} y_0^3 = \frac{4}{3} V_{x \max} y_0$$

$$\langle V_{x \text{ ave}} \rangle = \frac{Q}{A} = \frac{\frac{4}{3} V_{x \max} y_0}{2 y_0} = \frac{2}{3} V_{x \max}$$

(-) By shell Balance :



Momentum Balance : In - Out + $\sum F^z$ = Accum

(∵ fully developed)

$$\rho (Vv|_x - vV|_{x+\Delta x}) \Delta y \Delta z \leftarrow \text{convective term}$$

$$+ (\tau_{yx}|_y - \tau_{yx}|_{y+\Delta y}) \Delta x \Delta z \leftarrow \text{shear force term}$$

$$+ (P|_x - P|_{x+\Delta x}) \Delta y \Delta z \leftarrow \text{pressure force term}$$

$$= abc \quad (\because s.s)$$

$$\Rightarrow (\tau_{yx}|_y - \tau_{yx}|_{y+\Delta y}) \Delta x \Delta z + (P|_x - P|_{x+\Delta x}) \Delta y \Delta z = 0$$

$$\div \Delta x \Delta y \Delta z$$

$$\Rightarrow \frac{\tau_{yx}|_y - \tau_{yx}|_{y+\Delta y}}{\Delta y} + \frac{P|_x - P|_{x+\Delta x}}{\Delta x} = 0$$

take limit $\Delta x \rightarrow 0 \quad \Delta y \rightarrow 0$

$$\Rightarrow \frac{d\tau_{yx}}{dy} + \frac{dP}{dx} = 0$$

Because it. is a Newton's fluid

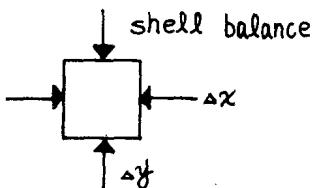
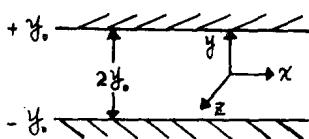
$$\tau_{yx} = -\mu \frac{dV_x}{dy}$$

$$\Rightarrow \frac{d\tau_{yx}}{dy} = -\mu \frac{d^2V_x}{dy^2} = -\frac{dP}{dx}$$

$$\Rightarrow \frac{dP}{dx} = \mu \frac{d^2V_x}{dy^2}$$

just the same the result By N-S Eq

Detail discussion:



$$\frac{1}{\mu} \frac{d^2 V_x}{dy^2} = \frac{dP}{dx}$$

$$\Rightarrow V_x = \frac{1}{\mu} \frac{dP}{dx} \frac{y^2}{2} + C_1 y + C_2 \rightarrow (A)$$

B · C discussion

(1) If both plates are stationary

$$V_x = (V_x)_{\text{max}} \left[1 - \left(\frac{y}{y_0} \right)^2 \right]$$

(2) A sufficient force is applied to the upper plate to maintain a velocity V_0

$$\begin{aligned} & (1) y = -y_0, \quad V_x = 0 \\ & \text{B · C} \{ \\ & (2) y = y_0, \quad V_x = V_0 \end{aligned}$$

Substituting B · C into eq(A), We get C_1, C_2

$$0 = \frac{1}{2\mu} \frac{dP}{dx} y_0^2 + C_1(-y_0) + C_2$$

$$V_0 = \frac{1}{2\mu} \frac{dP}{dx} y_0^2 + C_1(y_0) + C_2$$

$$\text{聯立解: } C_1 = \frac{V_0}{2y_0}, \quad C_2 = \frac{V_0}{2} - \frac{1}{2\mu} \frac{dP}{dx} y_0^2$$

$$\begin{aligned} V_x &= \frac{1}{2\mu} \frac{dP}{dx} y^2 + \frac{V_0}{2y_0} y + \frac{V_0}{2} - \frac{1}{2\mu} \frac{dP}{dx} y_0^2 \\ &= \frac{1}{2\mu} \left(-\frac{dP}{dx} \right) (y_0^2 - y^2) + \frac{V_0}{2} \left(\frac{y}{y_0} + 1 \right) \end{aligned}$$

(3) If the Lower plate is set in motion $V = V_0^*$

$$\begin{aligned} & (1) y = -y_0 \quad V_x = V_0^* \\ & \text{B · C} \{ \\ & (2) y = y_0 \quad V_x = 0 \end{aligned}$$

代入 eq. (A) 聯立解 C_1, C_2

$$C_1 = \frac{-V_0^*}{2y_0}$$

$$C_2 = \frac{V_0^*}{2} - \frac{1}{2\mu} \frac{dP}{dx} y_0^2$$

$$\Rightarrow V_x = \frac{1}{2\mu} \frac{dP}{dx} y^2 - \frac{V_0^*}{2y_0} y + \frac{V_0^*}{2} - \frac{1}{2\mu} \frac{dP}{dx} y_0^2$$

$$= \frac{1}{2\mu} \left(-\frac{dP}{dx} \right) (y_0^2 - y^2) + \frac{V_0^*}{2} \left(1 - \frac{y}{y_0} \right)$$

(4) If Both plate are moving

upper plate $= V_0$

Lower plate $= V_0^*$

a. if the direction is the same.

$$B \cdot C \begin{cases} (1) y = -y_0 & V_x = V_0^* \\ (2) y = y_0 & V_x = V_0 \end{cases}$$

代入 eq(A) 联立解

$$C_1 = \frac{V_0 - V_0^*}{2y_0}$$

$$C_2 = \frac{V_0^* + V_0}{2} - \frac{1}{2\mu} \frac{dP}{dx} y_0^2$$

$$\Rightarrow V_x = \frac{1}{2\mu} \left(-\frac{dP}{dx} \right) (y_0^2 - y^2) + \frac{y}{2y_0} (V_0 + V_0^*) + \frac{V_0 + V_0^*}{2}$$

b. if the direction is reversed

$$B \cdot C \begin{cases} (1) y = -y_0 & V_x = -V_0^* \\ (2) y = y_0 & V_x = V_0 \end{cases}$$

$$C_1 = \frac{1}{2y_0} (V_0 + V_0^*)$$

$$C_2 = \frac{V_0 - V_0^*}{2} - \frac{1}{2\mu} \frac{dP}{dx} y_0^2$$

$$\Rightarrow V_x = \frac{1}{2\mu} \left(-\frac{dP}{dx} \right) (y_0^2 - y^2) + \frac{y}{y_0} (V_0 + V_0^*) + \frac{V_0 - V_0^*}{2}$$

(5) (Power Law) applied for Non-Newtonian fluid between parallel plate

$$B \cdot C \begin{cases} (1) y = \pm y_0, V_x = 0 \\ (2) y = 0, \tau_{yx} = 0 \end{cases}$$

$$\frac{d\tau_{yx}}{dy} = - \left(\frac{dP}{dx} \right) \Rightarrow \tau_{yx} = \left(- \frac{dP}{dx} \right) y + C_1$$

$$B \cdot C \quad (2) \Rightarrow C_1 = 0 \Rightarrow \tau_{yx} = \left(- \frac{dP}{dx} \right) y$$

in Power Law fluid

$$\tau_{yx} = m \left(- \frac{dV_x}{dy} \right)^n = \left(- \frac{dP}{dx} \right) y$$

$$\Rightarrow - \frac{dV_x}{dy} = \left[\frac{1}{m} \left(- \frac{dP}{dx} \right) y \right]^{1/n}$$

integral

$$\Rightarrow - V_x = \int \left[\frac{1}{m} \left(- \frac{dP}{dx} \right) \right]^{1/n} y^{1/n} dy$$

$$= \left[\frac{1}{m} \left(- \frac{dP}{dx} \right) \right]^{1/n} \int y^{1/n} dy$$

$$= \left[\frac{1}{m} \left(- \frac{dP}{dx} \right) \right]^{1/n} \left[\frac{y^{1/n+1}}{1+\frac{1}{n}} + C_2 \right]$$

$$= \left[\frac{1}{m} \left(- \frac{dP}{dx} \right) \right]^{1/n} \left(\frac{n}{n+1} y^{1/n+1} + C_2 \right)$$

$$B \cdot C \quad (1) \Rightarrow C_2 = - \frac{n}{n+1} y_0^{-\frac{1}{n}+1}$$

$$\Rightarrow V_x = \underbrace{\left[\frac{1}{m} \left(- \frac{dP}{dx} \right) \right]^{1/n} \left(\frac{n}{n+1} y_0^{-\frac{1}{n}+1} \right)}_{(V_x)_{max} \text{ at } y=0} [1 - \left(\frac{y}{y_0} \right)^{\frac{n+1}{n}}]$$

$$\Rightarrow V_x = (V_x)_{max} [1 - \left(\frac{y}{y_0} \right)^{\frac{n+1}{n}}]$$

$$\langle V_x \rangle = \frac{\int_0^w \int_{-y_0}^{y_0} V_x dy dz}{\int_0^w \int_{-y_0}^{y_0} dy dz} = \frac{2w \int_0^{y_0} [(V_x)_{max} (1 - (\frac{y}{y_0})^{\frac{n+1}{n}})] dy}{2y_0 \cdot w}$$

$$= (V_x)_{max} \int_0^{y_0} [1 - (\frac{y}{y_0})^{\frac{n+1}{n}}] d(\frac{y}{y_0})$$