

MINERAL PROCESSING DESIGN AND OPERATIONS

An Introduction

Second Edition

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Ashok Gupta

Retired Head of Metallurgy Department WA School of Mines, Kalgoorlie Curtin University of Technology, Western Australia

Denis Yan

Consulting Metallurgist Minerals Engineering Technical Services Perth, Western Australia



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Radarweg 29, PO Box 211, 1000 AE Amsterdam, Netherlands The Boulevard, Langford Lane, Kidlington, Oxford OX5 1GB, UK 50 Hampshire Street, 5th Floor, Cambridge, MA 02139, USA

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Mineral Processing Design and Operations

Dedicated to all students interested in the Science and Technology of Mineral Processing

And especially to the memory of late dear Elmie Yan and also to Chitra Gupta for her patience and forbearance while preparing this manuscript.

Preface to the Second Edition

Demand for the first edition of this book prompted us to revise, enlarge and update it. The format of the second edition is in keeping with the first edition. The logic of presentation remains the same.

This edition includes additional chapters on stirrer mills and magnetic separation. The stirred mills for ultrafine grinding of minerals which were developed in the last three decades are described and discussed in detail. These are now being extensively used in large-scale operating circuits for enhanced recovery of minerals from their ore body. Magnetic, conductive and electromagnetic forces for the recovery of minerals with natural or induced magnetic, conducting and semi-conducting properties are a common beneficiation technique particularly in the mineral sands and iron ore industries. The basic elements of atomic theory that help to understand magnetic forces in minerals are explained and the designing of equipment as well as separation processes of magnetic from non-magnetic minerals based on these theories are described.

The objective of the book remains the same as that of the first edition which is to help students interested in processing minerals to economically liberate and concentrate them for down-stream extraction processes. To understand the unit as well as the integrated processes the subject has been treated somewhat mathematically with the view to apply them in actual process designs and operations. In so doing it is expected that the book would suit students from the disciplines of Metallurgy, Chemical Engineering, Process Engineering and to a limited extent Electronics Engineering, who are engaged in the beneficiation of minerals and who are at under-graduate, graduate and post-graduate levels of study. Some data provided in the appendix is expected to aid in calculations of designing and plant operations. Solutions to simple and common plant problems are provided.

In writing this second edition of the book we offer our thanks to the reviewers who offered help and guidance to improve on the first edition. Also our renewed thanks to Dr Lutz Elber and Dr Halit Eren for their help and contribution in writing Chapter 20 on Process Control. We would also like to thank the various state and university libraries who helped in supplying

up-to-date information. We would especially like to thank our publishers who prompted us to write this edition; especially Dr Kostakitas, Anitha Sivaraj and Christine McElvenny who helped us to produce this edition.

Ashok Gupta and Denis Yan

Perth, Western Australia, November 2015

A general convention used in this text is to use a subscript to describe the state of the quantity, for example, S for solid, L for liquid, A for air, SL or P for slurry or pulp, M for mass and V for volume. A subscript in brackets generally refers to the stream, for example, (O) for overflow, (U) for underflow, (F) for feed, (C) for concentrate and (T) for tailing. There are a number of additions to this convention which are listed later.

-		
<u>a</u>	a constant	
а	amplitude	m
a_{P}	particle acceleration	m/s²
a_{m}	media acceleration	m/s ²
A	a constant	_
A	aperture	microns
A	area	m²
$A_{\rm C}$	cross-sectional area	m ²
$A_{\rm E}$	effective area	m ²
$A_{\rm EFF}$	areal efficiency factor	
A_{i}	abrasion index	_
A _{ij}	assay of particles in the ith size and jth density fractions	=
$A_{\rm m}$	cross-sectional area of media	m ²
A_{M}	assay of mineral	%, g/t, ppm
$A_{\rm O}$	open area	%
A _{OE}	effective open area	%
A _p	cross-sectional area of particle	m²
\mathbf{A}_{U}	underflow area	m ²
)	a constant	_
)	Rosin-Rammler distribution parameter	
3	magnetic induction, flux density	Wb/m², T
30	magnetic induction at the drum surface	Wb/m², T
$B_{\rm S}$	magnetization saturation	T
B_{ij}	breakage distribution function	_
2	a constant	_
C	a constant	æ

2	Curie constant	-
2 2	circulation ratio or load	_
,	concentration (mass solid/volume of slurry)	kg/m³
A	concentration of air	kg/m³
C	average concentration of solids in the compression zone	kg/m³
CRIT	critical concentration	kg/m³
	drag coefficient	-
P F F F F F F F F F F F F F F F F F F F	correction factor	
7	concentration of the feed (mass of solid/volume of slurry)	kg/m³
F	concentration of the rece (mass of softer volume of starry)	kg/m³
7	initial concentration (mass of solid/volume of slurry)	kg/m³
	maximum concentration (mass of solid/volume of slurry)	kg/m³
MAX		%
MS(F)	concentration of solids in the feed by mass	70
S(C)	concentration of solid (C = concentrate, $F = feed$, $T = tail$, $f = froth$,	=
4	P = pulp) solids concentration in the underflow (O = overflow, F = feed)	%
S(U)		
T T T	concentration at time t (mass of solid/volume of slurry)	kg/m³
T	correction factor or transfer coefficient	1 / 3
U	concentration of the underflow (mass of solid/volume of slurry)	kg/m³
VS(F)	concentration of solids in the feed by volume	%
	concentration criterion	
CI	confidence interval	
CR	confidence range	
CV	coefficient of variation	
C_{∞}	concentration at infinite time	kg/m³
d	a constant	
d	particle size, diameter	m
d_{32}	Sauter mean diameter	m
d_{50}, d_{50C}	cut or separation size, corrected cut size	microns
d_{B}	ball diameter	cm, m
$d_{\rm C}$	cylpeb diameter	mm
$d_{ m cutter}$	cutter opening	m
d_{d}	disc diameter	m
d_{F}	63.2% passing size in the feed	m
d_{H}	diameter of helix stirrer	m
$d_{\rm L}$	liberation size	m
$d_{ m m}$	media diameter	m
d_{M}	mill diameter	m
d_{MAX}	largest dimension	m
d_{MIN}	smallest dimension	m
d_{MID}	mid-range dimension	m
$d_{\rm N}$	nominal diameter	m
$d_{\rm w}$	wire diameter	m

D	discharge mass ratio (liquid/solid)	
D	displacement, distance, diameter	m
D^*	dimensionless parameter	
$D_{\rm C}$	cyclone diameter	m
$D_{\rm I}$	inlet diameter	m
$D_{\rm O}$	overflow diameter	m
D_{U}	underflow diameter	m
e	a constant	_
e^+, e^-	quantity of charge	C
E	energy	kWh
E	potential difference	V
$\overline{E_{\mathrm{B}}}$	energy of rebound	Wh
$\overline{E_{C}}$	corrected partition coefficient	<u>-</u> 1
$\overline{E_{G}}$	specific grinding energy	kWh/t
$\overline{E_{\mathrm{i}}}$	partition coefficient of size $i = recovery of size i$ in the U/F	_
$\overline{E_o}$	uniform electric filed strength	N/C, V/m
$\overline{E_{\rm O}}$	efficiency based on oversize	_
$E_{\rm p}$	Ecart probability, probable error of separation	_
$\overline{E_{\mathrm{S}}}$	surface electric field intensity	N/C, V/m
$\overline{E_{\mathrm{T}}}$	total energy	kW
$\overline{E_{U}}$	efficiency based on undersize	
$\frac{1}{f}$	a constant	-
$f(J_{\mathrm{B}})$	ball load-power function	-
$f_{\rm P}, f_{\rm F}$	function relating to the order of kinetics for pulp and froth	_
$\frac{f(r)}{f(r)}$	ball wear rate	kg/h
f(s)	suspensoid factor	_
f_i	mass fraction of size i in the circuit feed	_
F_{80}	80% passing size of feed	microns
$\frac{1}{F}$	feed size	cm, microns
\overline{F}	floats at SG	_
\overline{F}	froth stability factor	
F	feed mass ratio (liquid/solid)	
$\overline{F_{\mathrm{B}}}$	Rowland ball size factor	_
$F_{\rm B}$	buoyancy force	N
$\overline{F_{\rm C}}$	Bond mill factor	_
$F_{\rm C}$	centrifugal force	N
$\overline{F_d}$	diffusion force	N
$F_{\rm D}$	drag force	N
$\overline{F_{\rm e}}$	electrostatic force	N
$F_{\rm E}$	electric dipole force	N
$F_{\rm f}$	frictional force	N
F_{g}	gravitational force	N
$F_{\rm gt}$	tangential component of gravitational force	N
gt		

$F_{\rm G}$	correction factor for extra fineness of grind	:-
F	settling factor	
T _i	inertia or centrifugal force	N
7	electric field gradient force	N
I M	magnetic force	N
M MR	radial component of magnetic force	N
7os	correction factor for oversized feed	
OS R	correction factor for low reduction ratio	
r S	mass flow rate	kg/s, t/h
rs rs	Bond slurry or slump factor	- Kg/5, UII
	viscous force (drag)	N
7 v	gravitational constant (9.81)	m/s ²
<u>;</u>	grade (assay)	%, g/t, ppm
	net grams of undersize per revolution	
G, G_{bp}		g/rev
	grinding parameter of circulating load	
ΔG	free energy	J
h	parameter = x/σ	
h_1, h_1^*	distances within the conical section of a mill	M
Н	hindrance factor	
Н	height	m, cm
Н	magnetic field strength	A/m
$H_{\rm B}$	height of rebound pendulum	m
H_{B}	height of bed	m
$H_{\rm C}$	height of ball charge	m
$H_{\rm C}$	height of the start of the critical zone in sedimentation	m
H_{OF}	height of the clarification zone (overflow)	m
H_{R}	height of rest	m
$H_{\rm S}$	hindered settling factor	_
$H_{\rm t}$	height at time t	m
H_{U}	mudline height at the underflow concentration	m
H_{∞}	height after infinite time	m
i	current	A
I	impact crushing strength	kg.m/mm
I	imperfection	_
$J_{ m B}$	fraction of mill volume occupied by bulk ball charge	
$J_{ m C}$	fraction of mill volume in cylindrical section occupied by balls and c	coarse –
	ore	
$J_{ m G}$	superficial gas velocity	m/s
J_{R}	fraction of mill volume occupied by bulk rock charge	
$J_{\rm p}$	fraction of mill volume filled by the pulp/slurry	
k	constant	
K	Boltzmann's constant, 1.381×10^{-23}	J/K
$k_{\rm A}, k_{\rm A}$	rate constant for air removal via froth and tailings respectively	

$k_{\rm C}, k_{{ m C}50}$	screening rate constant, crowded condition, normal and half size	t/h/m²
k_e	Coulomb's constant, 8.99×10^9	Nm ² /C ²
$k_{\rm F}, k_{\rm S}$	rate constant for fast and slow component respectively	min ⁻¹
r _i	comminution coefficient of fraction coarser that ith screen	=
$k_{\rm S}, k_{\rm S50}$	screening rate constant, separated condition, normal and half size	m^{-1}
(constant	-
~	ratio of vertical to horizontal media pressure	_
(flatness factor	_
D0	material constant	_
Œ	kinetic energy	kW
,	length	m
'A	aperture size	m
'AE	effective aperture	m
C	length of cyclone	m
$L_{\rm CYL}, L_{\rm CONE}$	length of cylindrical and cone sections	m
D	drum radius	m
E	distance between electrodes	m
EFF	effective grinding length	m
F	Nordberg loading factor	_
L_{MAX}	minimum and maximum crusher set	m
'r	distance from centre of rotation	m
Т	crusher throw	m
V	length of vortex finder	m
VF	length from end of vortex finder to apex of a cyclone	m
ı	moisture (wet mass/dry mass)	-
ı	mass	g
1	mineralogical factor	kg/m³
$l_{i(U)}$	mass of size i in the underflow (F = feed)	kg
l _k	mass fraction of makeup balls of size k	_
u(r)	cumulative mass fraction of balls less than size r	=
l_{T}	mass rate of ball replacement per unit mass of balls	kg/h.t
U(F)	mass fraction of undersize in the feed	
l _{U(O)}	mass fraction of undersize in the oversize	
U(U)	mass fraction of undersize in the undersize	_
1	magnetization	A/m
ſ	mass	kg, t
1	mass of new feed	g
В	mass of block	kg
В	mass of balls	kg
l _c	mill capacity	t/h
I _C	mass of crushing weight	kg
I _F	mass of feed	t
1 _F	mass of fluid	kg
Г	000000000000000000000000000000000000000	0

M_{FT}	mass of floats	kg, t
$M_{\scriptscriptstyle m F}$	Nordberg mill factor	
$M_{\rm i}$	mass/mass fraction of ith increment	kg, t
M_{oi}	cumulative mass fraction retained on ith screen at zero time	_
M_{ij}	mass percent of the ith size fraction and jth density fraction	%
$M_{ m MIN}$	minimum mass of sample required	kg, t
$M_{\rm p}$	mass of particle	kg
M_r	cumulative mass fraction of balls of size r in the charge	_
$M_{\rm R}$	mass of rock	kg
$M_{\rm R}$	mass fraction of rock to total charge (rock + water)	_
$M_{\rm S}$	mass of striking pendulum	kg
$M_{\rm S}$	mass of solid	kg, t
$M_{S(f)}$	mass of solid in froth	_
$M_{S(F)}, S(C), S(T)$	mass of solid feed, concentrate and tailing respectively	kg, t
$M_{\rm SK}$	mass of sinks	kg, t
$M_{S(P)}$	mass of solid in the pulp	kg, t
M_{W}	mass of water	kg, t
$\Delta M(t)$	mass of top size particle	kg, t
	number of revolutions/min	min ⁻¹
n	number of increments, measurements	
n		
n	order of rate equation	
n ()	number of unpaired electrons	_
n(r)	cumulative number fraction of balls of size less than r	
n _S	number of sub-lots	
N	number of mill revolutions	
N	revolutions per second	S ⁻¹
N	number of strokes/min	min ⁻¹
N	number	
N	concentration of ions per unit volume	m ⁻³
<i>N</i> '	number of particles/gram	g ⁻¹
$N_{\rm o}$	Avogado's number, molecules/mol	-
$N_{\rm L}$	number of presentations per unit length	m ⁻¹
$N_{\rm m}$	number of media per unit volume	m ⁻³
$N_{\rm S}$	number of stress events	
<u>o</u> i	mass fraction of size <i>i</i> in the overflow	
p	Probability	
<u>P</u> i	mass fraction of size <i>i</i> in the new feed	=
P	product size	microns
P	proportion of particles	=
P	pressure	Pa
P	powers roundness factor	
P	jig power	W
P	JKSimFloat ore floatability parameter	_

P	probability	=
P_{80}	80% passing size of product	microns
$P_{\rm A}, P_{\rm C}, P_{\rm E}, P_{\rm F}$	probability of adherence, collision, emergence, froth recovery	=
$P_{\rm CON}$	power of the conical part of a mill	kW
P_{CYL}	power for the cylindrical part of a mill	kW
P_{D}	particle distribution factor	
$\overline{P_{\mathrm{F}}}$	pinning factor	_
$P_{\rm g}$	pressure due to gravity	N/m ²
$P_{\rm G}$	proportion of gangue particles	_
P_{ij}	proportion of particles in the <i>i</i> th size and <i>j</i> th density fractions	=
$P_{\rm L}$	liberation factor	
$P_{\rm m}$	grinding media pressure	N/m²
P_{M}	proportion of mineral particles	_
P_{M}	mill power	kW
$P_{ m NET}$	net mill power draw	kW
$P_{ m NL}$	no load power	kW
$P_{\rm OS}$	period of oscillation	S
$P_{\rm R}$	relative mill power	
$P_{\rm S}$	particle shape factor	_
$P_{\rm S}$	power at the mill shaft	kW
PE	potential energy	kW
ΔP	pressure drop	kPa
9	alternate binomial probability = $1 - p$	
Q	capacity	t/h
Q_1, Q_2	point charges	С
$Q_{\rm B}$	makeup ball addition rate	kg/day
Q_{B}	basic feed rate (capacity)	t/h/m
$Q_{ ext{MS(O)}}$	flowrate of solids by mass in the overflow ($U = U/F$, $F = feed$)	t/h
$Q_{MS(C)}$	mass flow of solid in concentrate	t/h
$Q_{M(F)}$	capacity, of feed slurry by mass	t/h
Q_0	tonnage of oversize material	t/h
Q_{U}	capacity of the underflow	t/h
$Q_{\text{V(C)},\text{ (T)},\text{ (F)}}$	flowrate by volume in concentrate, tailing and feed respectively	m³/h
$Q_{V(f)}$	flowrate by volume in the froth	m³/h
$Q_{\rm VL(O)}$	capacity (flowrate) of liquid by volume in the overflow (U = underflow, F = feed)	m³/h
$Q_{V(O)}$	flowrate by volume of overflow (pulp) (U = underflow)	m³/h
$Q_{\text{VOL(U)}}$	flowrate by volume of entrained overflow liquid in the U/F	m³/h
$Q_{\text{VOP(U)}}$	flowrate by volume of entrained overflow pulp in the U/F	m³/h
$2_{\text{VOS(U)}}$	flowrate by volume of entrained overflow solids in the U/F	m³/h
$Q_{\rm VS(O)}$	flowrate by volume of solids in the overflow ($U = U/F$, $F = feed$)	m³/h
$Q_{\rm W}$	ball wear rate	mm/h
r	radius	m

	ratio of rate constants = $k_A/(k_A + k_A)$	_
0	fraction of test screen oversize	_
r_1, r_2	radius within the conical section of a mill	m
p	particle radius	m
v	vector radius	m
?	radius	m
?	recovery	%
?	reduction ratio	
2	the mean radial position of the active part of the charge	m
?'	fractional recovery, with respect to the feed to the first cell	=
ξ'	mass of test screen oversize after grinding	g
R_1, R_2, R_3	Dietrich coefficients	-
$R_{\rm C}$	radius of cone at a distance L_i from cylindrical section	m
Re_A, Re_C	Reynolds number in the apex and cone section respectively	_
Re_{p}	particle Reynolds number	
R _F	froth recovery factor	
R_i	radial distance to the inner surface of the active charge	m
R _o	mass of test screen oversize before grinding	g
$R_{\rm p}$	radial distance of particle from the centre of a mill	m
R _{RO}	optimum reduction ratio	
R_{T}	radius at the mill trunnion	m
$R_{\rm V}$	recovery of feed volume to the underflow	
R_{∞}	recovery at infinite time	
	speed	m/s
S S	sinks at SG	_
S	surface area	m ²
S	spacing, distance	m
S*	dimensionless parameter	-
$S_{\rm B}$	surface area of ball	m ²
$S_{\rm B}$	bubble surface area flux	s^{-1}
S_F	Nordberg speed factor	_
S_{i}	breakage rate function	min ⁻¹
SE	stress energy	Nm
SE_{Vb}	specific energy per unit volume at level b	Nm/m³
SG, SG _s	specific gravity, specific gravity of solid	=
SI	stress intensity of grinding media	Nm
t	time	h, min, s
t ₁₀	size that is one tenth the size of original particle	mm
$\frac{t_{10}}{\overline{t}_A}$	mean time taken for active part or charge to travel from the toe to the shoulder	S
$t_{\rm D}$	detention or residence time	h
$\frac{t_{\mathrm{D}}}{\overline{t_{\scriptscriptstyle F}}}$	mean time for free fall from the shoulder to the toe	S