

普通高等教育土建学科专业"十一五"规划教材 高校土木工程专业规划教材

Underground Structures (地下建筑结构)

Edited By Zixin Zhang & Xinyu Hu

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Preface

Underground structures originated thousand years ago under the pressure of necessity. As the practical problems involving underground structures broadened in scope, the inadequacy of the scientific tools available for coping with them became increasingly apparent. Underground structures may be a tunnel, a shaft, or a cavern, either alone or a combination thereof. These texts were well received by instructors, students, and practitioners alike. The philosophy of the book was to include only items of utmost importance which will improve the quality of the final designed product, and will render a very cost effective design.

About seven years ago, there were several requests to prepare a single volume that was concise in nature but combined the essential components of underground structures. Nature is always smarter than some of us, and sometimes smarter than all of us. In response to those requests, the book was written for a broad spectrum of readers, ranging from engineers seeking technical guidance to owners and other decision makers hoping to glean a better understanding of alternatives. It included the fundamental concepts and methods of underground structures as well as underground engineering, including rock and soil tunnels, shafts, caverns, diaphragm walls and tunnelling methods.

Research into the development of underground structures and design has been extensive during the past five decades. Authors are tempted to include all of the recent developments in a text book; however, since this text is intended as an introductory text, it stresses the fundamental principles without becoming cluttered with too many details and alternatives. In the text itself, the authors have included cross-references to others chapters as appropriate. It is our hope that this combination will help readers locate information more quickly than a traditional, keyword-based index would.

Underground structures is abundantly illustrated to help students understand the material. Several examples are presented in related chapters. Problems are provided at the end of each chapter for homework assignment, and they are all SI units.

The authors have obviously devoted considerable effort to chapter preparation and they thank the various colleagues, publishers, websites and institutions who gave us permission to use and reproduce their copyrighted materials. Texts, tables and figures taken in whole or in part from various sources are acknowledged where they occur in the text.

The authors are especially indebted to Prof. Evert Hoek, Prof. M. Karakus, Specialist R. S. Sinha, Mr. R. J. Fowell, Prof. K. M. Lee, Prof. Xueyuan Hou, Dr. Yiming Sun, Prof. V. Gabriel Guzman and Prof. R. Kastner for their invaluable assistance and permission in preparing and revising the manuscript. Figures and tables from journals, proceedings, and books are reproduced with permission from the respective publishers.

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Activity is the only road to knowledge, we are slow walkers, but we never walk backwards.

Zixin Zhang

Xinyu Ku

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Symbols

```
A (m^2) = area
A = porewater-pressure coefficient
A_c = activity = I_n / CF
B(m) = width
C(any\ dimension) = constant
C(kN) = resultant cohesion
CF = clay fraction
CRP = constant rate of penetration
CRS = constant rate of strain oedometer test
c(kPa) = cohesion intercept
c (m/s) = compression wave velocity
c'(kPa) = cohesion intercept of Mohr-Coulomb failure envelope in terms of effective stress at failure
c (m) = constant in Engineering News formula
c_{\rm u} (m<sup>2</sup>/year) = coefficient of consolidation
c'(kPa) = soil\ cohesion
c_n(kPa) = undrained shear strength
D = discharge factor (in relation to vertical drains)
D (m) = depth; diameter; spacing between centers of piles
D \text{ (mm)} = grain \ size
D_{10} (mm) = effective grain size
D_{50}(\text{mm}) = mean \ grain \ size
D_{e}(mm) = effective grain size
D_f(m) = depth \ of \ foundation
D_r = relative density of cohesionless soil
DS = direct shear test
DSS = direct simple shear test
d(m) = distance
d \text{ (mm)} = grain \ size
d_h(m) = base diameter of drilled shaft
d_s(m) = shaft diameter of drilled shaft
E 	ext{ (kPa)} = modulus of elasticity}
E (kN/m) = normal force on side of slice (stability analysis)
E_i(kPa) = initial tangent Young's modulus
E_{\cdot}(kPa) = modulus of deformation computed from pressuremeter measurement
E_u(kPa) = undrained Young's modulus
```

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EA (kN) = Normal stiffness of pile or wall

```
EI (kN · m<sup>2</sup>) = flexural stiffness of pile or wall

E (kPa) = Young's modulus of tunnel lining (ML-1T-2)
```

 $(EI)_{\epsilon}(kN \cdot m^2/m) = effective bending rigidity per unit length of a segmental tunnel$

 $EI(kN \cdot m^2/m) = bending \ rigidity \ per \ unit \ length \ of \ the \ actual \ tunnel \ lining$

ESSA = effective stress stability analysis

e = void ratio

 $e_o = initial \ void \ ratio$

F(kN) = reaction; resultant force

 $F = factor \ of \ safety$

 $FS = factor \ of \ safety$

f = coefficient of friction between soil and base of structure

 $f_k(kPa) = physical index of rock mass$

 $G = shear \ modulus; \ also, \ specific \ gravity$

 $GPa = 10^3 MPa$

g (gal) = acceleration due to gravity

H(m) = thickness of stratum

h (m) = thickness of the soil layer

 $h_i(m) = thickness of the soil layer i$

 $IL = incremental \ loading \ oedometer \ test$

I = Moment of inertia of area

 $I_i = liquidity index$

 $I_{n} = plasticity index$

 $I_{z} = vertical strain influence factor$

 I_1 , I_2 , I_3 = invariants of stress

 $I(m^4/m) = moment of inertia per unit length of tunnel lining$

I_s (m⁴/m) = effective moment of inertia per unit length of tunnel lining

 $I_i(m^4/m) = moment of inertia per unit length at the joint$

 $I_L = liquidity index$

i = hydraulic gradient

i = angle of the leading edge of an asperity on a joint

 $i_n(kN/m^3) = pressure\ gradient$

 $J_n = joint \ set \ number$

 $J_r = joint \ roughness \ number$

 $J_a = joint \ alteration \ number$

 $J_w = joint water reduction factor$

K = ratio between intensities of effective horizontal and effective vertical pressures at a given point in a mass of soil

 K_0 = coefficient of earth pressure at rest (value of K for initial state of equilibrium)

 K_{op} = coefficient of earth pressure at rest in normally consolidated young deposits

 $K_a = coefficient$ of active earth pressure

 K_{p} = coefficient of passive earth pressure

 K_{ns} = coefficient of passive earth pressure during passive shearing

K (kPa) = bulk modulus of soil skeleton

K (kPa/m) = spring stiffness

K_b(kPa/m) = modulus of horizontal subgrade reaction

K. (kPa/m) = coefficient of soil resistanc; coefficient of subgrade reaction

K = coefficient of earth pressure

 K_0 = coefficient of earth pressure at rest

 $K_{c}(kN/m^{3}) = soil\ resistance\ coefficient$

 $K_{\theta}(kN \cdot m/(rad \cdot m)) = flexural stiffness of a joint per unit length$

k (m/s) = coefficient of permeability

l(m) = length

l(m) = calculation length of a tunnel (usually adopted as 1 m)

 $M_c(kN/m) = moment of cohesive forces$

 $M (kN \cdot m/m) = bending moment per unit length in tunnel lining$

 $M_n(kN \cdot m/m) = bending moment per unit length due to surrounding earth pressures$

 $M_{ni}(kN \cdot m/m) = bending moment per unit length under the jth loading case$

 \overline{M} = internal bending moment per unit length due to a dimensionless unit force

 $MPa = megapascals (MN/m^2)$

N = dimensionless factor

 $N_b = base stability number$

 $N_{\rm c}$ = equivalent significant number of uniform shearstress pulses produced by earthquake or imposed in the laboratory

n = porosity

 n_a = ratio between distance from bottom of lateral support to point of application of earth pressure and total height of lateral support

 $n_d = depth \ factor \ (stability \ of \ slopes)$

 $n_h(kPa/m) = coefficient of horizontal subgrade reaction$

 $n_o = initial porosity$

n = number of joints in the tunnel half ring

N (kN/m) = axial force per unit length in the tunnel lining

N = axial force per unit length due to a dimensionless unit force

 $N_{\rm p}(kN/m) = axial$ force per unit length due to surrounding earth pressures

 $N_{\rm pi}({\rm kN/m})$ = axial force per unit length under the jth loading case

 $OCR = overconsolidation \ ratio = \sigma'_{v}/\sigma'_{vo} = \sigma'_{vmax}/\sigma'_{vo}$

P = percent of grains smaller than given size

```
P(kN \text{ or } kN/m) = resultant pressure, normal force
P_A(kN/m) = active earth pressure if arching is absent (retaining wall; active Rankine state)
PCPT = push cone penetration test
P_{i} = plasticity index
p_1(kPa) = vertical \ overburden \ earth \ pressure \ at \ the \ tunnel \ crown
p_2(kPa) = reaction pressure at the bottom of tunnel lining
p_3(kPa) = total\ lateral\ earth\ pressure\ at\ the\ crown\ level\ of\ tunnel\ lining
p_4(kPa) = additional \ earth \ pressure \ developed \ at \ the \ tunnel \ invert \ level
p_5(kPa) = self-weight of the tunnel lining
p_{\epsilon}(kPa) = lateral \ soil \ resistance \ pressure
p (kPa) = surrounding earth pressure around a tunnel
p_h(kPa) = value of p along the horizontal axis of the tunnel
p_{v}(kPa) = value of p along the vertical axis of the tunnel
p_r(kPa) = soil\ resistance\ developed\ at\ the\ springline\ of\ a\ tunnel
P(kN/m) = applied \ vertical \ load \ (MT-2)
P_a(kN/m) = active earth pressure if arching is present (bracing in open cuts)
P_0(kN) = Surcharge
P_{p}(kN/m) = passive \ earth \ pressure \ (May \ be \ subdivided \ into \ [P_{p}]_{II}, which depends on cohesion
                and surcharge. )
P_{\cdot}(kN) = resultant \ of \ forces \ having \ seat \ on \ surface \ of \ particle
P_{w}(kN/m) = resultant water pressure
p (kPa) = pressure of normal stress; subgrade reaction
p'(kPa) = effective stress = (\sigma'_1 + \sigma'_3)/2
p_{A}(kPa) = intensity of active earth pressure
p_{L}(kPa) = limiting pressure reached in pressuremeter
p<sub>a</sub>(kPa) = increase in pressure on retaining wall due to surcharge q per unit of area
p_{q1}(kN/m) = increase in pressure on retaining wall due to surcharge q_1 per unit of length parallel to
                crest
p_s(kPa) = swelling pressure
p_1, p_2(kPa) = secondary principal stresses
 Q(kN) = concentrated load; strut load
 q1 (kPa) = total earth pressure developed above tunnel level
 q2 (kPa) = total earth pressure developed at the shoulder regions of a tunnel
 O = shear force per unit length due to a dimensionless unit force
 Q_{\rm p}({\rm kN/m}) = shear force per unit length due to surrounding earth pressures
 Q_{\rm pj}(\,{\rm kN/m}) = shear force per unit length under the jth loading case
 q (kPa) = average gross bearing pressure over the foundation
```

 $q \text{ (kPa)} = shear \ stress = (\sigma_1 - \sigma_3)/2$

```
q (kPa) = uniformly distributed load; surcharge per unit of area; uniformly distributed line load
q (m^3/day) = seepage rate or flow rate
q_a(kPa) = allowable \ soil \ pressure
q_c(kPa) = the pressure at which the material passes from the elastic into the semiplastic or plastic
q_f(kPa) = bearing \ capacity
q_t(kPa) = cone \ tip \ resistance
q_u(kPa) = unconfined compressive strength
R = ratio of size of filter material to size of material to be protected
R (m) = radius of influence of well; radius of curvature of deformed slope
R_c = uniaxial \ compression \ strength
R_f = parameter used in hyperbolic stress strain equation
R_{\cdot} = total \ surcharge \ ratio
R'_{\cdot} = effective surcharge ratio
RMR = rock mass rating according to the Geomechanics Classification
ROD = Rock Quality Designation
R(m) = tunnel calculation radius defined as the average of outer (R_0) and the inner (R_i) ra-
          dii(L)
R_d = displacement \ ratio
R_{hd} = horizontal \ displacement \ ratio
R_{vd} = vertical displacement ratio
r(m) = radius
r_0 = radius of logarithmic spiral
S (kN/m) = total sliding resistance between base of dam and subsoil
S (mm) = settlement; heave; penetration of pile under hammer blow
S = shear wave
S = spacing between joints of a given set
SML = slow maintained load
SRF = stress \ reduction \ factor
S<sub>c</sub>(mm) = settlement at end of construction and application of permanent live load
S_i(kPa) = shear strength intercept according to the Mohr Coulomb relationship ('cohesion')
 S_i(kPa) = shear strength intercept for a joint
S_p(mm) = settlement at end-of-primary consolidation
S_r = degree \ of \ saturation
S_{i} = degree of sensitivity
SQD = specimen quality designation
s (kPa) = shearing resistance; shear strength; drained shear strength
```

 $s_u(kPa) = undrained shear strength$

 $s_u(critical)$ (kPa) = undrained shear strength of liquefied sand

```
s_u(mob) (kPa) = undrained shear strength mobilized in full-scale field failures; undrained shear strength mobilized during stage construction
```

 $s_{\mu\nu}(DSS)$ (kPa) = preconstruction undrained shear strength measured by direct simple shear test

 $s_{uo}(FV)$ (kPa) = preconstruction undrained shear strength measured by field vane test

 $s_{uo}(TC)$ (kPa) = preconstruction undrained shear strength measured by triaxial compression test

 $s_{uo}(TE)$ (kPa) = preconstruction undrained shear strength measured by triaxial extension test

 $s_{\mu\sigma}(UC)$ (kPa) = preconstruction undrained shear strength measured in unconfined compression test

 $s_{uo}(UU)$ (kPa) = preconstruction undrained shear strength from unconsolidated undrained compression test

s_{ua}(kPa) = preconstruction undrained shear strength

T(kN/m) = shear force on side of slice (stability analysis)

 $T(degrees\ centigrade) = temperature$

 $T_c = construction time factor$

 $T_{\rm MR} = magnitude$ of the flexural tensile strength ("modulus of rupture")

 $T_{\rm r}$ = time factor for radial consolidation (vertical compression with radial flow)

T_v = time factor for one-dimensional consolidation in vertical direction

 $T_{\rm o}$ = magnitude of the tensile strength; uniaxial tensile strength unless indicated other wise

 $TC = triaxial \ compression \ test$

 $TE = triaxial \ extension \ test$

t (s) = time t (m) = thickness of the tunnel lining

t (m) = thickness of the tunnel lining

 $t_c(days) = construction time$

 $U = average \ degree \ of \ consolidation$

UU = unconsolidated undrained triaxial compression test

USSA = undrained strength stability analysis

u (kPa) = porewater pressure

u, v (m) = displacements parallel to x, y; positive in positive direction of coordinate axis

 u_r , $u_\theta = displacements parallel to <math>r$, θ

 Δu (mm) = shear displacement along a joint; also radial deformation

 Δh (mm) = the horizontal displacement of the tunnel lining at the springline level

 Δv (mm) = normal displacement across a joint

 $\Delta'_h(m)$ = predicted horizontal displacement of the equivalent tunnel by matching the vertical displacement in the equivalent process

 Δ_{ip} (m) = displacement developed at the location of the redundant force xi due to the action of surrounding earth pressures

 $\Delta_v(m)$ = vertical displacement of a tunnel defined as the total change of the tunnel diameter in the vertical direction

 $\Delta'_{v}(m)$ = predicted vertical displacement of the equivalent tunnel by matching the horizontal displacement in the equivalent process

```
V(m^3) = total\ volume
\nu_{\cdot} = Poisson's ratio of soil
W (kN \text{ or } kN/m) = weight
w = water content in percent of dry weight
w_i = liquid \ limit
w_{o} = natural \ water \ content \ in \ percent \ of \ dry \ weight
w_n = plastic \ limit
w_{\cdot} = shrinkage \ limit
x, y, z = right-handed Cartesian coordinates
z (m) = depth, position, or elevation head
z_c(m) = depth \ of \ tension \ cracks
\alpha = angle
\alpha = pressuremeter rheological coefficient
\alpha = reduction factor on strength of clay adjacent to shaft of pier
\beta (degrees) = slope angle
\gamma (kN/m^3) = total unit weight
\gamma' (kN/m<sup>3</sup>) = submerged unit weight
\gamma_c(kN/m^3) = average unit weight of the comcrete (lining material, etc.)
\gamma_d(kN/m^3) = dry \ unit \ weight, \ unit \ weight \ of \ soil \ if \ water \ is \ entirely \ replaced \ by \ air
\gamma_{m}(kN/m^{3}) = unit weight of water
\gamma_{\rm s}(kN/m^3) = average unit weight of solid constituents
\gamma_{sat}(kN/m^3) = unit weight in saturated state
\gamma_i(kN/m^3) = total unit weight of soil layer i
\gamma_{\rm el}({\rm kN/m}^3) = average total unit weight of soil at the shoulder regions
\gamma_{c}(kN/m^{3}) = unit weight of lining material
\gamma_{m}(kN/m^{3}) = unit weight of water
\Delta = change
δ (degrees) = angle of wall friction; angle between resultant stress on plane and normal to plane
\delta (mm) = displacement at a point of rock mass
\delta_{k} (mm) = lateral movement
\delta_{h_{max}}(mm) = maximum \ lateral \ movement
\delta_{ii} = displacement developed at the location of the redundant force xi and displacing in the same di-
     rection as xi due to the action of a dimensionless unit force x_i = 1
\delta_{ii} = displacement developed at the location of the redundant force xi and along the direction of xi due
     to the action of a dimensionless unit force x_i = 1
\varepsilon = base of Naperian logarithms; unit strain
\varepsilon_{c} = compression strain index
\varepsilon_f = axial \ strain \ at \ failure
```

```
\varepsilon_R = reference strain
\varepsilon_v = vertical \ strain
\varepsilon_{\alpha} = secondary \ compression \ strain \ index
\eta (kN/m<sup>2</sup>) = effective bending rigidity ratio, viscosity
\theta (degrees) = angle; central angle
\lambda = joint stiffness ratio; coefficient of the lateral pressure; creep patameter
\mu = Poisson's ration; field vane correction factor for embankment and foundation stability analysis;
     micron; friction coefficient (= \tan \phi); also same as \eta
\mu_{\scriptscriptstyle UC} = correction factor for unconfined compression test on specimens from D to B quality
\mu_s = field vane correction factor for slope stability analysis
\mu_{t} = time-to-failure correction factor for undrained shear strength from laboratory tests
v = Poisson's ration
\rho = mass\ density\ (FL^{-4}T^2)
\rho_d(\text{Mg/m}^3) = density in dry state
\rho_s(Mg/m^3) = average density of solid constituents
\rho_{sat}(Mg/m^3) = density in saturated state
\rho_{m}(Mg/m^{3}) = density of water
σ (kPa) = total normal stress, normal stress at the cross section of the tunnel lining
\sigma_{\alpha}(kPa) = normal \ grout \ stress
\sigma' (kPa) = effective normal stress
\sigma_1(kPa) = major \ principal \ stress
\sigma_2(kPa) = intermediate \ principal \ stress
\sigma_3(kPa) = minor principal stress
 \sigma_1'(kPa) = effective major principal stress
 \sigma_2'(kPa) = effective intermediate principal stress
 \sigma_3'(kPa) = effective minor principal stress
 \sigma'_c (kPa) = preconsolidation pressure or critical pressure resulting from secondary compression
 \sigma_{1c}'\left(kPa\right) = effective major principal stress after consolidation and before undrained shear
 \sigma_{3c}^{\prime}\left(kPa\right) = effective minor principal stress after consolidation and before undrained shear
 \sigma_{\alpha^{\prime}}^{\prime}\left(\,\mathrm{kPa}\,\right) = in suti effective normal stress on a plane with orientation lpha to the horizontal
 \sigma_h' (kPa) = effective horizontal pressure
 \sigma'_n (kPa) = effective normal stress on a plane
 \sigma_{p}'(kPa) = preconsolidation pressure
 \sigma'_{pl} (kPa) = preconsolidation pressure measured in isotropic consolidation test
 σ'<sub>s</sub> (kPa) = isotropic effective stress in an undisturbed specimen
 \sigma_v'(kPa) = total \ vertical \ stress
 \sigma'_{vc} (kPa) = vertical consolidation pressure
```

ture plunged into the ground

- $\sigma_{vf}(kPa) = postconstruction total vertical stress$
- σ'_{vf} (kPa) = final effective vertical stress = σ'_{vo} + $\Delta\sigma'_{v}$
- σ'_{max} (kPa) = maximum past pressure
- $\sigma_{no}(kPa)$ = preconstruction total vertical stress
- σ'_{m} (kPa) = in situ effective vertical stress, effective overburden pressure
- σ'_{vs} (kPa) = maximum effective vertical stress reached before the removal of surcharge
- $\Delta \sigma_a(kPa)$ = axial stress imposed during the second step of a triaxial test
- τ (kPa) = shear stress
- τ (seismic) (kPa) = equivalent uniform shear stress pulse produced by an earthquake
- $\tau_{\rm c}({\rm kPa})$ = shear stress carried by soil after consolidation and before undrained shear
- $\tau_h(kPa)$ = shear stress on horizontal planes
- $\tau_{max}(kPa) = maximum shear stress pulse produced by an earthquake$
- $\tau_{r\theta}(kPa)$ = the shear stress in the radial of tangential direction, at any point of ground
- $\tau_s(kPa)$ = shear stress applied under undrained conditions followed by consolidation
- $\tau_v(kPa) = shear stress on vertical planes$
- $\tau_{\alpha o}(kPa)$ = in situ shear stress on a plane with orientation α to the horizontal
- Φ = velocity potential (flow net)
- $\phi'(\text{degree}) = \text{effective-stress friction angel}; \text{ effective internal friction angle of soil}; \text{ angle of shearing resistance}$
- ϕ'_{cv} (degree) = constant-volume friction angle
- ϕ'_d (degree) = component of friction angle produced by dilation
- ϕ'_{α} (degree) = component of friction angle of granular soils resulting from geometrical interference
- ϕ_i' = friction angle for a joint
- ϕ_m' (degree) = effective-stress friction angle mobilized at undrained yield condition
- $\phi_{\scriptscriptstyle o}'$ (degree) = component of friction angle of granular soils resulting from particle rearrangement
- ϕ'_s (degree) = secant friction angle for granular soils
- ϕ'_{μ} (degree) = angle of interparticle sliding friction
- φ (degree) = internal friction angle of soil/rock
- $\psi(\text{degrees}) = angle \ of \ dilatancy$
- Ψ =function defining flow lines; angle between the direction of σ_1 and the plane of a joint
- $\overline{\omega}$ = average displacement of a bearing plate
- $\omega(\%)$ = moisture content of the soil
- lna = Naperian (natural) logarithm of a
- log a = log arithm of a to the base 10
- $x_1(kN \cdot m/m) = bending moment per unit length acting at the tunnel crown$
- $x_2(kN \cdot m/m) = axial$ force per unit length acting at the tunnel crown

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