李德平 潘白强 胡遵素 等著



### 图书在版编目(CIP)数据

辐射防护及相关学科论文集(SELECTED WORKS FOR RADIATION PROTECTION AND RELATED TOPICS)/李德平、潘自强、胡遵素等著. 一北京:原子能出版社,1996. 10 ISBN 7-7022-1603-0

I. 辐···I. 李···II. 辐射防护-研究-文集 N·R. 142-53 中国版本图书馆 CIP 数据核字(96)第 17993 号

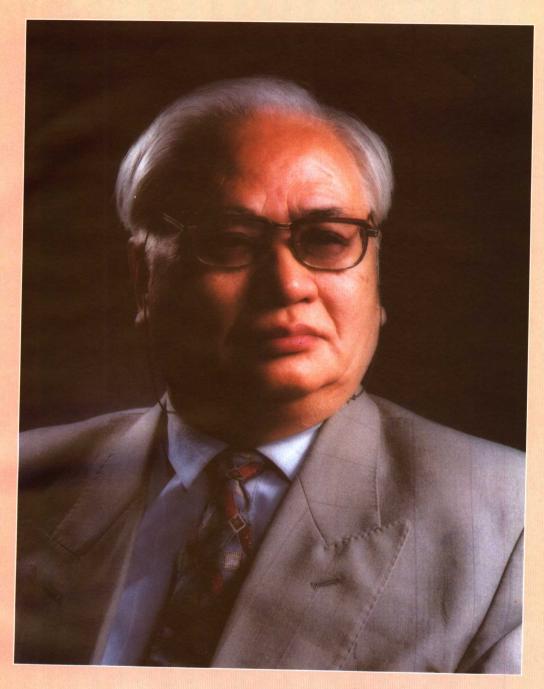
### 内容简介

本文集选录了中国科学院院士、中国辐射防护研究院名誉院长李德平先生以及国内辐射防护界部分人士发表过的和未发表过的学术论文 70 余篇。这些论文涉及辐射防护、辐射物理、核电子学与探测技术、核安全与辐射安全、环境保护和辐射损伤与效应等领域,部分反映了国内该领域的科研活动与发展历程。在李德平院士从事辐射防护工作 42 年之际,组织出版本论文集是一次有益的回顾与总结。

本文集可供上述领域的广大科技工作者和有关大专院校师生阅读和参考。

②原子能出版社,1996

原子能出版社出版发行 责任编辑:李 镁 封面设计:崔 彤 技术编辑:杨京蜀 社址:北京市海淀区阜成路 43 号 邮政编码:100037 原子能出版社 印刷厂印刷 新华书店经销 开本:787×1092 mm 1/16 印张 33.5 字数 840 千字 1996年10月北京第一版 1996年10月北京第一次印刷 印数:1—500 定价:(精)81.00元



李德平院士近照(1995年)



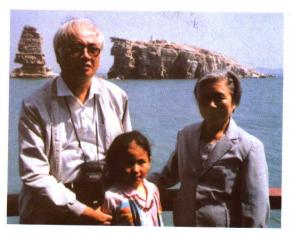
国际放射防护委员会(ICRP)主委员会全体委员在美国(1990年)



国际原子能机构(IAEA)核安全咨询顾问组(INSAG)全体成员在维也纳(1992年)



李德平院士与来自台湾地区的辐射防护专家翁宝山亲切交谈(1993年)



李德平院士与夫人王怀珍及外孙女在长岛 (1992年)

## 前言

今年11月4日是我国著名的辐射物理、辐射防护与核安全专家、中国科学院院士、中国辐射防护研究院名誉院长、国际放射防护委员会(ICRP)主委员会委员李德平先生从事辐射防护工作42年和70寿辰。李德平先生不仅是我国核工业辐射防护学科的开创者和奠基人;而且,他的博大精深的学识,严谨的学风,以事业为己任的敬业精神和为人师表的高尚品德,感染并造就了我国核工业辐射防护系统一大批科研和技术骨干(包括以后调入其他有关单位的一些同志),他们中的许多人发表的第一篇或最主要的论文都倾注着李先生的智慧、关心和帮助。在庆贺李先生70寿辰之际,由中国核工业总公司安防环保卫生局、中国辐射防护研究院、中国辐射防护学会、中国原子能科学研究院保健物理部、国家环保局监督管理司辐射处和四川联合大学核技术应用研究所等单位联合组织征文、编纂本文集。这是对李先生诲人不倦、不惜以自己创造性思想之光点燃他人智慧之火的崇高精神的敬仰和回报;又表示我们将继续推进李先生关于加强学术交流的一贯主张,以繁荣辐射防护事业。

此次征文共征集到论文 150 多篇,由于篇幅所限,收入本文集 70 余篇。其中包括李德平先生过去没有公开发表的论文三篇;还包括部分著名专家早期在李德平先生指导下发表的有相当重要意义的论文或近期完成的新作。文集的内容涉及辐射防护、辐射物理、核电子学与探测技术、核安全与辐射安全、环境保护和辐射损伤与效应等,可供有关专业研究人员参考。

原子能出版社孙家辉、李盈安和韩国光编审参加了本论文集的审稿工作,特在此致以谢意。

《辐射防护及相关学科论文集》编委会 1996 年 9 月

# 目 录

	前 言
	A 辐射物理
	Performance and Optimization of Potential Alpha-Energy Concentration Measurement
	Li Deping(1)
	An Electron Transport Theory of Cavity Ionization Luo Zhengming(9)
	盖革管的起始电压和气体放大倍数的测量 李忠珍等(23)
	测量活度的双4π 方法 于凤翘等(30)
	6~300 keV X 射线刻度辐射源 ······ 陈明焌(37)
<b>✓</b>	<b>氡子体在室内表面沉积速率的测量</b> ·························· 王恒德(46)
	高能 Y 射线参考辐射场空气比释动能(率)测定 ··················· 李景云等(51)
	低大气层中宇宙射线电离量的分布测量 岳清宇等(58)
	测量放射性气溶胶的双道能量补偿法 郑仁圻等(66)
	毫居里级 <sup>60</sup> Co 标准源的制备 ······· 丁健生等(72)
	环境辐射仪器 7 照射量率刻度的阴影屏蔽法 丁民德等(78)
	电离室能量响应补偿的实验研究及防护水平照射量传递电离室组设计 张友忠(84)
	用重叠面积法计算的几何因子及其实验验证 石志侠等(93)
	三类微量元素谱样本的计算机模式识别 滕慧洁(100)
	10年来环境样品放射性测量的国际比对 黄治俭等(106)
	TO JOS AND AND THE
	B <b>保健物理</b>
	保健物理概论 潘自强(117)
	Radiation Risk A Chinese Status and Future Pan Ziqiang(135)
	β剂量标准的建立 张延生等(145)
	指数过滤规律假设在多分散度钚气溶胶浓度监测中的适用性考察 吴德强等(154)
	定向吸收剂量率的刻度 陈丽姝等(163)
	氡及其子体暴露量-有效剂量的转换 李素云(169)
	ICRP 呼吸道模型的沿革
	体内 <sup>124</sup> Sb 滞留量的测定及内照射剂量的估算 ··················· 冯定华等(179)
	Radiation Protection Against Medical X-ray Diagnosis in Beijing Wu Yi et al(183)
	高分子超细纤维滤纸对空气中氡氧子体的静电吸附 汪佳明等(187)
	用 IAEA 胸腔模型作体外计数的刻度研究 樊耀国等(190)

## C 核电子学与探测技术

一个简单的电流-频率变换器 李德平(196)
电离室型直读式个人剂量仪与剂量率仪 胡遵素(216)
感应简拾取束流脉冲信号的分析 ************************************
个人剂量仪可靠性分析 杨华庭(232)
选通式环境 7 照射量率仪 陆雪明等(239)
乙烯-聚乙烯快中子剂量正比计数器 冷瑞平等(244)
模拟计数率表误差的自身原因及其读数的刻度方法 张凤翔(252)
1πα 计数器 叶敏坤等(260)
300 cm <sup>2</sup> 平行板 α 屏栅电离室的研制 ····································
板形铀元件表面污染量检测仪的研制 王庆恒等(269)
空气中氚实时连续监测仪的研制 杨怀元等(276)
D 核安全与辐射安全
对辐射事故的预防与处理的几点意见 李德平(281)
核或辐射应急中的干预与干预水平    陈竹舟(288)
论核事故应急范畴与范围 任镜暄(297)
模块式高温气冷堆的环境安全特性
风险的概念与风险的可接受性 曲静原等(307)
我国高放废物处置库选址与安全问题分析 周子荣(313)
E 环境保护
环境辐射影响评价方法学 张永兴(317)
辐射防护新概念对放射性废物管理的启发意义 陈 式(334)
关于确定秦山核电厂(一期工程)烟羽应急计划区大小的建议 陈竹舟等(341)
豁免原则应用中某些有关问题的讨论
Impacts of Atmospherically Deposited Radionuclides on Drinking Water Supply
after a Nuclear Power Plant Accident Fang Dong et al (354)
地下水环境影响评价的几种方法 李书绅(361)
非饱和黄土介质中核素迁移行为的分析与评述 王志明等(369)
全国环境天然放射性水平调查回顾 何振芸等(375)
中国原子能科学研究院地区的环境辐射容量 谢建伦等(380)
放射性核素在陆地和淡水食物链中的转移系数 寿芸二签(2021)

SRDAAR-QNPP: A Computer Code System for the Real-time Dose Assessment
of an Accident Release for Qinshan Nuclear Power Plant Hu Erbang et al (395
广东低中放废物处置场环境影响预测评价 黄雅文等(404
我国核电站气载碘去除技术的研究与应用 贾 明等(414
用同位素示踪测定基岩裂隙岩溶中地下水弥散系数 郑汝宽等(420
基于微机的核设施环境评价软件包 杨 胤等(425
南京地下空间中的氡污染与新构造断裂带的关系研究 戴鸿贵(433
F 辐射损伤与效应
小剂量受照人员的淋巴细胞染色体畸变 曹淑媛等(439
Cytogenetic Adaptive Response Induced by Pre-exposure in Human Lymphocytes
and Marrow Cells of Mice Zhang Lianzhen (446
辐射与化学污染物致体细胞 HGPRT 基因位点突变的比较研究 ····· 徐洪兰等(452
电离辐射对中枢神经系统发育的影响 杨志远等(460
辐射诱发小鼠胸腺淋巴瘤中包含易位的染色体畸变 陈 英等(465
β射线所致皮肤损伤的远期效应及疗效观察 刘雁玲等(470
711矿开采35年粉尘浓度与矽肺发病分析 高增林等(475
两种标准铀矿样粉对肺巨噬细胞毒性的体外研究 ······ 温晋爰等(479
<sup>226</sup> Ra 内污染一例临床观察和评价 ······ 齐汝全等(484)
大量钚伤口污染案例的医学处理及随访观察 李俊梅等(489
一例多种核素超剂量内污染者16年医学随访 李爱筠等(495)
G 其 他
高精度地应力仪的研制及其在地震预测预报中的应用 胡遵素等(502)
辐射交联氯化聚乙烯防水卷材 马信民等(508)
撰写和审改学术论文中应重视的一些问题 胡逢全等(513)
杰出的学者、导师和顾问 赵亚民(520)
李德平院士简历及国内外任职情况 (523)
后 记

# A辐射物理

# PERFORMANCE AND OPTIMIZATION OF POTENTIAL ALPHA-ENERGY CONCENTRATION MEASUREMENT

### Li Deping

(Institute of Radiation Protection, MNI P. O. Box 120, Taiyuan, Shanxi, P. R. China)

Abstract Some calculations were made to evaluate procedures for Rn daughters pontential alpha-energy concentration  $C_E$  measurements through filter sample counting, possible difference in counting efficiencies for different alphas have been taken into consideration. A method for selecting the time schedule for measurement with given total time, to minimize the dependence of the estimated  $C_E$  on the concentration ratios, is presented. It is found that two counts at selected times can eliminate this dependence.

Possible improvements with separate RaA counting, and the optimized time schedule for daughter concentrations measurements, have been preliminarily explored. Some slight improvement is gained by inserting a waiting time between the two counting intervals. Influence of change of concentrations or sampling rate during sampling is briefly discussed.

The potential α-energy concentration of Rn daughters in air is more directly connected with the hazards to person exposed to Rn and its daughters. This quantity is a weighted sum of the activity concentrations C<sub>A</sub>, C<sub>B</sub>, C<sub>C</sub> of the three daughters RaA, RaB and RaC:

$$C_{\rm E} = E_1 C_{\rm A} + E_2 C_{\rm B} + E_3 C_{\rm C}$$
  
= 3. 611 $C_{\rm A}$  + 17. 815 $C_{\rm B}$  + 13. 095 $C_{\rm C}$  (GeV/Bq) (1)

In field methods, the  $\alpha$ -activity of daughters on a filter sample of the air is counted in an appropriate time interval after sampling. This count is another weighted sum of the concentrations

$$N = \eta_{\rm C} v n$$

$$n = (aa\eta_{\rm A}/\eta_{\rm C} + ac)C_{\rm A} + bC_{\rm B} + cC_{\rm C}$$
(2)

here  $\eta_A$ ,  $\eta_C$  are counting efficiencies for alphas from RaA and RaC, v volume sampled in unit time, a, b, c, aa, ac are constants determined by the time schedule adopted. Following the classical Kusnetz's method, approximate value of  $C_E$  is obtained by multiplying N with a constant k. This inevitably introduces an error of the method, whose magnitude depends on the range of possible concentration ratios  $X(=C_B/B_A)$ ,  $Y(=C_C/C_A)$  encountered. Various modifications have

been proposed with a view to improve the accuracy or to reduce time. Such proposals had been reevaluated by us, and the general trends of performance and optimization of such methods have been studied.

On the X-Y plane, possible values of concentration ratios are enclosed in the curve representing the growth of daughters with Rn age and the straight line, joining its ends, since mixture of Rn of different ages can not go outside. As the ventilation rate is limited in practice, extreme points (e. g. with ventilation rate greater than 10 times per hour) can be excluded as shown in fig. 1.

If the straight lines N=0,  $C_E=0$  meet at the point  $P(X_P, Y_P)$ , then points on any straight line passing throught P

$$Y-Y_P=m \cdot (X-X_P)$$

where m is the slope, will give the same

$$C_{E}/n = (E_1 + E_2 \cdot X + E_3 \cdot Y)/(a + b \cdot X + c \cdot Y)$$
$$= (E_2 + m \cdot E_3)/(b + m \cdot c)$$
(3)

And two such lines (with slopes m and  $m_T$ ) touching the

boundary of the concentration ratio region give the range of values of  $C_E/n$ . These slopes and the Rn age corresponding to the point of contact are shown in fig. 2. Now the trick of narrowing down the range of  $C_E/n$  lies in selecting P for small viewing angle substended by this region and keeping the angle between  $C_E = 0$ , n = 0 small (b/c near to  $E_2/E_3 = 1$ . 36).

It is convenient for general discussion to introduce an effective delay time  $T_{\rm D}'$  which is the time between instantaneous sampling and counting that gives the same value of b/c.

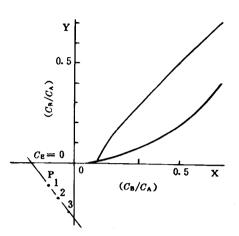


Fig. 1 Region of possible values of concentration ratios

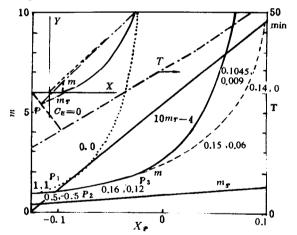


Fig. 2 Slopes  $m, m_T$  of bond lines passing P on  $C_E = 0$ 

With non-overlapping sampling interval and counting interval of time  $t_s$  and  $t_m$ , and the time between the mid-points of each interval  $T_D$ , we can rewrite(2) into

$$n/\psi_{s}\psi_{m} = (aa'R + ac' - waa')C_{A} + b'C_{B} + c'C_{C}$$

$$T_{D}' = T_{D} + \Delta T_{s} + \Delta T_{m}$$

$$R = (\eta_{A}/\eta_{C} + w)\zeta_{s}\zeta_{m}$$
(4)

Extreme concentration ratios may occure down stream a near by strong local Rn source or when an efficient local recirculating filter is operated.

where w=0.023525, aa' to C' are corresponding coefficients for the effective delay time while  $\psi$  and  $\zeta$  correction factors  $\Delta T$  correction for finite  $t_*$  and  $t_m$ , as shown in fig. 3. Thus slope of the line n=0 is determined by  $T_D'$ , while  $\zeta$  depends on  $T_D'$  and R.

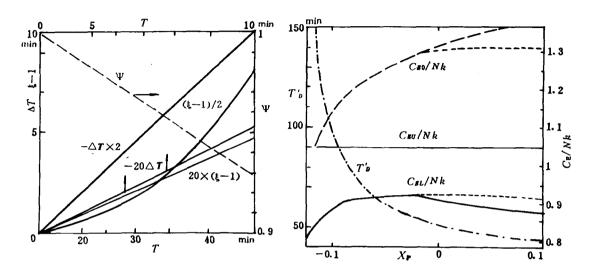


Fig. 3 Correction for finite sampling and counting times

Fig. 4  $C_E/Nk$  and effective delay time  $T_D'$  for Kusnets's method

For the Kusnetz's method, the term aa' R is negligible, and the point P is nearly uniquely determined by  $T_{\rm D}'$ . Relationships between  $T_{\rm D}'$ ,  $C_{\rm E}/Nk$  and  $X_{\rm P}$  are shown in fig. 4. When  $T_{\rm D}'$  increases from 45 min, the effect of increase of the angle between  $C_{\rm E}=0$  and n=0 is compansated

by the decrease of viewing angle up to 83min. This is illustrated by the curve for  $C_{\rm EL}/Nk$ , the lower branch corresponds to the extreme point X=0.1045, Y=0.009, it follows the same trends but  $T_{\rm D}{}'$  longer than 50 min, is preferable. When the point 0, 0 is included, the upper bound of  $C_{\rm E}$  will be significantly higher, this means undesirable underestimation and longer delay time, say 83 to 155 min., helps to reduce it.

When we start counting early enough to catch sufficient RaA alpha counts to keep P at the optimum point  $P_2$  X = -0. 08753. (or  $P_1$ , X = -0. 11682 when 0,0 is included), further reduction of error is possible with long time counting as shown in fig. 5 for  $\eta_A/\eta_C = 1$ , 2. 669min sampling followed by 160min,

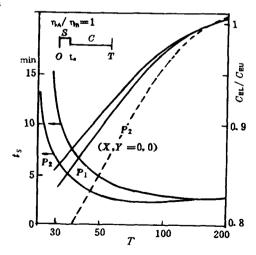


Fig. 5 Reduction of error with long counting and early starting

counting will eliminate this error completely.

For the rapid methods, the parameter R is very important. Since  $T_D' = 33.19 \mathrm{min}$ . (i. e. b/c 1. 36), for fixed P, increase of  $T_D'$  will decrease the angle between  $C_E = 0$  and N = 0, and reduce the range of  $C_E/N$ ; and optimun  $T_D'$  is determined by R and increases with R, as more time is needed for the RaA to decay to the required counting rate. Such trends are clearly shown in fig. 6 and fig. 7; in these figures  $C_{EU}$  to  $C_{EL}$  is the range of  $C_E$  under normal ventilation rate and  $C_{EU}$  corresponding to the extreme case X, Y = 0, 0, the value of  $C_{EU}/Nk$  is assigned to be 1. 1 through choice of k.

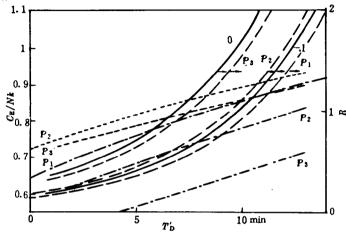


Fig. 6 R and  $C_E/Nk$  for rapid methods  $- \cdot - \cdot - \cdot C_{E0}/Nk$ 

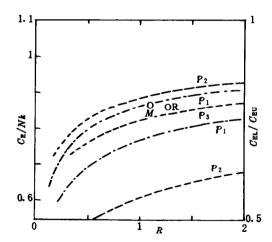


Fig. 7 Curve of  $C_{\rm E}$  vs R circles indicate Markov's and Rolle's methods

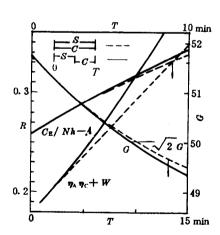


Fig. 8 Parameters for instant methods
G is proportional to counting fluctuations

R and  $C_{\rm E}/Nk$  for the Rolle's and the Markov's methods are also indicated in fig. 7, they are

near to the curve for  $P_1$  (optimun including 0,0), yet leave some room for slight improvement: for instance, shorten  $T_D$  by 39 sec.  $C_E/Nk$  will increase from 0.859 to 0.881 and to 0.90 on the curve for  $P_2$  with 99.5 sec. shortening.

It is possible to save time further, at the expanse of some increase of the range of  $C_E/Nk$ , through intentional reduction of  $\eta_A/\eta_C$ . To the extreme one gets various instant methods. For the measurement schemes illustrated in fig. 8,  $T_D = T/2$  when  $t_* = t_m = T/2$ , and  $T_D' = T/3$  when sample and count simultaneously with  $t_* = t_m = T$ ,  $t_* = t_m = T$ , thus  $C_E/Nk$  can be read from the left end of the same curve in fig. 7. Exact values of  $C_E/Nk$  and the  $\eta_A/\eta_C + w$  required are plotted in fig. 8, coefficient of variation of the estimated  $C_E(Nk)$  is given through G in the figure with

$$CV = G/(\sqrt{Nk \cdot \eta_{c} v} \cdot T)$$
 (5)

With  $\eta_c = 0.35$ ,  $v = 2.1/\min$ ,  $t = 5\min$ . CV due to counting statistics will be 17% at one tenth of the ICRP DACa.

It is also possible to combine two counts  $N_1$ ,  $N_2$  of the same sample at different time together as N, e.g.  $N=rN_1+N_2$ . For the instant metoods, r is chosen for intersection  $P_2$  and circumambulate the need of tailoring  $\eta_A/\eta_C$  when it is known. In most cases,  $\eta_A/\eta_C$  is higher than the value needed, and r is nagative; this increases  $T_D$  with slight improvement in  $C_E/Nk$ , but the counting fluctuation increases enormously. Fig. 9 demonstrates these trends for the time schedule; half of the total time for sampling and counting and half for the second counting.

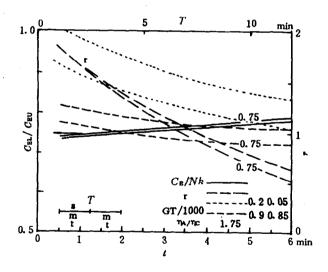


Fig. 9 Instant methods with two counting intervals

When we chose the second counting interval with  $T_{\rm D}'$  arround 33 min, the error of the method will be drastically reduced or even eliminated; for example,  $\eta_{\rm A}/\eta_{\rm C} = 1.0-5 {\rm min}$  sampling and simutaneous counting 35.96-45.96 min second counting with  $N=0.21250~N_1+N_2$ , and  $\eta_{\rm A}/\eta_{\rm C} = 0.75$ , 38.02-48.02 min second counting with  $N=0.27994N_1+N_2$ .

When the measuring scheme makes the three straight lines  $C_E = 0$ ,  $N_1 = 0$ ,  $N_2 = 0$  meet at

$$r = (-b_2 E_2 - c_2 E_3) / (b_1 E_2 - c_1 E_3)$$
(6)

then  $C_E/N$  is a constant and independent of the concentration ratios X and Y, i. e. free from this error of the method.

For example, any rapid method with intersection at  $P_2$  for routine monitoring, can be combined with the Kusnetz's method with delay time of 83. 3 min for some important data or when extreme ventilation conditions might have happened. Colinear mapping between the X,Y plane and the  $N_2/N_1$ ,  $C_E/N_1$  plane had been used to deal with pair of counts not exactly matched on P.

To count alphas from RaA and RaC separately with spectrometric method, one would provide more fluxibility in obtaining the effective  $\eta_A/\eta_C$  required. One possibility of utilizing this additional information is to narrow down the range of X and Y with the constraint, see equation (3). Typical performance is shown in fig. 10.

$$bX + cY = aa\eta_{\rm C}/\eta_{\rm A} - ac \tag{7}$$

As to the measurement of the concentrations of the three daughters, some calculations have been made on the method counting separately  $N_A$  and  $N_C$  with spectrometric instruments in two counting intervals.  $N_A$  in the first interval gives  $C_A$  directly, and then  $C_B$  and  $C_C$  are solved from the two  $N_C$  counts. Optimization of the time schedule depends on the objective function aimed at, and the concentration ratio is also involved, and two levels of degree of equilibrium X,Y=0.9,0.85(H) and 0.2,0.05(L) are considered. To illustrate the trend we choose as the objective

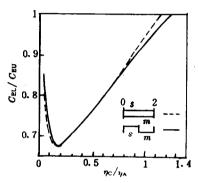


Fig. 10 Inprovement with known NA

function some thing mid-way between the sum of variances and the sum of square of coefficients of variation of the daughters i. e.

$$OB = (\sigma_{A}^{2} + \sigma_{B}^{2}/X + \sigma_{C}^{2}/Y)/C_{A}^{2}$$
 (8)

it is only an index as correlations between estimated values are ignored. The time schedule thus optimized is shown in fig. 11, H is proportional to the objective function

$$OB = S/(60T\eta_{C}vEC) \tag{9}$$

where EC is the equivalent equibrium Rn concentration. When the time schedule shifts to that optimized for the other level, increase in S (shown with short vertical bars) is slight, so a schedule mid-way between these two would be appropriete for practical purpose. H for other indices, for the same schedule is shown in fig. 12 with the shifted curves in dotted lines.

It is interesting to note that a waiting time  $T_G$  between the two counting intervals can decrease the S (unfortunately, by less than 10%). As the effect of decrease of counts, hence the variances, is dominating at moderate  $T_G$ . Similar effects are observed for other plausible objective functions, as shown in fig. 13. On the other hand, waiting time between sampling and counting will increase H and should be minimized.

The assumption of constancy of the product v • concentration for all the three daughters, during sampling, taken for granted in most such works, have been examined. In most cases, 20% decrease during sampling will decrease the estimated CE by a few percents even for pure RaA, and far less for higher X and Y. For concentration measurement, the situation is less happy, usually the error of concen trations and their ratios are less than 10%.

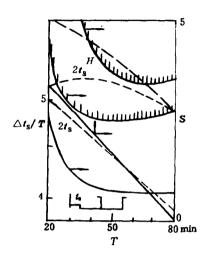


Fig. 11 Optimized time schedule for daughter conc. OBJ see equation (8)

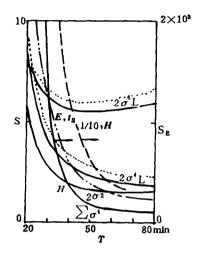


Fig. 12 S for other combinations of statistical error

#### **APPENDIX**

The counts corrected for counting efficiency and sampling rate are:

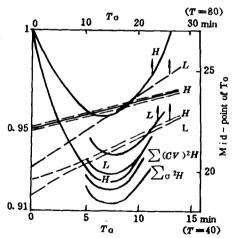
$$n_{A} = aaC_{A}$$

$$n_{C} = acC_{A} + bC_{B} + cC_{C}$$
where
$$aa = f_{1} \quad c = f_{3}$$

$$b = \frac{\lambda_{3}}{\lambda_{3} - \lambda_{2}} \cdot (f_{2} - f_{3})$$

$$ac = \frac{\lambda_{2}}{\lambda_{2} - \lambda_{1}} \times \frac{\lambda_{3}}{\lambda_{3} - \lambda_{1}} (f_{1} - f_{3}) + \frac{\lambda_{2}}{\lambda_{1} - \lambda_{3}} \times \frac{\lambda_{3}}{\lambda_{3} - \lambda_{2}} (f_{2} - f_{3})$$

For non-overlapping sampling time t, counting time  $t_{\rm m}$  and the delay time between the mid-points of the two Fig. 13 Reduction of a with waiting time intervals  $T_{\rm D}$ ,



 $T_G t_* = 40,10.43;80,15.55 \text{ min}$ 

$$f_{i} = 4 \cdot \sinh(\lambda_{i} t_{s}/2) \cdot \sinh(\lambda_{i} t_{m}/2) \exp(-\lambda_{i} T_{D}) / \lambda_{i}^{2}$$
(A2)

i=1,2,3 for RaA, RaB, RaC. And for simultaneous counting and sampling,

$$f_i = [\lambda T + \exp(-\lambda_i T) - 1]/\lambda^2$$
(A3)

introduce

$$\Delta T = \ln \{\lambda_3 \sinh(\lambda_2 t/2) / [\lambda_2 \sinh(\lambda_3 t/2)] \} / (\lambda_2 - \lambda_3)$$

$$\psi = \{ [2\sinh(\lambda_3 t/2) / \lambda_3 t]^{\lambda_2} \cdot [2\sinh(\lambda_2 t/2) / \lambda_2 t]^{-\lambda_3} \}^{1/(\lambda_2 - \lambda_3)}$$

$$\zeta = 2\sinh(\lambda_1/2) \exp(-\lambda_1 \Delta t) / \lambda_1 t \psi$$
(A4)

denote 
$$\frac{\lambda_2}{\lambda_2 - \lambda_1} \cdot \frac{\lambda_3}{\lambda_3 - \lambda_1}$$
 with  $w$ 

we can rewrite (A1) into

$$n_{A}/\psi_{s}\psi_{m} = aa'\zeta_{s}\zeta_{m}C_{A}$$

$$n_{C}/\psi_{s}\psi_{m} = (waa\zeta_{s}\zeta_{m} + ad')C_{A} + b'C_{B} + c'C_{C}$$
(A5)

and total counts

$$N_A + N_C = \eta_C v_n = [(aa'R + ad')C_A + b'C_B + c'C_C]\psi_s\psi_m\eta_c v$$

coefficients with prime are those corresponding to the effective delay time  $T_{\rm D}{'}=T_{\rm D}-\Delta T_{\rm s}-\Delta T_{\rm m}$  with

$$f'_{i} = \exp(-\lambda_{i} T_{D}')$$

$$ad' = ac' - aa'w$$

$$R = (\eta_{A}/\eta_{C} + w) \zeta_{s} \zeta_{m}$$

This helps in expressing the effect of finite  $t_s$  into a single  $\psi$  and small corrections.

#### REFERENCES

- 1 Ji Wanhua, Li Deping. Atomic Energy, 1964(8):711(in Chinese)
- 2 Li Deping. Radiation Protection, 1981, 1(3):1(in Chinese)

# AN ELECTRON TRANSPORT THEORY OF CAVITY IONIZATION

### Luo Zhengming

(Southwestern Institute of Physics, P.O. Box 15, Leshan, Sichuan, P. R. China)

Zhengming L. An Electron Transport Theory of Cavity Ionization. Radiat. Res. 84,1-15(1980).

Abstract An electron transport equation is applied to the study of the cavity ionization phenomenon. It has been proved that the effect of the cavity on the energy spectrum of electrons inside this cavity can be attributed to an equivalent electron source uniformly distributed in the cavity. A formula for the energy spectrum of the equivalent electron source is obtained. The deposited energy due to the equivalent electron source in the cavity of the plate chamber has been calculated. The new theory, compared with experimental results, is better than the Spencer-Atitx theory for describing the phenomenon of cavity ionization.

The idea that ionization in the cavity may be applied to estimating energy deposition in the surrounding medium was first proposed by Bragg<sup>[1]</sup>. A similar idea was again formulated by Gray in his cosmic ray research, and the relationship between the energy deposition of radiation in the medium and ionization in the cavity was found<sup>[2,3]</sup>. It is generally called the Bragg-Gray principle. Many experiments have shown that the Bragg-Gray principle is more accurate in cavities of greater dimensions for such wall material as graphite, whose atomic number is approximately that of air. However, many experiments, including Gray's own work, have shown that the difference between the prediction of the Bragg-Gray principle and experimental results is appreciable for such wall materials as lead, tin, and copper, whose atomic numbers differ greatly from that of air. In contradiction with the conclusion of the theory, the experiments have shown that specific ionization (i. e., ionization per gram gas in the cavity) regularly varies with the dimension of the cavity<sup>[4~6]</sup>. This variation is especially apparent in experiments with X and Y rays of lower energy<sup>[7]</sup>. It is clear that the Bragg-Gray principle cannot fully describe the phenomenon of ionization in the cavity.

Analyzing the discrepancy between the Bragg-Gray principle and ionization experiments with small cavity chambers, Spencer and Attix<sup>[8]</sup> and Burch<sup>[9]</sup> published their theoretical work in 1955. They showed that a full analysis of the electron spectrum in the wall ought to take into account accumulation of  $\delta$  electrons with higher energy. The fundamental assumption of the Bragg-Gray principle has been kept in the Spencer-Attix theory; i. e., the electron spectrum in