# Industrial separators for gas cleaning

O. STORCH ETAL.

# INDUSTRIAL SEPARATORS FOR GAS CLEANING

# OTAKAR ŠTORCH et al.

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ELSEVIER SCIENTIFIC PUBLISHING COMPANY
Amsterdam — Oxford — New York — 1979

Published in co-edition with SNTL Publishers of Technical Literature, Prague

Distribution of this book is being handled by the following publishers

for the U.S.A and Canada Elsevier North-Holland, Inc. 52 Vanderbilt Avenue

New York, N. Y. 10017

for East European Countries, China, Northern Korea, Cuba, Vietnam and Mongolia SNTL Publishers of Technical Literature, Prague

for all remaining areas
Elsevier Scientific Publishing Company
335 Jan van Galenstraat
P.O. Box 211, 1000 AE Amsterdam, The Netherlands

#### Library of Congress Cataloging in Publication Data

Štorch, Otakar.

Industrial separators for gas cleaning.

(Chemical engineering monographs; v. 6)

Translation of Čištění průmyslových plynů a exhalací odlučovači.

Bibliography: p.

Includes index.

1. Separators (Machines) 2. Gases—Cleaning—Equipment and supplies. 3. Dust—Removal—Equipment and supplies.

TP 159. S4S7513

628.5'3'2

78-10916

ISBN 0-444-99808-X

ISBN 0-444-41295-6 (series)

Translation by Julius Freundlich

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Printed in Czechoslovakia

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#### Foreword

In these times of constant progress in technology, of rapidly expanding industries and ever new processing techniques in so many of them, industrial gas cleaning is rapidly gaining in scope and importance. Gas cleaning facilities are nowadays indispensable ancillaries of every plant where, for economic or environmental reasons or both, solid or liquid particles have to be separated out from a gas stream. Moreover, the equipment used for this purpose up to now is increasingly falling short of the ever more stringent requirements imposed by public health regulations, so that much of it is growing ripe for replacement by new, more efficient and more dependable installations. In most countries, the introduction of new and replacement of existing gas cleaning facilities is being hastened by legislation which reflects our growing awareness of the enormity of the damage caused by industrial air pollution.

All too often, however, any rational selection of gas cleaning equipment is hampered by the sheer diversity of types now on the market. The prospective buyer is confronted by a wide range of units based on entirely different physical principles, and with a huge variety of others which, although identical in their basic principles, differ substantially in detail design.

This book therefore sets out to review the existing types of gas cleaning equipment; to outline their underlying principles and principal design features; to list their chief technical data, their relative advantages and drawbacks; and to facilitate the choice by making a few recommendations about the kinds of equipment which are most suitable for some of the major industries. Most of these recommendations are based on long-term experience, but some have of necessity had to be founded on theory rather than on accumulated know-how.

Apart from this survey of the presently available gas cleaning equipment, the book also deals in brief outline with the fundamentals of the dust handling techniques involved in the operation of this equipment. This aspect is all too often underrated; yet it is a fact, borne out by dearly paid experience, that no one can design, install or operate gas cleaning facilities properly unless he is fully familiar with the problems specific to the field of dust handling.

# Symbols and terminology

а	(microns), (m)	Particle diameter
a	$(m s^{-2})$	Acceleration
$a_{\mathrm{mean}}$	(m)	Mean particle diameter
$a_1$	(microns)	Reduced equivalent diameter of a fictitious
		spherical particle
$b_{\mathbf{v}}$	$(m s^{-2})$	Acceleration by centrifugal field
j'	$(s m^{-1})$	Specific area of collecting surface
g	$(m s^{-2})$	Acceleration by gravity
h	(hours)	Annual utilization of separator
i	$(A m^{-1})$	Specific current intensity
i	$(kJ kg^{-1}), (kcal kg^{-1})$	Enthalpy per kg of matter
k	$(kg m^{-3})$	Concentration of solid or liquid particles in
		gas
$k_0$	$(g m^{-3}), (kg m^{-3})$	The part of $k_p$ trapped in the separator,
		$k_0 = k_p - k_v$
$k_{p}$	$(g m^{-3}), (kg m^{-3})$	Particle concentration in gas at separator
	,	inlet
$k_{v}$	$(g m^{-3}), (kg m^{-3})$	Particle concentration in gas at separator
		outlet
1	(m)	Thickness of dust layer at time of resistance
		measurement
$m_{ m m}$	(kg)	Mass of solid particle
_	$(m_n^3)$	1 m <sup>3</sup> at +20 °C and 1 atmosphere
$m_{\nu}$	(kg)	Mass of macroparticle of gas
n	$(kg^{-1})$	Number of particles in 1 kg of dust
p	(Pa)	Gas pressure
$p_0$	(Pa)	Reference gas pressure
$p_{p}$	(Pa)	Partial pressure of saturated water vapour
$q_{\rm p}$	$(C kg^{-1})$	Electrical charge of 1 kg of dust
r	$(J kg^{-1} \circ K^{-1})$	Specific gas constant
r	(m)	Half diameter of cyclone outlet
r	(m)	Half diameter of wire electrode
r	(m)	Radius of curvature
$r_{\rm m}$	(m)	Radius of solid particle trajectory
$r_{\rm v}$	(m)	Radius of gas flow line
		1=1

t	(°C)	Temperature
u'	_	Amortization factor of separating equipment
u"	_	Amortization factor of enclosed space in
		buildings
u‴	_	Amortization factor of floor space occupied
		by separators
$v_{i}$	$(m s^{-1})$	Average ion velocity in electric field
$v_m$	$(m s^{-1}), (cm s^{-1})$	Particle velocity
$v_{\mathbf{k}}$	$(m s^{-1}), (cm s^{-1})$	Terminal particle velocity
$v_{p}$	$(m s^{-1}), (cm s^{-1})$	Free falling velocity of particle
$v_{\rm r}$	$(m s^{-1})$	Centripetal velocity component
$v_{\rm u}$	$(m s^{-1})$	Circumferential velocity component
$v_{\mathbf{v}}$	$(m s^{-1}), (cm s^{-1})$	Gas flow velocity
$v_{\star}$	$(m s^{-1})$	Absolute velocity of gas macroparticle
$v_z$	$(m s^{-1})$	Axial velocity component
$v_{\mathrm{D}}$	$(m s^{-1})$	Velocity related to cross section of cyclone
		of diameter D
$v_{ m F}$	$(\text{cm s}^{-1})$	Flow speed of filtered gas
W	$(cm s^{-1})$	Mean (effective) separating brisk velocity in
		electrostatic precipitator
X	$(kg kg^{-1})$	Specific moisture content
A	$(m^3 hour^{-1})$	Make-up water needed for separator
A	$(m^3 kg^{-1})$	Constant for permittivity calculations,
		dependent on gas or particle material
C	$(N m^{-1})$	Surface tension
$C_{\mathbf{a}}$	(crowns m <sup>-3</sup> )	Water costs
$C_{\rm e}$	(crowns kWh <sup>-1</sup> )	Electricity costs
$C_{n}$	(crowns)	Annual costs of spares and replacement parts
$C_{oz}$	(crowns)	Cost price of separating equipment
$C_{p}$	(crowns m <sup>-3</sup> )	Cost of enclosed space in buildings
$C_{u}$	(crowns m <sup>-2</sup> )	Cost of floor space
$C_{12}$	$(N m^{-1})$	Surface tension at interface of solid and liquid
$C_{13}$	$(N m^{-1})$	Surface tension at interface of solid and gas
$C_{23}$	$(N m^{-1})$	Surface tension at interface of liquid and gas
D	$(m^2 s^{-1}), (cm^2 s^{-1})$	Diffusion coefficient
E	(kW)	Power input for fan drive
E'	(kW)	Total power input for separator and all its ancillaries
F	$(V m^{-1})$	Electric field intensity
$F_0$	$(V m^{-1})$	Initial critical intensity of electric field
G	$(kg s^{-1}), (kg hour^{-1})$	Mass flow through separator

$G_{\mathbf{c}}$	(N)	Gravitational force of particle
$G_{m}$	(kg)	Weight of solid particles
$G_{o}$	(kg)	The part of $G_p$ trapped in the separator,
$G_{\mathfrak{p}}$	(kg)	$G_0 = G_p - G_v$ Weight of solid or liquid particles entering the separator
$G_{\mathbf{v}}$	(kg)	Weight of solid or liquid particles leaving the separator untrapped
$H_{d}$	(hours)	Annual shutdown time for replacing com-
$H_{\rm u}$	(hours)	Annual shutdown time for maintenance
1	(A)	Electric current intensity
$K_{\rm m}$	(%)	Cost coefficient for erection and installation
***		work
$K_{p}$	(%)	Cost coefficient for design work
$\dot{M}_{ m d}$	(crowns hour <sup>-1</sup> )	Wage rate of equipment operator, including overheads allowance
$M_{\rm u}$	(crowns hour <sup>-1</sup> )	Wage rate of maintenance worker, including overheads allowance
MO	(microns), (m s <sup>-1</sup> )	Separation limit
N	, , , , , ,	Number of molecules per mol
		(Loschmidt number)
$N_1$	(crowns per 1000 m <sup>3</sup> )*	Cost of project and design work
$N_2$	(crowns per 1000 m <sup>3</sup> )*	Cost price of separating equipment
$N_3$	(crowns per 1000 m <sup>3</sup> )*	Cost of erection/installation work
$N_4$	(crowns per 1000 m <sup>3</sup> )*	Costs of buildings to house separating equipment
$N_4'$	(crowns per 1000 m <sup>3</sup> )*	Cost of site for separating equipment
$N_5$		Electricity costs for fan drive
$N_6$		Total electricity costs for separator operation
$N_7$	(crowns per 1000 m <sup>3</sup> )*	
$N_8$	(crowns per 1000 m <sup>3</sup> )*	Costs of spares and replacements
$N_9$	(crowns per 1000 m <sup>3</sup> )*	Wage bill for operation and routine mainten-
$N_{10}$	(crowns per 1000 3)*	Wage hill for installation of replacements
$O_{\rm c}$	(%)	Wage bill for installation of replacements Overall collecting efficiency
$O_{\rm d}$	(%)	Partial collecting efficiency
$O_{\rm f}$	(%)	Fractional collecting efficiency
P	(N)	Force, electrical forces
A	(14)	rorce, electrical forces

<sup>\*</sup>Note: Costs  $N_1$  to  $N_{10}$  are referred to 1000  $\mathrm{m}^3$  of cleaned gas.

$P_{m}$	$(m^2)$	Particle surface area
$P_{n}$	(N), (kp)	Force perpendicular to the gas flow
$P_{t}$	(N), (kp)	Force opposing the motion of a macroparticle
* t	(11), (NP)	of gas
$P_{\rm m}^{\prime}$	$(m^2 kg^{-1})$	Specific surface area of particles
PMO	(microns), $(m s^{-1})$	Approximate separation limit
P	(Pa)	
	15. 5	Vector of pressure gradient
$P_n$	(Pa)	Pressure gradient component perpendicular to gas flow lines
$\bar{P}_{\rm t}$	(Pa)	Pressure gradient component tangential to gas
I t	(1 a)	flow lines
0	$(m^3 s^{-1}), (m^3 h^{-1})$	Volumetric flow rate
$Q$ $Q_c$	(C)	Electric charge of particles
$Q_{c1}$	(C)	Electric charge of one particle
	$(m^3 s^{-1}), (m^3 h^{-1})$	Throughflow capacity of separator
$Q_{\rm h}$		Saturated particle charge
$Q_n$	(C) (C)	Parcicle charge in time τ
$Q_{\tau}$	$(J \text{ mol}^{-1} {}^{\circ}K^{-1})$	
R R	21 15	Molar gas constant
	(N)	Aerodynamic drag
R	(ohms)	Resistance of dust layer
R	(m)	Half diameter of centrifugal chamber in
D.	(\)	a cyclone
R	(m)	Half diameter of tubular electrode
R	(m)	Gap between wire and plate electrodes
S	$(m^2)$	Surface area of dust layer at time of resistance measurement
T	(K)	Thermodynamic temperature of gas
$T_0$	(K)	Reference absolute temperature of gas
U		Feed voltage
	(V)	
$U_0$	(V)	Initial critical voltage
$U_{\mathfrak{p}}$	(V)	Arc-over voltage
V	$(m^3)$	Enclosed space needed for separator opera- tion and maintenance
V'	(2)	
V	$(m^2)$	Floor space needed for separator operation
17	(3)	and maintenance
V <sub>m</sub>	(m <sup>3</sup> )	Volume of solid particles
$V_{\rm s}$	(m <sup>3</sup> )	Apparent bulk volume
Z	(%)	Proportion of retained particles
Z(a)	_	Retained fractions curve related to a
$Z(v_p)$	_	Retained fractions curve related to $v_{\rm p}$
$-\frac{dZ}{dz}$	-	Particle frequency related to a
da		

$-\frac{\mathrm{d}Z}{\mathrm{d}v_p}$	-	Particle frequency related to $v_p$
$-\frac{\mathrm{d}Z(a)}{\mathrm{d}a}$	j=	Particle size distribution curve related to a
$-\frac{\mathrm{d}Z(v_{\mathrm{p}})}{\mathrm{d}v_{\mathrm{p}}}$	- '	Particle size distribution curve related to $v_{\rm p}$
α	(degrees)	Angle of impact
β	_	Damping coefficient
β	1-	Relative charging coefficient (ratio of real to saturated particle charge)
$\beta_{mean}$	==	Mean relative charging coefficient
S	-	Relative weight of gas in given reference state
3	$(F m^{-1})$	Permittivity
$\varepsilon_0$	$(F m^{-1})$	Permittivity of vacuum (8.855 . 10 <sup>-12</sup> )
$\varepsilon_{\rm r}$	_	Relative permittivity
η	(Pa s)	Dynamic viscosity of gas
9	(degrees)	Angle between liquid/solid interface and
		tangent to liquid surface at point of contact
		between solid, liquid and gas (contact angle)
20	_	Charging coefficient
λ	-	Excess air ratio in combustion process
ν	$(m^2 s^{-1})$	Kinematic viscosity of gas
ξ	_	Drag coefficient of particle
$\xi_{\mathbf{D}}$	_	Aerodynamic resistance coefficient of
		separator
Q	$(kg m^{-3})$	Specific gravity
$\varrho_{i}$	$(C m^{-3})$	Space charge of gas ions
$Q_{im}$	$(C m^{-3})$	Maximum space charge of gas ions
$\varrho_{\mathbf{k}}$	$(kg m^{-3})$	Specific gravity of fluid
$\varrho_{\mathbf{m}}$	$(kg m^{-3})$	Specific gravity of a solid particle
$\varrho_{\rm p}$	$(C m^{-3})$	Space charge of dust
$Q_{pn}$	$(C m^{-3})$	Saturated space charge of dust
$\varrho_{s}$	$(kg m^{-3})$	Bulk density
$\varrho_{\mathrm{st}}$	$(kg m^{-3})$	Tapped density
$\varrho_{\mathbf{v}}$	(ohmmetres)	Specific resistance of dust layer
τ	(s)	Time; time elapsed since start of charging
ω	$(s^{-1})$	Angular velocity
$\Delta h$	(Pa)	Pressure drop across the separator at $\varrho = 1 \text{ kg m}^{-3}$
$\Delta p$	(Pa)	Pressure drop across the separator
$\Delta p_{\mathrm{F}}$	(Pa)	Pressure gradient across filter cloth

11.

# Explanations of some of the terms

#### Particle diameter a (microns or m)

This measure of solid or liquid particle sizes is either the diameter of a spherical particle which will just pass through a screen with a mesh size of a, or else the diameter of a fictitious spherical particle with the same free falling velocity and same specific gravity as the real particle under consideration (i.e the equivalent particle diameter).

# Free falling velocity $v_p$ (m s<sup>-1</sup>)

This is the speed at which the particle will descend, under the effect of gravity alone, in a stationary volume of carrier gas. For Reynolds' numbers up to and including unity, it can with sufficient accuracy be established from Stokes's expression

$$v_{\rm p} = \frac{1}{18} a^2 \frac{\varrho_2 - \varrho_1}{\eta} g \tag{1}$$

Terminal velocity vk (m s-1)

This is the ultimate speed which the particle will attain, relative to the carrier gas, under the effects of the equilibrium of forces acting upon it in the separator.

## Proportion of retained particles Z (%)

This is the numerical proportion, or proportion by weight, of particles which exceed a specified value of the parameter which characterizes the particle size; in other words, which exceed a given mesh size, equivalent diameter, free falling velocity, or actual particle size, in terms of a or  $v_p$ .

# Retained fractions curve Z(a) or Z(vp)

This curve (Fig. 1) shows how the magnitude of Z varies with the value of the characteristic parameter a or  $v_p$ .

Particle incidence 
$$-\frac{dZ}{da}$$
 or  $-\frac{dZ}{dv_p}$ 

This quantity, related either to the number of particles or to their weight, is the negative value of the figure obtained by differentiation of the retained particle proportion Z by the size-governing parameter (a or  $v_p$ ).

Particle size distribution curve 
$$-\frac{dZ(a)}{da}$$
 or  $-\frac{dZ(v_p)}{dv_p}$ 

This curve (Fig. 1) indicates how the frequency of incidence of any given particle size varies with the value of the size-governing parameter (such as a or  $v_p$ ).

## Overall collecting efficiency Oc (%)

This is the ratio (multiplied by 100) between the weight of solid or liquid particles trapped in the separator  $(G_0)$  and the weight of these particles  $(G_p)$  entering that separator in the carrier gas within a certain span of time, at a certain flow rate and physical state of the carrier gas, and given a certain concentration and a certain set of physical properties of the particles,

$$O_{\rm c} = \frac{G_{\rm o}}{G_{\rm p}} 100 \tag{2}$$

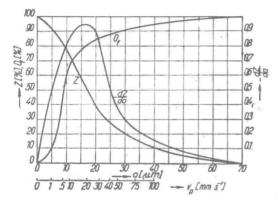


Fig. 1 How the proportion of retained particles Z, the particle frequency  $-\frac{dZ}{da}$ , and the fractional collecting efficiency  $O_t$  vary with the equivalent particle size a.

Since the weight of solid or liquid particles entering the separator equals the sum of the weight of particles trapped  $(G_0)$  and the weight of particles leaving the separator untrapped  $(G_v)$ , i.e.  $G_p = G_0 + G_v$ , we can also define  $O_c$  as

$$O_{c} = \frac{G_{o}}{G_{o} + G_{v}} 100 = \frac{G_{p} - G_{v}}{G_{p}} 100$$
(3)

## Fractional collecting efficiency Of (%)

This is the ratio (multiplied by 100) between the weight of solid or liquid particles with a certain magnitude of the size-governing parameter which are trapped in the separator, and the weight of particles with the same magnitude of that parameter which enter the separator in the carrier gas, again at a certain flow rate and physical