

The Force Analogy Method for Earthquake Engineering

Gang Li Kevin K.F. Wong

WILEY

THEORY OF NONLINEAR STRUCTURAL ANALYSIS

THE FORCE ANALOGY METHOD FOR EARTHQUAKE ENGINEERING

Gang Li

Dalian University of Technology, China

Kevin K.F. Wong

Ph.D., University of California Los Angeles, USA



This edition first published 2014 © 2014 John Wiley & Sons, Singapore Pte. Ltd.

Registered Office

John Wiley & Sons, Singapore Pte. Ltd., 1 Fusionopolis Walk, #07-01 Solaris South Tower, Singapore 138628.

For details of our global editorial offices, for customer services and for information about how to apply for permission to reuse the copyright material in this book please see our website at www.wiley.com.

All Rights Reserved. No part of this publication may be reproduced, stored in a retrieval system or transmitted, in any form or by any means, electronic, mechanical, photocopying, recording, scanning, or otherwise, except as expressly permitted by law, without either the prior written permission of the Publisher, or authorization through payment of the appropriate photocopy fee to the Copyright Clearance Center. Requests for permission should be addressed to the Publisher, John Wiley & Sons, Singapore Pte. Ltd., 1 Fusionopolis Walk, #07-01 Solaris South Tower, Singapore 138628, tel: 65–66438000, fax: 65–66438008, email: enquiry@wiley.com.

Wiley also publishes its books in a variety of electronic formats. Some content that appears in print may not be available in electronic books.

Designations used by companies to distinguish their products are often claimed as trademarks. All brand names and product names used in this book are trade names, service marks, trademarks or registered trademarks of their respective owners. The Publisher is not associated with any product or vendor mentioned in this book. This publication is designed to provide accurate and authoritative information in regard to the subject matter covered. It is sold on the understanding that the Publisher is not engaged in rendering professional services. If professional advice or other expert assistance is required, the services of a competent professional should be sought.

Limit of Liability/Disclaimer of Warranty: While the publisher and author have used their best efforts in preparing this book, they make no representations or warranties with respect to the accuracy or completeness of the contents of this book and specifically disclaim any implied warranties of merchantability or fitness for a particular purpose. It is sold on the understanding that the publisher is not engaged in rendering professional services and neither the publisher nor the author shall be liable for damages arising herefrom. If professional advice or other expert assistance is required, the services of a competent professional should be sought.

Library of Congress Cataloging-in-Publication Data applied for.

ISBN: 978-1-118-71806-3

A catalogue record for this book is available from the British Library. Printed and bound in Singapore by Markono Print Media Pte Ltd.

1 2014

Preface

Although the seismic design for buildings is currently based on elastic analysis, nonlinear structural analysis has become increasingly important in the investigation of structural response to environmental loads, especially during earthquakes. Nonlinear structural analysis in civil engineering is not a new topic, but the existing method used for calculating the nonlinear behavior of civil engineering structures is often by changing the structural member stiffness. With respect to the dynamic analysis algorithms, the typical method is the time integral of variable stiffness matrices, such as the Wilson- θ and Newmark- β methods. For these conventional methods, the primary problem is that significant iterative computations have to be carried out to ensure numerical convergence once the structure experiences yielding and nonlinear deformation. As a result, the iterative operation is time consuming and the entire dynamic analysis process becomes practically uneconomical. The Force Analogy Method as a relatively new algorithm was first developed in 1999 for solving nonlinear dynamic analysis problems, in which the state transition matrix needs to be computed only once due to the consistent use of initial stiffness, and this greatly simplifies the overall computation and makes the nonlinear analysis readily available for solving various practical problems.

This book focused on the Force Analogy Method, a novel method for nonlinear dynamic analysis and simulation. A review of the current nonlinear analysis method for earthquake engineering is summarized and its importance explained. Additionally, how the force analogy method can be used in nonlinear static analysis will be discussed through several nonlinear static examples. The emphasis of this book is to extend and develop the force analogy method to performing dynamic analysis on structures under earthquake excitations, where the force analogy method is incorporated in the flexural element, axial element, shearing element and so on will be exhibited. Moreover, the geometric nonlinearity into nonlinear dynamic analysis algorithm based on the force analogy method is included in this book. The application of the force analogy method in seismic design for buildings and structural control area will be discussed combined with practical engineering. This book will be a milestone of nonlinear dynamic analysis and may bring about significant advancement in earthquake engineering.

Preface

The authors would like to express their appreciation to Professor Hong-Nan Li at the Dalian University of Technology (DUT), for his advice and support, Professor Larry A. Fahnestock at University of Illinois at Urbana & Champaign, Mr. Yu Zhang, a Ph. D candidate at DUT, and Mr. Feng Zhang, a graduate student at DUT, for their collaborative works, and Mr. Ying Li, for his early contributions. In addition, many thanks go to Zhi-Qian Dong, Yong-Qiang Jin, Jia-Long Li and Li-Hua Zhu, present students at DUT, for their work on the figures.

Gang Li

About the Authors

Gang Li is an associate professor of the Faculty of Infrastructure Engineering, Dalian University of Technology, China. He received a B.S. degree in civil engineering from the Hebei University of Engineering, China and Ph.D. degree in civil engineering from the Dalian University of Technology, China. His research interest is in the earthquake engineering, structural control, structural dynamic analysis, steel structures, large-scale structural experiments, etc. Some of his techniques have been applied to many engineering structures.

Kevin K.F. Wong is a research structural engineer at the National Institute of Standards and Technology (NIST) in the United States. He received a B.S. degree in civil engineering from the University of Hawaii and M.S. and Ph.D. degrees in civil engineering from the University of California, Los Angeles (UCLA). His research areas include structural dynamics, nonlinear structural analysis, earthquake engineering, and structural control.

Dr. Wong was first exposed to the Force Analogy Method as a graduate research assistant under the supervision of Dr. T. H. Lin at UCLA in 1992 while conducting research on the development of plastic strains in high-cycle fatigue of materials. He successfully captured the essence of the method and applied it to the nonlinear analysis of civil engineering structures, where he summarized the work in his Ph.D. thesis titled *Optimal Linear Control of Inelastic Building Response During Earthquakes* in 1996. Since then, he has published over 30 journal articles and 30 conference papers related to the method.

Prior to joining NIST, Dr. Wong was an assistant professor at the University of Utah, USA, for four years, and the Nanyang Technological University, Singapore, for six years. He coauthored the textbook *Structural Dynamics for Structural Engineers* for John Wiley & Sons in 2000 with his Ph.D. advisor, Dr. Gary Hart. Currently at NIST, he is a member of the National Earthquake Hazards Reduction Program research group, conducting research on the development of Codes and Standards on the use of nonlinear analysis for performance-based seismic engineering.

xii About the Authors

Disclaimers:

The opinions expressed in this book are those of the authors and do not necessarily reflect the opinions of the National Institute of Standards and Technology or the United States Government. While the information in this book is believed to be correct, the National Institute of Standards and Technology and the authors assume no liability for, nor express or imply any warranty with regard to, the information contained herein. Users of the information contained in this book assume all liability arising from such use.

Contents

	Preface			
About the Authors				
1	Introduction			
	1.1 History of the Force Analogy Method	1		
	1.2 Applications of the Force Analogy Method	4		
	1,2.1 Structural Vibration Control	4		
	1.2.2 Modal Dynamic Analysis Method	6		
	1.2.3 Other Design and Analysis Areas	6		
	1.3 Background of the Force Analogy Method	6		
	References	14		
2	Nonlinear Static Analysis			
	2.1 Plastic Rotation	17		
	2.2 Force Analogy Method for Static Single-Degree-of-Freedom Systems	19		
	2.2.1 Inelastic Displacement	19		
	2.2.2 Application of the FAM on SDOF System	20		
	2.2.3 Nonlinear Analysis Using FAM	22		
	2.3 Nonlinear Structural Analysis of Moment-Resisting Frames	26		
	2.4 Force Analogy Method for Static Multi-Degree-of-Freedom Systems	31		
	2.5 Nonlinear Static Examples	36		
	2.6 Static Condensation	52		
	References	61		
3	Nonlinear Dynamic Analysis			
	3.1 State Space Method for Linear Dynamic Analysis	63		
	3.1.1 Equation of Motion	64		
	3.1.2 State Space Solution	66		
	3.1.3 Salution Proceedings	60		

vi

	3.2	Dynamic Analysis with Material Nonlinearity	72			
		3.2.1 Force Analogy Method	72			
		3.2.2 State Space Analysis with the Force Analogy Method	74			
		3.2.3 Solution Procedure	76			
	3.3	Nonlinear Dynamic Analysis with Static Condensation	87 99			
	3.4 Nonlinear Dynamic Examples					
	Refe	rences	109			
4	Flex	Flexural Member				
	4.1	Bending and Shear Behaviors	111			
		4.1.1 Hysteretic Models	111			
		4.1.2 Displacement Decomposition	113			
		4.1.3 Local Plastic Mechanisms	115			
	4.2	Inelastic Mechanisms of Flexural Members	115			
		4.2.1 Elastic Displacement x^{\prime}	116			
		4.2.2 Plastic Bending Displacement x_1''	117			
		4.2.3 Plastic Shear Displacement x_2''	117			
		4.2.4 Combination of the Bending and Shear Behaviors	117			
	4.3	Nonlinear Static Analysis of Structures with Flexural Members	118			
		4.3.1 Force Analogy Method for Static Single-Degree-of-Freedom Systems	118			
		4.3.2 Force Analogy Method for Static Multi-Degree-of-Freedom Systems	129			
	4.4	Nonlinear Dynamic Analysis of Structures with Flexural Members	143			
		4.4.1 Hysteretic Behaviors of the Flexural Members	143			
		4.4.2 Solution Procedure of the FAM	146			
	Refe	erences	159			
5	Axial Deformation Member					
	5.1	Physical Theory Models for Axial Members	161			
		5.1.1 General Parameters	162			
		5.1.2 Displacement Decomposition	163			
	5.2	Sliding Hinge Mechanisms	164			
	5.3	Force Analogy Method for Static Axial Members	166			
		5.3.1 Regions $O-A_a$ and $O-F$	166			
		5.3.2 Region F–G	166			
		5.3.3 Regions A_a -A and A -B	167			
	5.4	Force Analogy Method for Cycling Response Analysis of Axial Members	170			
		5.4.1 Region B–C	170			
		5.4.2 Region C–D	171			
		5.4.3 Region $D'-A_2$	172			
		5.4.4 Region D–E	173			
		5.4.5 Region E–F	174			
		5.4.6 Region A_{a2} – A_2	174			
	5.5	Application of the Force Analogy Method in Concentrically Braced Frames	178			
		5.5.1 Force Analogy Method for Static SDOF CBFs	178			

Contents

		5.5.2 5.5.3	Force Analogy Method for Static MDOF CBFs Force Analogy Method for Dynamical CBFs under	182		
			Earthquake Loads	188		
	Refe	rences		194		
6	Shear Member					
	6.1	Physic	al Theory Models of Shear Members	195		
			Flexural Behavior	195		
		6.1.2	Axial Behavior	197		
		6.1.3	Shear Behavior	197		
	6.2	Local	Plastic Mechanisms in the FAM	198		
		6.2.1	Displacement Decomposition	198		
		6.2.2	Behavior of VSH	199		
		6.2.3	Behavior of HSH	200		
	6.3	Nonlii	near Static Analysis of the Shear Wall Structures	201		
	6.4	Nonli	near Dynamic Analysis of RC Frame-Shear Wall Structures	222		
		6.4.1	Hysteretic Behaviors of the RC Shear Wall Members	222		
		6.4.2	Solution Procedure of the FAM	224		
	Refe	erences		234		
7	Geometric Nonlinearity					
	7.1	Classi	cal Stiffness Matrices with Geometric Nonlinearity	236		
		7.1.1	The P - Δ Approach	237		
		7.1.2	The Geometric Stiffness Approach	238		
	7.2	Stabil	ity Functions	239		
		7.2.1	Stiffness Matrix $[\mathbf{K}_i]$	240		
		7.2.2	Stiffness Matrix $[\mathbf{K}'_i]$	244		
		7.2.3	Stiffness Matrix $[\mathbf{K}_{i}^{"}]$	246		
	7.3		Analogy Method with Stability Functions	250		
	7.4	Nonli	near Dynamic Analysis Using Stability Functions	261		
			Force Analogy Method	261		
		7.4.2	Nonlinear Dynamic Analysis with the Force Analogy Method	262		
	7.5	7.4.3 Nonli	State Space Analysis with Geometric and Material Nonlinearities near Dynamic Analysis with Static Condensation Using	263		
	1.00		ity Functions	272		
	7.6		near Dynamic Examples	283		
		erences	near Bynamic Examples	294		
8	Application of the Force Analogy Method in Modal Superposition 29					
	8.1	Nonli	near Static Pushover Analysis in the FAM	298		
	U.1	8.1.1	NSPA for Mass-Normalized SDOF Systems	299		
		8.1.2	NSPA for Multi-Degree-of-Freedom Systems	303		
	8.2		Il Decomposition in the FAM	312		
	77 7 000			0.14		

351

Index

Introduction

1.1 History of the Force Analogy Method

The force analogy method (FAM) is an analytical tool for solving structural analysis problems with material nonlinearity. It uses the concept of "inelastic displacement", or more commonly known as the "residual displacement" in the formulation, where the nonlinear stiffness force due to material nonlinearity is represented by a change in displacement instead of a change in stiffness. The original concept of FAM was first introduced by Lin (1968), where the proposed method was actually applied to stress and strain in continuum mechanics with the inelastic behavior defined by plastic strain. Unfortunately, this concept only found limited acceptance because it was developed at approximately the same time as researchers were focusing their attention on studying the deformation of solids using numerical simulation methods, such as the finite element method with the inelastic behavior defined by changing stiffness. Although the finite element method is a powerful tool and widely used, the procedure of the step-by-step numerical integration is unavoidable, time consuming, cumbersome, and costly for practical design in 1980s and even today.

Recognizing that nonlinear finite element method of analysis is a time-consuming process, many structural engineers are constantly seeking a simplified dynamic analysis approach for analyzing nonlinear multi-degree-of-freedom (MDOF) systems to carry out their structural designs. One simplified approach is to represent the nonlinear MDOF system as an elastic system, in which structural response can be estimated by response spectra analysis of using the convenient and efficient modal superposition method. Newmark (1970) proposed a well-known method of extending the elastic response spectra analysis to engineering design of nonlinear systems through the use of inelastic response spectra. However, the method is strictly valid for single-degree-of-freedom (SDOF) systems and thus is inadequate for the analysis

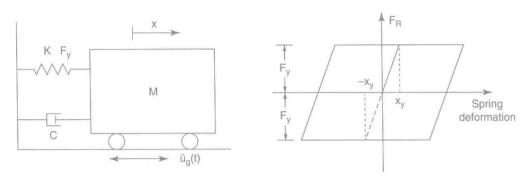


Figure 1.1 SDOF system and restoring force model.

of nonlinear MDOF systems due to the changing stiffness matrix. The changing stiffness matrix in the equations of motion for the nonlinear MDOF system is the drawback of this method, since the nonlinearity effect is coupled in each and every mode. Thus, significant effort was spent towards extending the modal superposition method in elastic analysis to inelastic analysis. One effort similar to the FAM, where the restoring force term of nonlinear MDOF systems was expressed by the sum of the elastic restoring force and additional external force, was presented by Villaverde (1988, 1996). After moving the additional external force term to the right-hand side of the equation of motion, the left-hand side of the equation is interpreted as an equivalent linear system. A different approximate modal decomposition method for the equation of motion was subsequently presented by Georgoussis (2008). While the above works emphasized the development of simplified analysis methods, only simple system models and load–deformation relationships, such as those shown in Figure 1.1, were selected to explore the physical significance of the external force term. The relationship between the external force term and inelastic behavior of structural members were ignored at that time.

The same problem was encountered by Wong (1996) during his study on the structural control of nonlinear structures. Since the theory of state space dynamic analysis, as a computing platform for performing structural control calculation, was only applicable to elastic systems, it was an obvious barrier when apply the structural control technique in nonlinear structures. Thus, a method of analyzing the inelastic response of the building by recovering the forces from the states of the building was introduced. Subsequently, Wong and Yang (1999) formally published the first application of the FAM for civil structures where the method was formulated in force-deformation space for inelastic dynamic analysis. The fundamental concept of the FAM is that each inelastic deformation in the structure is formulated as a degree of freedom such that the initial stiffness matrix is computed only once at the beginning and can be used throughout the inelastic analysis. Coupling the FAM with the state space formulation for dynamic analysis provides an accurate, efficient, and stable solution algorithm such that it can be used to analyze structures with various material properties, not only for elastic-plastic property but also for both hardening and softening properties. In addition, the external force term was interpreted as the force analogy, which causes inelastic deformation of structural members at certain locations in the structure. The inelastic deformation includes nonlinear extension of the braces in a braced frame, plastic rotation of the beams and columns in a moment resisting frame, or yielding of the base isolators in a base isolation system. Since then, Zhao and Wong (2006) further

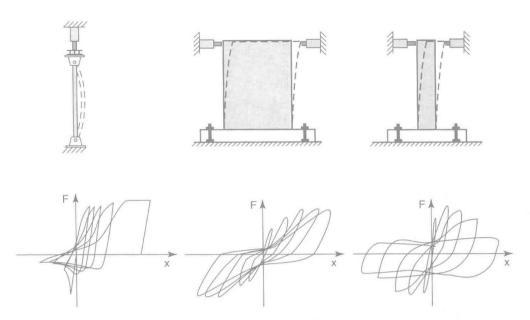


Figure 1.2 Complex cyclic behaviors of structural members.

developed the FAM by incorporating the geometric nonlinear effect and presented a comprehensive nonlinear approach for inelastic framed structures, including geometric nonlinearity and material nonlinearity. The approach uses finite element formulation to derive the elemental stiffness matrices, particularly to derive the geometric stiffness matrix in a general form. However, the geometric stiffness matrix used in the nonlinear formulation was not exact, and further improvement by Wong (2012, 2013) was recently conducted and will be presented in Chapter 7.

Although Wong and Yang (1999) pointed out that all material properties can be used in the FAM and they have no influence on the algorithm stability, only nonlinear response of a steel moment-resistant frame with simple bilinear moment versus plastic rotation relationship was mentioned in the study. In fact, structural members often exhibit complex cyclic inelastic behavior (i.e. buckling of braces, strength degradation of reinforced concrete members, as shown in Figure 1.2) when they undergo excessive dynamic loadings, and some well-known models have been proposed and developed. It is clear that updating element local stiffness matrices, re-assembling them and performing static condensation to derive system global tangent stiffness matrix is not necessary in the FAM. However, existing material models cannot be applied in the FAM directly because they often reveal a highly nonlinear relation of the external force and total deformation rather than plastic deformation. Since the global behavior of nonlinear structures is closely associated with the relationship between the internal force and plastic deformation, some investigations were carried out to extend the application of the FAM for structural members with different material behaviors.

Chao and Loh (2007) used three different plastic mechanisms to simulate the reinforced concrete beam-column elements in the FAM. The load versus deformation comparison shows that the proposed algorithm gives results very similar to experimental data. Additionally,

the *P*-Delta effect also has been considered in this study. Li *et al.* (2013a) implemented an existing brace physical theory model for use in the FAM. In the procedure, the physical theory model developed by Dicleli and Calik (2008) is chosen for implementation in the FAM, because it is a relatively simple and efficient model that has been shown to provide reasonable accuracy. Two sliding plastic mechanisms, which simulate axial displacements produced by transverse brace displacement and the so-called growth effect, are used to represent the inelastic brace behavior. The resulting model is shown to provide good agreement with experimental data. Moreover, this brace model is implemented in a frame where inelastic response occurs in both the frame and braces to demonstrate the value of the brace model and the potential for simulating complex inelastic dynamic behavior of concentric braced frames with the FAM. The model is validated against prior experimental results to be an accurate, efficient, and stable algorithm for conducting dynamic analysis when coupled with the state space formulation.

In addition, Li and Zhang (2013b) developed a framework for the seismic damage analysis of reinforced concrete frame structures considering the stiffness degradation based on the FAM. A damage hinge model, which is located at the ends of columns and beams, is proposed for modeling damage behavior due to concrete cracking. As a damage effect is implemented by introducing the damage indices as internal variables, the real-time structural performance and damage level can be evaluated during the computation process. The damage hinge, together with the plastic hinge arising from structural materials, forms a complete inelastic mechanism including stiffness degradation behavior for reinforced concrete frame structures. Since only initial stiffness is used throughout the dynamic computation analysis, the usage of the state space formulation, as an outstanding advantage of the FAM, is retained and makes the real-time damage analysis more accurate, efficient, and stable. As for the reinforced concrete shear wall member, a procedure for modeling the hysteretic response of reinforced concrete shear wall members based on the existing models in the FAM was established and will be discussed in Chapter 6. An reinforced concrete (RC) flexural member model, where the strength deterioration and stiffness degradation effect due to increasing loading cycles, and the pinching behavior that mainly roots in the crack opening and closing during loading reversals are considered, was established and incorporated in the FAM. The methodology will be presented in Chapter 4 together with several examples.

1.2 Applications of the Force Analogy Method

Because the FAM has two outstanding benefits in terms of computation efficiency and stability, it has the advantage over other analysis tools for the following applications:

1.2.1 Structural Vibration Control

Since the concept of structural vibration control in civil engineering was proposed by J.T.P Yao in 1972, it has made considerable progress in the development of theoretical and experimental researches. A number of structural control techniques and strategies have been developed and applied in practices, specifically in seismic regions. The structural vibration control began in the mechanical engineering in the early 20th century and the majority of control theories,

Introduction 5

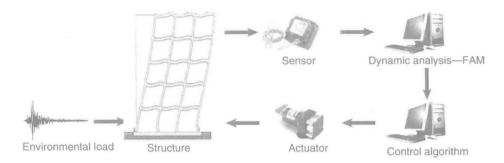


Figure 1.3 The framework for the combination of FAM and control algorithm.

includes the linear quadratic regulator, modal control, smart control, H2 control, $H\infty$ control, etc., and algorithms were applied to elastic systems and have been matured. These control algorithms together with dynamic analysis procedure run together for determining controlling force of actuators, as shown in Figure 1.3. However, structural members in civil engineering buildings will always experience inelastic deformation when the buildings are subjected to excessive loadings. This causes significant problems, such as time delay, incompatible program, etc., during the combination of inelastic computation procedures and control algorithms.

The emergence of the FAM provides a way to solve this type of problem because the left-hand side of the equation of motion of nonlinear systems retains the linear properties of corresponding elastic system. Thus, many problems, which are relatively difficult to answer while applying traditional control algorithms to inelastic systems, have been solved to some degrees using the FAM. Wong and Yang (2003) and Wong (2005) proposed inelastic structural control algorithms, which compensates for the time delay that happens in practical control systems, through incorporating the FAM with the predictive instantaneous optimal control algorithm and the predictive instantaneous optimal control algorithm, respectively. Moreover, since the earthquake ground velocity is not at high frequency as compared with the ground acceleration, it can be predicted at certain time steps beforehand in the real-time domain with higher accuracy. Thus, Pang and Wong (2006) proposed a simple control algorithm expressed using the input ground velocity, namely the Predictive Instantaneous Optimal Control algorithm.

To capture the damaging effects during earthquake ground motions, the FAM is used to characterize structures responding in the inelastic domain. Li and Li (2011a) developed an approach based on the FAM to analyze the dynamic response of structure with energy-dissipation devices. The proposed algorithm is applicable to a variety of energy-dissipation devices by turning them to the equivalent force applied at the joints of the frame. Wong (2008) and Wong and Johnson (2009) presented studies on the use of tuned mass dampers as a passive energy-dissipation device to investigate the benefits of using such devices in reducing the inelastic structural responses. In addition, Wong (2011a) presented a simple numerical algorithm based on the combination of the state space method and FAM to calculate the inelastic dynamic analysis of structures with nonlinear fluid viscous dampers. Finally, Li et al. (2011b) proposed a control algorithm for inelastic structures through combining the market-based control strategy and force analogy method. The framework of this work will be discussed in Chapter 9.

1.2.2 Modal Dynamic Analysis Method

Since each term on the left-hand side of the equation of motion for nonlinear MDOF systems is feasible for modal decomposition like elastic systems, it suggests that the FAM is probably a good baseline for applying the modal dynamic analysis method to solve nonlinear MDOF system problems. Wong (2011b) extended the modal superposition to the nonlinear domain by using the FAM to address material nonlinearity. In addition, because linear modal superposition has found great acceptance in performance-based seismic engineering, geometric nonlinearity is incorporated into the analysis using stability functions. Through the combination of FAM, stability functions, the state space method, and modal superposition, numerical simulations are performed and results are demonstrated to be both accurate and efficient. Moreover, a simple analysis tool for capturing the effect of rigid-end offsets in framed structures under earthquake excitation has been incorporated into the above nonlinear modal analysis methodology by Wong (2012). Author also demonstrated that the equation of motion for nonlinear MDOF systems in the FAM can be uncoupled, but two other governing equations in the FAM relating the internal force, such as the moment and force of structural members are not decomposable. However, uncoupled modal SDOF system responses can be determined by incorporating the FAM with the modal pushover analysis method such that the modal superposition method is suitable for the solution of the nonlinear MDOF system. Although the procedure presented is still an approximation method due to the modal pushover analysis method application, its value and potential for the maximum displacement estimation of the nonlinear MDOF system based on the FAM were validated. The procedure will be discussed in Chapter 8 along with examples.

1.2.3 Other Design and Analysis Areas

Wong and Yang (2002) derived the plastic energy dissipation of structures based on the FAM and used the energy as the response parameter in evaluating the performance of the structure, and Wong and Wang (2003) extended the energy-balance equation to include control energy as an addition form of energy dissipation to resist earthquake inputs. In these studies, the FAM was modified and extended to analyze real moment-resisting frames with zero rotational mass moment of inertia using the method of static condensation. The static condensation method in the FAM will be discussed in Chapter 2 for static analysis and Chapter 3 for dynamic analysis.

Wang and Wong (2007) introduced the FAM for the first time into the field of stochastic dynamic analysis for inelastic structures. This stochastic FAM maintains the advantage of high efficiency in the numerical computation of the FAM in dynamic analysis. According to the stochastic FAM, the variance covariance functions of inelastic dynamic responses, such as displacement, velocity, inelastic displacement of the entire moment-resisting framed structures, and plastic rotation at individual plastic hinge location, can be produced for structures subjected to random excitation.

1.3 Background of the Force Analogy Method

The first step in learning the force analogy method for solving nonlinear structure problems is to understand the matrix method of structural analysis. Because understanding each term in the stiffness matrix (i.e. $12EI/L^3$, $6EI/L^2$, 4EI/L, and 2EI/L) is so important