BIOMEDICAL INSTRUMENTS: THEORY AND DESIGN

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Preface

Since 1966, we have offered a one-year course entitled "Theory and Design of Biomedical Instruments" as part of the Rutgers University graduate program in biomedical engineering. Although several fundamental books on biomedical instrumentation are available, most of them are addressed to instrument users such as physicians and hospital technicians rather than to engineers. It was necessary, therefore, to prepare notes for our design course, and this book is based upon these notes. The book is written at the level of a senior or beginning graduate engineering student.

The book aims at (a) presenting a physical explanation for the behavior of various transducers, (b) developing the mathematical theory applicable to these transducers, and (c) discussing the practical design of biomedical instruments. Our hope is that the book will serve as a text for biomedical engineering students who will be engaged in the design of instruments, as a reference book for medical instrument designers, and as a source of ideas for the large numbers of biomedical research workers who, at one time or another, must build a gadget to implement their research. Numerous examples of medical instrument design are presented in order to clarify the mathematical analyses.

Chapter 1 introduces the reader to various concepts involved in physiological measurements and to transducers employed to implement these measurements. Chapter 2 provides background in the various analytical techniques that are utilized throughout the book, and acts as a "refresher course" for readers who are not currently using them. Since the book is organized around transduction mechanisms, Chapters 3–9 indicate how each transduction technique can be used in the design of instruments. Because ultrasonic systems have an ever-increasing application in the medical field, Chapter 5 describes some techniques in ultrasonic system design. Most of the electromechanical transducers described need some electronic signal conditioning; the design of signal conditioning amplifiers is covered in Chapter 11. The remaining chapters cover the important, but specialized, areas of computerized radiographic imaging, closed-feedback-loop instrument design, and biotelemetry.

The theory and design of biomedical instruments draws upon many different scientific disciplines – physiology, system analysis, circuit theory, solid state physics, acoustics, electromagnetic theory, and so forth. Each of these

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disciplines has evolved its own language and set of symbols. This has made it particularly difficult to generate a list of symbols that bears a close resemblance to those that are typically employed in each separate discipline.

The authors would like to thank their many colleagues for stimulating discussions on medical instrumentation. We are grateful to the students whose classroom questions and comments and examination pitfalls are inevitably reflected in the final product. We are indebted to Mrs. Constance Zylman for typing the manuscript. Finally, we wish to thank the publishers and authors who gave us permission to reproduce many of the figures from the literature.

List of Symbols

а	acceleration	$l_{\rm c}$	length of core
a_n	peak cosine component	$l_{\mathbf{d}}$	dielectric-slab thickness
a_{o}	a particular acceleration	$l_{\mathbf{e}}$	effective length
b	a constant	$l_{\mathbf{F}}$	focal length
b_n	peak sine component	$l_{\mathbf{g}}^{-}$	air-gap length
c	a constant	$l_{\mathbf{g0}}^{\sigma}$	quiescent air-gap length
c_n	spectral component	$l_{\rm m}$	magnetic-path length
d	diameter	l_{o}	reference-temperature length
d_{B}	beam diameter	$l_{\mathbf{p}}$	length of primary
$d_{\rm c}$	coil-form diameter	$l_{\mathbf{R}}^{r}$	depth resolution
$d_{\mathbf{p}}$	piezoelectric constant	$l_{\rm s}$	length of secondary
d_{T}	transducer diameter	m	mass
$d_{\mathbf{w}}$	wire diameter	m_l	strain-gage factor
e	transducer constant	n	an integer
f	frequency	p	pressure
$f_{\mathbf{a}}$	parallel resonant frequency	p_c	cardiac pressure
$f_{\mathbf{BW}}$	frequency bandwidth	$p_{\mathbf{g}}$	gage pressure
f_{0}	resonant frequency	q	charge
$f_{\mathbf{r}}$	series resonant frequency	r	radius
$f_{\mathbf{R}}$	received frequency	$r_{\mathbf{a}}$	average radius, membrane radius
$f_{\mathbf{T}}$	transmitted frequency	$r_{\rm c}$	core radius
g	magnetostrictive constant	$r_{\rm i}$	inner radius
gp	piezoelectric constant	r_0	outer radius, maximum radius
'n	height, thickness, depth	s	$j\omega$
i	magnetic loss factor	t	time
j	$(-1)^{1/2}$	$t_{\mathbf{c}}$	period of one cycle
k	coefficient of coupling	$t_{\mathbf{d}}$	downstream transit time
$k_{\mathbf{a}}$	voltage gain of amplifier	t_{o}	time delay
$k_{\mathbf{B}}$	Boltzmann's constant	tout	period of output pulse
k_{c}	controller gain	t_{p}	pulse period
$k_{\mathbf{d}}$	damping constant	$t_{\mathbf{u}}$	upstream transit time
$k_{\mathbf{f}}$	restoring-force constant	t_{ν}	normalized time
$k_{\mathbf{g}}$	transducer constant	и	a variable, function of radius,
k_{o}	proportionality constant, voltage gain		horizontal component
	of active device	$oldsymbol{v}$	velocity, vertical component
$k_{\mathbf{p}}$	transducer constant	$v_{\mathbf{a}}$	average velocity
$k_{\mathbf{r}}$	spring constant	$v_{\mathbf{f}}$	flow velocity
$k_{\mathbf{t}}$	restoring torque constant	v_l	velocity at $x = l$
l	length	$v_{\rm o}$	velocity at $x = 0$

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	peak sinusoidal velocity		conductance
-	radial component of velocity		compensating conductance
3	velocity of sound		magnetic field intensity
•••	x component of velocity	H_{c}	coercive force
,	y component of velocity	I	current
-	z component of velocity	$I_{\mathbf{p}}$	power density
•	angular component of velocity	Ĵ	current density
w	width	J_n	Bessel function of the first kind
	distance	K	dielectric constant
	quiescent input, horizontal shift	K_{o}	quiescent dielectric constant
$x_{\mathbf{p}}$	horizontal width	\boldsymbol{L}	inductance
x_{ν}	normalized distance	$L_{\mathbf{c}}$	inductance of core section
y	distance	L_{o}	quiescent inductance, a particular
y_0	quiescent output, vertical shift	_	inductance
y_p	vertical width	$L_{\mathbf{p}}$	inductance of primary
Z	distance	$L_{\mathbf{s}}$	inductance of secondary
$z_{\mathbf{k}}$	an X-ray density	M	magnetomotive force
		$M_{\rm m}$	magnetomotive force of magnet
\boldsymbol{A}	area		magnitude response
$A_{\mathbf{g}}$	air-gap cross-sectional area	N	number of turns
$A_{\rm m}$	magnet cross-sectional area	N_n	Bessel function of the second kind
$A_{\mathfrak{p}}$	area of primary coil	Np	primary turns
A_{s}	area of secondary coil	$N_{\rm s}$	secondary turns
В	magnetic flux density	$N_{\rm T}$	primary/secondary turns ratio
$B_{\mathbf{A}}$	flux density at point A	P	power
$B_{\rm m}$	flux density of magnet	$P_{\mathbf{E}}$	electric polarization
B_{r}	residual flux density	Q	quality factor
$\boldsymbol{B}_{\mathbf{x}}$	x component of flux density	Q_{V}	flow volume
B_{y}	y component of flux density	R	resistance
B_z	z component of flux density	R_{c}	compensating resistance
C	capacitance	$R_{\mathbf{f}}$	feedback resistance
$C_{\mathbf{d}}$	capacitance of dielectric slab	R_{i}	input resistance of active device input resistance seen by noninverting
$C_{\mathbf{f}}$	feedback capacitance	R_{inn}	generator
$C_{\rm g}$	air-gap capacitance	D.	•
$c_{\rm L}$	load capacitance	Rinv	generator
C_{o}	quiescent capacitance, a particular	D.	load resistance
_	capacitance	R_{L}	resistance of noninverting source
$C_{\rm s}$	capacitance across secondary	R_{n}	resistance at reference temperature,
C_{v}	inverting source capacitance	Λo	output resistance of active device
D	electric flux density	$R_{\mathbf{p}}$	potentiometer resistance, parallel
D_{x}	x component of flux density	Мp	resistance
D_{y}	y component of flux density	$R_{\rm r}$	reflected resistance
D_z	z component of flux density	R(r)	a function of radius
E	electric field intensity x component of electric field	$R_{\rm s}$	series resistance
E_{x}		$R_{\rm T}$	thermistor resistance
E_{y}	y component of electric field z component of electric field	R_{Th}	
$\frac{E_z}{F}$	force	$R_{\mathbf{v}}^{\mathrm{In}}$	resistance of inverting source
	force at $x = l$	R	magnetic reluctance
F_l	force at $x = 0$	\mathscr{R}_{g}	air-gap reluctance
F_{0}	peak sinusoidal force	$\mathcal{R}_{\mathbf{m}}^{\mathbf{g}}$	magnetic-path reluctance
$F_{\mathbf{p}}$ $F(\omega)$		ℛ _U	reluctance of U-shaped path
1·(w)	i oution transform	0	

S	strain	γ	conductivity
T	temperature	δ	deflection
$T_{\mathbf{o}}$	reference temperature	ϵ	2.718 · · ·
U	volume	$\epsilon_{_{0}}$	permittivity of vacuum
V	voltage	5	elastic constant
$V_{\mathbf{a}}$	amplifier output voltage	η	small displacement
$V_{\mathbf{C}}$	capacitor voltage	$\boldsymbol{\theta}$	an angle
$V_{\mathbf{G}}$	gyrator voltage	θ_{BW}	angular length bandwidth
$V_{\rm inn}$	voltage of noninverting source	θ_{o}	angular length at resonance
V_{inv}	voltage of inverting source	λ	viscosity
$V_{\mathbf{n}}$	voltage at noninverting terminal	μ	magnetic permeability
$V_{\mathbf{N}}$	rms noise voltage	μ_{i}	incremental permeability
$V_{\mathbf{Nf}}$	feedback resistor noise voltage	μ_{ir}	incremental relative permeability
V_{Nk}	noise voltage of active device	$\mu_{\mathbf{m}}$	permeability of magnet
V_{Nn}	noninverting-source noise voltage	μ_0	permeability of vacuum
V_{Nv}	inverting-source noise voltage	$\mu_{\mathbf{f}}$	relative permeability
V_{p}	voltage of primary	ν	inverse of permeability
$V_{\mathbf{R}}$	received voltage	ν_i	inverse of incremental permeability
V_{s}	voltage of secondary	ξ	susceptibility constant
$V_{\mathbf{T}}$	transmitted voltage	π	3.141 · · ·
V_{Th}	Thevenin source voltage	π_{ijkl}	piezoresistive constant
$V_{\mathbf{v}}$	voltage at inverting terminal	ρ	resistivity
V_{ν}	normalized voltage	$\rho_{\rm D}$	mass density
W	work, energy	ρ_{0}^{-}	resistivity at reference temperature
X	reactance	ρ_a	charge density
X_L	inductive reactance	σ	Poisson's ratio
X_{Lp}	inductive reactance of primary	τ	time constant
X_{LS}	inductive reactance of secondary	$\tau_{\mathbf{f}}$	$2\pi\tau$
$X_{\rm m}$	mutual inductive reactance	φ	an angle, magnetic flux
X_{s}	reactance of secondary	$\phi_{ m c}$	flux of core section
$Y_{\mathbf{m}}$	mechanical admittance	$\phi_{\mathbf{d}}$	downstream phase shift
Y_0	Young's modulus of elasticity	$\phi_{\mathbf{u}}$	upstream phase shift
$Y_{\mathbf{p}}$	maximum tensile stress	ψ^-	electric flux
Z.	impedance	ω	radian frequency
$Z_{\mathbf{f}}$	feedback impedance	ω_a	parallel resonant radian frequency
$Z_{\mathbf{k}}$	coil impedance	ω_{o}^{-}	resonant radian frequency
$Z_{\mathbf{L}}$	load impedance	ω_r	series resonant radian frequency
Z_{o}^{-}	characteristic impedance	$\omega_{\mathbf{x}}$	horizontal component of spatial
Z_{Th}	Thevenin source impedance	~	radian frequency
$Z_{\mathbf{v}}$	impedance of inverting source	ω_y	vertical component of spatial radian
α	a constant, attenuation constant		frequency normalized radian frequency
$\alpha_{\mathbf{E}}$	temperature coefficient of expansion	$\omega_{m{ u}}$	reflection coefficient
α_{FS}	temperature coefficient of expansion	Δ	a small change
~F.5	of structure	Λ	inverse of temperature
α_{EW}	temperature coefficient of expansion	Λ_{0}	inverse of reference temperature
	of wire	Σ	a complicated algebraic sum
$\alpha_{\mathbf{R}}$	temperature coefficient of resistivity	Υ	stress
α_{R_c}	temperature coefficient of	Υ_R	radial stress
·	compensating resistance	Υ_z	length stress
β	a constant	$\Upsilon_{m{ heta}}$	hoop stress

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Some Physiological Specifications

When one considers the design of instruments for physiological measurements it should be stressed that the same basic constraints that apply to other fields, such as instruments for industrial measurements or instruments for ocean-ography, also apply to this field. However, additional considerations such as anatomy, physiological function, and medical safety must also be taken into account in the design of these special instruments.

The particular emphasis of this book is on transducers, particularly electromechanical transducers. Some consideration will also be given to electrothermal devices and to electronic and systems concepts. The transducers being considered are all electrical output devices. Such devices can operate most readily with a variety of metering output instruments, recording equipment, and computers. Matching of transducers to output systems requires extensive consideration of sensitivity, signal to noise concepts, and signal conditioning circuitry. As mathematical techniques are applied more extensively in physiology and medicine, it is necessary that accurate data be supplied for these analyses. This requires that the basic measurements be accurate, and therefore that the measuring instruments be accurate. Crude instrument design has no place in the medical field.

A problem particular to medical instrument design is the anatomy of the system being measured. The geometry of many organs is complex and a choice must therefore be made between designing a transducer compatible with the geometry or attempting to make the measurement from outside the body. The measurement of heart sounds is a good example of this choice. One can carry out sound measurements from the chest wall and attempt to distinguish between

the original signal and the distortions produced by transmission through the chest cavity. Alternatively, one can design a microphone small enough to fit through the blood vessels and heart valves so that measurements can be made inside the heart chambers. The anatomy of the blood vessels places difficult constraints upon this approach.

The physiological function also determines many of the design criteria. Considering again the problem of measuring heart sounds, one finds that the sound levels inside the heart have a magnitude of approximately 60 dB referred to 1 dyne/cm². The chest surface sound level is approximately 40 dB referred to 1 dyne/cm². The frequency range of the sounds is about 5-2000 Hz. In either case the design must be of a device of sufficient sensitivity to have a reasonable output voltage and of appropriate frequency response.

Of special import in the medical field are the questions of safety and reliability. The intracardiac microphone mentioned must be compatible with the blood chemistry. Its mechanical configuration must be such that it does not damage the blood vessels or heart valves during insertion. It in turn must be rugged enough so that it is not damaged either during insertion or during measurement. Any voltage-carrying leads must be adequately insulated from the body. In addition, care must be taken in design so that even under damage conditions, unsafe voltages are not presented to the body. In fact, for any instrument with electrical measurement characteristics care must be taken to eliminate the possibility of unsafe voltages being applied to the body.

Thus far the discussion has been of transducers in general, without any specific types detailed. This book includes the following transducers that are in common use in instruments:

- 1. variable resistance,
- 2. piezoelectric,
- 3. electrodynamic,
- 4. variable inductance,
- 5. differential transformer,
- 6. magnetostrictive,
- 7. variable capacitance.

In the area of electrothermal tranducers, variable resistance devices are discussed in detail. In particular, the design of thermistor instruments is considered. While most of the design discussion is restricted to simple transducers, the design of force balance instruments is also covered in detail. Such instruments, with only a slight increase in complexity, yield greatly increased accuracy and environmental insensitivity.

The point of view being taken here is quite a bit different from some other approaches to medical instrumentation. The emphasis is on the transduction technique rather than on the measurement being made, such as pressure. It is

believed that there is much more similarity between different measurement instruments (for example, pressure gage and accelerometer) using the same transduction technique than between instruments making the same measurement with different transduction techniques (for example, strain gage versus differential transformer pressure instruments). Certain analytical methods (analogies, transfer function techniques) are common to all electromechanical transducers and can be discussed as a unified topic. Similarly, pressure-coupling characteristics are a common problem and will be discussed without regard to specific transducers.

Since the ultimate aim of this textbook on medical instrumentation is to teach instrument design, many examples of such designs are discussed in detail. These include:

- 1. respiratory-flow transducer,
- 2. catheter tip blood pressure gage,
- 3. electronic thermometer.
- 4. intracardiac catheter microphone,
- 5. piezoelectric ventricular-assist device.
- 6. ultrasonic blood flowmeter,
- 7. electrodynamic ventricular-assist driving system.
- 8. electrodynamic blood flowmeter.
- 9. variable-capacitance microphone,
- 10. force balance blood pressure gage,
- 11. biotelemetry units.

Before considering details of analysis, transducer design, and instrument design it is important to consider the nature of some of the measurements that one would like to make on biological systems. Figure 1-1 schematically represents typical physiological measurements made on man and displays some of the waveforms that can be recorded. In addition to direct electrical measurements such as the electrocardiogram, electroencephalogram, and electromyogram, which can be recorded by use of appropriate electrodes and signal conditioning amplifiers, there are a number of measurements that require the use of medical instrument transducers. These include blood flow, blood pressure, temperature, breathing flow and rate, and heart sounds. The characteristics of these measurements determine the requirements for the applicable transducers, as considered in the sections that follow.

1-1 Blood Flow

In this instance one would like to measure flow in an elastic vessel with a variety of nonuniform characteristics. Because the flow is pulsatile, it is desirable to measure frequencies from 0 to 100 Hz. The flow amplitude depends upon the

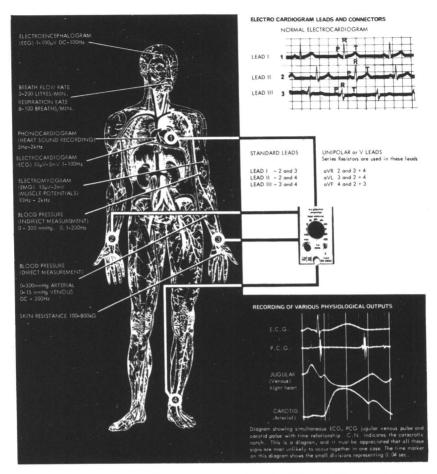


Fig. 1-1 Typical physiological measurements and ranges. (Reprinted by permission from SE Labs (EMI) Ltd.)

vessel being studied, but the maximum instantaneous velocity is less than 1 m/sec. Ideally, one would like to make this measurement without inserting anything into the body, and some ultrasonic instruments attempt this. More commonly, the measurement is made from outside the blood vessel with the objective of not interfering with the normal flow while making the measurement. Vessel sizes are small, ranging from a maximum diameter of a few centimeters down to a fraction of a millimeter.

If the transducer is inserted into the body it must be compatible with the body chemistry. An implantable device is advantageous.

1-2 Blood Pressure

It is desirable in this case, too, to make the measurement from outside the body — and to some degree this is commonly done. By the indirect occluding-cuff technique the maximum and minimum values (systolic and diastolic) of the pressure waveform are measured externally. Often, however, a complete pulsatile waveform is needed. This measurement requires a frequency response of the instrument of approximately 0–300 Hz. If this measurement is made at various locations inside the heart or in the blood vessels, the instrument must not interfere with the normal function. The pressure amplitude ranges from 0 to 15 mm Hg in the veinous system and from 0 to a maximum of 300 mm Hg in the arterial system. If an external technique of measurement is used, it must be suitable for monitoring over an extended period of time.

1-3 Body Temperature

For diagnosis it is desirable to measure temperature inside the body, and when this is required it is customary to make an oral or rectal measurement. Other locations for core temperature have been investigated but none has widespread acceptance. In evaluating vascular difficulties it is sometimes desirable to measure temperature at the ends of the fingers and toes. Temperature sensors should be small so that their response time is short and the measurement is automatically localized. Normally, great accuracy is required $(0.1-0.2^{\circ}F)$. The required range for monitoring core temperatures is about $95-110^{\circ}F$ ($35-44^{\circ}C$) and for peripheral temperatures about $80-100^{\circ}F$ ($26-38^{\circ}C$). As a control device during hypothermia, an instrument with a measurement range from 60 to $110^{\circ}F$ ($15-44^{\circ}C$) is needed.

1-4 Breathing Flow and Rate

In order to make accurate flow measurements of respired air, the transducer must surround the total inspired or expired breath. The breath is generally moist so that the transducer must be operable in a high humidity environment. The number of breaths per minute can range from about 8 to perhaps 100. The flow rate has an even wider dynamic range — from 3 to 200 liters/min. The former is characteristic of very shallow breathing, while the latter occurs during coughs. Since respiration is very sensitive to oral pressure, the breathing instrument must produce very low back pressure during normal flow. Thus it must carry out its function with a very low flow impedance. It must have a frequency response of about 0-20 Hz to reproduce the flow waveforms adequately.

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1-5 Heart Sounds

As implied in the course of this introductory chapter, appropriate measurements of heart sounds require a microphone that generates 1 mV, with a frequency response from 5 to 2000 Hz. This calls for a sensitivity of at least -120 dB referred to 1 V/dyne/cm² for internal heart sound measurement (or -100 dB referred to 1 V/dyne/cm² for external measurements). The mechanical design must be appropriate to the anatomy. It should always be kept in mind when designing an external cardiac microphone with electronic displays that there exists a very simple instrument – the stethoscope – with a long history of satisfactory performance.