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# Thermal Stress on Composite Materials

Process, Design, Experiments



**LAMBERT**  
Academic Publishing

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**Nagwa E. Elzayady  
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### **Dedication**

**To whole people who have encouraged me and granted me aids and supports over the years of study and search, especially my advisors. Also to my whole family, particularly, my late father, and my great mother. Included also are my husband, Emad, and my sons Kazem and Gawad.**

**Nagwa E. Elzayady**

## LIST OF SYMBOLES AND ABBREVIATIONS

### Symbol

$Q$ ( $\text{W/m}^2$ )	Heat flux
$\Delta T$ ( $^{\circ}\text{C}$ )	Temperature difference
$R$	Thermal resistance of material
$k$ ( $\text{W.m}^{-1}\text{.}^{\circ}\text{C}^{-1}$ )	Thermal conductivity of solids
$h$ ( $\text{W/ (m}^2\text{.}^{\circ}\text{C)}$ )	Heat transfer coefficient of medium
$g$ ( $\text{W/m}^3$ )	Energy generation rate per unit volume
$\text{CTE}$ ( $^{\circ}\text{C}^{-1}$ )	Coefficient of thermal expansion
$\delta \ell$	Deformation through insulation layer
$C_p$ ( $\text{J/kg.}^{\circ}\text{C}$ )	Specific heat
$\rho$ ( $\text{g/cm}^3$ )	Density
$t$ (Sec)	Time
$A$	Surface area
$V$	Volume ( $\text{cm}^3$ )
$\alpha = k/\rho C_p$	Thermal diffusivity
$Bi$	Biot number
$L_s = V/A$	Characteristic length
$Q$	Rate of heat flow into the solid during heating process
$dT$ (t)	Temperature changing of solid with time during heating or cooling process
$d$ (t)	Change in time during the thermal cycle
$T$ (t)	Solid temperature at certain time
$T_{\infty}$ ( $^{\circ}\text{C}$ )	Fluid temperature during a thermal cycle.
$\dot{m}$ ( $\text{kg/min}$ )	Rate of water currency
$\dot{V}$ ( $\text{cm}^3/\text{min}$ )	Volume of water per time
$\dot{v}$ ( $\text{m/min}$ )	Velocity of water
$\sigma_c$ (MPa)	Thermal shock resistance of materials
$E$ (GPa)	Young's Modulus
$\nu$	Poisson's ratio
$G = \frac{E}{2(1+\nu)}$ (GPa)	Shear modulus
$K = E/3(1-2\nu)$ (MPa)	Bulk modulus

$$\alpha_c = \frac{\alpha_m(1-\phi)K_m + \alpha_r\phi K_r}{(1-\phi)K_m + \phi K_r}$$

ROM

$$\mathbb{Y}_c = \mathbb{Y}_r \phi + \mathbb{Y}_m (1-\phi)$$

$\mathbb{Y}$

$\phi$

$c$

$r$

$M$

Turner's model for estimation the metal  
matrix composite properties

Role of mixture for estimation the metal  
matrix composite properties

Role of mixture equation

Express a property of material

Weight fraction (%) of the reinforcement in  
the composite

Subscript denotation for the composite  
material

Subscript denotation for the reinforcement

Subscript denotation for the matrix



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# CHAPTER 1

## INTRODUCTION

### 1.1 Historical Background

Metal-matrix composites (MMCs) have been attracting growing interest. MMCs' attributes include alterations in mechanical behavior; tensile, compressive, creep, notch resistance, and tribological properties by the filler phase. Also physical properties; intermediate density, thermal expansion, and thermal diffusivity can be altered [1]. Engineering interests in aluminum-based metal matrix composites (MMCs) has increased [2]. Among Aluminum alloys, Aluminum-Silicon (Al-Si) alloys are most versatile materials, comprising 85% to 90% of the total aluminum cast parts produced for the automotive industry, depending on the Si concentration in weight percent (wt.%) in the Al-Si alloy systems [3]. Aluminum-silicon alloys supply a good combination of mechanical properties and castability and for those reasons, they are widely used in the automotive and aerospace industry. [4] Silicon increases the fluidity in aluminum casting alloys and reduces the solidification interval and hot tears tendencies [4, 5].

Al-Si alloys such as A356 (Al-7Si- 0.3Mg) and A390 (Al-17.0Si-4.5Cu-0.6Mg) have been commercially used to produce an engine block due to their high strength over weight ratio [6].

Compared to conventional Al alloys, the Al alloy matrix based composites, reinforced with ceramic particles have the best density-properties-price combination. Therefore, it is legitimate to expect that these materials will substitute for part of conventional materials in mass production, for example in automotive, as well as in other industries of transport vehicles

[7]. Aluminum-matrix composites are not a single material but a family of materials whose stiffness, strength, density, thermal and electrical properties can be tailored. The matrix alloy, reinforcement material, volume and shape of the reinforcement, location of the reinforcement and fabrication method can all be varied to achieve required properties [8].

Particulate reinforced MMC's have recently found special interest because of their high specific strength and specific stiffness at room or elevated temperatures. Interest in particulate reinforced aluminum MMCs is mainly due to easy availability of particles and economic processing technique adopted for producing them [9]. The particulate reinforcements have been classified as the by-products from other technologies (e.g., SiC, SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, aluminosilicates, graphite, and fly-ash) and are readily available or are naturally renewable at affordable cost (e.g., coconut shell char, mica, palm-kernel shell char, and zircon). Further, the potential nature of these filler materials is attractive. For example, SiC has good thermal and chemical stability, both during synthesis and under severe service conditions, strength, cost (about \$13/kg for the particulate), and availability [1]. Also, Albite is common feldspar ceramic, a mineral aluminosilicate (NaAlSi<sub>3</sub>O<sub>8</sub>) that occurs most widely in acid igneous rocks such as granites [9 & 10]. It's basically consisting of silicates; it is abundantly available in the earth's crust. Albite ranges from white to dark grey in colour and is extremely wear resistant, having a Moh hardness of about 6.5, almost rivaling that of SiC but exceeding that of alumina. It has a low coefficient of thermal expansion of  $2.3 \times 10^{-6} \text{ }^{\circ}\text{C}^{-1}$  [9, 11]. Also low thermal conductivity ( $2.8 \text{ W.m}^{-1}.\text{C}^{-1}$ ) of Albite and density ( $2.6 \text{ g/cm}^3$ ) which is much lower than those of SiC ( $3.1 \text{ g/cm}^3$ ) and alumina ( $4.0 \text{ g/cm}^3$ ) [9, 11, 12]. These properties make Albite a candidate reinforcement material in MMCs. Among metal-ceramic combinations, the Al-SiC couple has been one of the most widely studied systems over the last years [8].



Continuously and discontinuously reinforced Al/SiC metal matrix composites (MMCs) are promising modern, light weight materials with excellent properties, such as: high hardness and strength at ambient and elevated temperatures, good wear resistance, and high modulus of elasticity.

Currently, the use of MMCs is limited predominantly to the military and the aerospace industry. However, the penetration of these materials has already begun also in civilian applications [7]. With increased SiC addition, the module of elasticity increases linearly and thermal expansion decreases. Unfortunately, with increased content of reinforcement the ductility of the composite is drastically decreased. Tensile and compression ductility of Al/SiC MMCs are very different. These composites have high compression strength, but they are very sensitive to tensile load. Therefore, these materials are appropriate for hot forming in closed dies (die forging, hot pressing, extrusion etc.) [7]. (Al-SiC) MMC has been studied by large number of searchers whom save plenty of concerning data. While, there is a leakage of information about (Al-Albite) MMC.

A great portion of the research efforts is focused on producing the MMCs by solidification processing, which is likely to be more economical and relatively simple in comparison with the competing solid processing [2].

Vortex method and forming in semi-solid state (SSM) has been proved as an advantageous route for producing Al alloys as well as their composites. Several advantages of semi-solid forming process are proved, the most important of these, in the view of most technologists today, is the non-turbulent filling of the die, which results from the high and controllable viscosity of the semi-solid material. This smooth mold filling eliminates the air entrapment encountered in the conventional die-casting process and