Multiphase Science and Technology

Volume 1

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MULTIPHASE SCIENCE AND TECHNOLOGY

Volume 1

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Contents

Preface xiii

Chapte	er 1	Spray Cooling of Hot Surfaces L. Bolle and J. C. Moureau 1
1	Intro	duction 1
	1.1	Main Uses of Liquid Sprays 1
	1.2	Previous Experimental Studies of Spray Cooling 4
		1.2.1 Laboratory Measurements 4
		1.2.2 Industrial Measurements 13
2	Main	Characteristics of a Liquid Spray 16
	2.1	Various Kinds of Atomizers 16
	2.2	Macroscopic Characteristics of a Spray 22
		2.2.1 Total Flow Rate and Related Parameters 22
		2.2.2 Liquid Flow Rate Density (m
		2.2.3 Dynamic Pressure of the Spray 25
	2.3	Microscopic Characteristics of a Spray 29
		2.3.1 Droplet Diameter Distribution 29 2.3.2 Droplet Velocity Distribution 36
		2.3.3 Mean Velocity of Drops in a Spray 40
3	Hydr	rodynamic Behavior of Droplets Impinging on a Hot Plate 42
0	3.1	The Single Drop 42
	3.1	3.1.1 Drop with We > 80 43
		3.1.2 Drop with We < 80 47
	3.2	The Liquid Spray 47
4	Heat	Transfer during the Impact of a Drop 52
	4.1	Existing Theoretical Models 52
		4.1.1 The Sessile Drop 52
		4.1.2 The Impinging Drop 57
	4.2	A New Theoretical Model 67
		4.2.1 Heat Transfer by Direct Contact 67
		4.2.2 Heat Transfer through the Vapor Film 70
-		4.2.3 Heat Transfer Due to a Single Drop 71
5		Transfer between a Hot Plate and a Spray: Theoretical Model and
		eriments 72
	5.1	
	5.2	
		5.2.1 Experimental Device 73 5.2.2 Wall Heat Flux Calculations 74
		5.2.3 Heat Transfer Results 76
		5.2.4 Comparison with Other Experimental Results 81
		5.2.5 Efficiency of Spray Cooling 83
	5.3	Comparison between Theoretical Model and Experiments 86
6	Conc	clusions 90
Nor	mencla	ature 91
Pof	orono	02

		The Spherical Droplet in Gaseous Carrier Streams: Review and Sy	nthesis
Ge	orge G	Syarmathy 99	ZPZ T
1	1.1 1.2	Poduction 99 Purpose and Scope 99 Historical Outline 103	14.50
2	State 2.1 2.2 2.3	Definition of Sample, Basic Assumptions 105 Balance Equations 110 Nondimensional Parameters 115 2.3.1 Basic Physical Variables 115 2.3.2 Nondimensional Variables 117 2.3.3 Basic Set of Nondimensional Parameters 118 2.3.4 Discussion of the Nondimensional Parameters and Their Numerical Values 125 2.3.5 Relationships Concerning the Expansion Rate 129	
		2.3.6 Other Nondimensional Groups 130 2.3.7 Review and Comparison with Literature 132	
3		sfer of Heat, Mass, and Momentum to a Sphere 135	
	3.1	Continuum Environment 138 3.2.1 General 138 3.2.2 Nusselt Number Expressions for Quiescent Media 139 3.2.3 Nusselt Number Expressions for Relative Flow 139 3.2.4 Other Effects 140	
	3.3	3.2.5 Review of the Crucial Parameters Free-Molecule Environment 144 3.3.1 General 144 3.3.2 Accomodation Coefficients 145 3.3.3 Transfer Rates 147 3.3.4 Nusselt Number Expressions 149 3.3.5 Review of the Crucial Parameters 152	
	3.4	Multirange Expressions 153 3.4.1 General 153 3.4.2 The Cunningham Correction 154 3.4.3 Multirange Expressions for the Nusselt Numbers 156 3.4.4 The Stationary, Isothermal Sphere 157 3.4.5 Relative Flow and Other Corrections 158 3.4.6 Comparison with Experimental Data 158 3.4.7 Review of the Crucial Parameters 160	
	3.5	Applicability to Droplet Growth; Proximity Effects 3.5.1 Constancy of r (Assumption IVa) 160 3.5.2 Constancy of T_r and T_r (Assumption IVb) 162 3.5.3 Constancy of Far Field Conditions (Assumption IVc) 162 3.5.4 Infinite Environment (Assumption IVd) 163 3.5.5 Body-Force Effects (Assumption IVe) 166	
	3.6	Heat Conduction in the Interior of the Droplets 166	
4	3.7 Fauil	Drift Velocity 169 librium and Stability of Droplets 171	
4	4.1 4.2	Thermodynamic Equilibrium 171 Mechanical Stability 174	

A2.4	Energy Balance 263
A2.5	Comments on Temperature Definitions 266
Append	lix 3 Free Molecule Transfer Processes in Mixture Carriers 267
A3.1	Mass Impingement Rate of Molecules 267
A3.2	Heat Transfer 267
A3.3	Mass Transfer 269
A3.4	Momentum Transfer (Drag) 271
Append	dix 4 The Analysis of Droplet Surface Temperature 272
A4.1	
A4.2	HE I ST - THE STATE OF THE STA
A4.3	
A4.4	
A4.5	
A4.6	
A4.7	
A4.8	
	lix 5 Biographic Notes Concerning the Non-Dimensional
	ed Groups Proposed 279
144111	00 0100p3110p0300
hapter 3	Boiling in Multicomponent Fluids R. A. W. Shock 281
1 Int	roduction 281
2 Ph	ase Equilibrium 283
3 Or	set of Boiling 286
3.1	Homogeneous Nucleation 286
3.2	Heterogeneous Nucleation 287
4 Bu	bble Growth Dynamics 295
4.1	Introduction 295
4.2	Free Bubbles 297
4.3	Attached Bubbles 308
5 Nu	cleate Boiling Heat Transfer 318
5.1	Introduction 318
5.2	
	5.2.1 General Form of Correlations 327
	5.2.2 Empirical Correlations 335
6 0-	5.2.3 Semiempirical Correlations 338 tical Heat Flux 341
6.1	1982년 1월 1일 전 10 12 12 12 12 12 12 12 12 12 12 12 12 12
	Thin Wires 342
6.3	
	m Boiling 350
	ow Boiling and Evaporation 361
	nclusions 368
Nomen	
Referen	
Annen	liv 383

5	Grow	th and Vaporization 175
	5.1	Simplification of the Basic Equations 5.1.1 Outline of Approach 5.1.2 General Nonsteady Case 77 5.1.3 Partially Quasi-Steady Formulation 77 5.1.4 Quasi-Steady Formulation 77
	E 0	
	5.2	The Surface Temperature of the Drop 180 5.2.1 Thermodynamic Parameters of the Droplet 180
		5.2.2 Parameter Domains of Practical Interest 182
		5.2.3 Discussion of the Equation Giving T_r 183
		5.2.4 Iterative Calculation of T_r 185
		5.2.5 The Caloric Effectiveness Q 187
		5.2.6 Approximate Expressions for Q 187
		5.2.7 Conclusions and Critical Remarks 191
	5.3	Laws of Quasi-steady Droplet Growth 192 5.3.1 General Formulation 192
		5.3.2 Simplified Growth Laws for Pure Vapor or Vapor-Rich Carriers 195
		5.3.3 Simplified Growth Laws for Lean, Cold Carriers 197
		5.3.4 Simplified Growth Laws for Lean, Hot Carriers 199
	5.4	Outline of Calculation Procedure 200
6	Appl	ication 109
	6.1	Time Constants 109
	6.2	Spray Droplet Vaporization 209
	6.3	The Influence of Droplet Size on Droplet Temperature 215
	6.4	Analytic Solutions for Growth in Carriers of Constant Conditions 21
	6.5	Entropy Production in Mist-Type Flows 223
		6.5.1 Polytropic Loss Coefficients 223
		6.5.2 Thermodynamic Disequilibrium 225
		6.5.3 Mechanical Disequilibrium 228 6.5.4 Similarity Law of Entropy Production 230
7	Critic	cal Discussion and Conclusions 231
,	7.1	Classification of Droplet Growth Theories 231
	7.1	7.1.1 Fully Nonsteady Treatment 231
		7.1.2 Partially Quasi-Steady Treatment 232
		7.1.3 Quasi-Steady Formulation Using a Differential Equation for T_r 232
		7.1.4 Quasi-Steady Theories Using an Algebraic Equation for T_r 233
	7.2	Conclusions 235
	7.3	Suggestions for Further Work 237
No	mencla	ature 238
	ference	
		1 Summary of Some Elementary Relationships and of Representative
1	Materia	als Data 253
1	41.1	
	11.2	Carrier-Phase Mixture Properties 254
	41.3	Vapor Pressure, Saturation Ratio, and Subcooling 255
1	41.4	Representative Materials Data 256
Ap	pendix	2 Balance Equations for the Two-Phase Fluid Sample 259
	42.1	Definitions 259
	42.2	Mass Balance 261
1	12.3	Momentum Balance 261

napt	er 4	Contact Angles Jacques Chappuis 307
1	Intro	duction 387
	1.1	Behavior of Liquids Relative to Solid Surfaces 387
	1.2	Applications of Contact Angles 388
	1.3	Theoretical Complexity and Present Standards of Understanding 389
	1.4	Purpose and Scheme of the Chapter 390
2		d Surfaces 392
-	2.1	Surface and Interfacial Tensions of Liquids, and Other Surface
		Thermodynamic Quantities 392
	2.2	Surface Tension Related to the Molecular Structure of Liquids 395
	2.3	Interfacial Tension Between Two Nonmiscible Liquids 400
	2.4	Adsorption at Liquid Surfaces 401
	2.5	Laplace's Law; The Condition of Mechanical Equilibrium
		of a Surface 403
	2.6	Cylindrical Meniscii in the Gravitational Field 404
		2.6.1 Cartesian Equation of the Curve $z = f(x)$ 406
		2.6.2 Parametric Equation of the Curve 407
		2.6.3 Volume of the Meniscus 4092.6.4 Elementary Work of Formation of a Cylindrical Meniscus 410
		2.6.5 Total Work of Cylindrical Meniscus Formation 412
	2.7	Axially Symmetrical Meniscii in the Gravitational Field 412
		2.7.1 The Volume of an Axially Symmetrical Meniscus 414
	2.8	Influence of a Liquid's Curvature on Its Vapor Tension 415
3	Solid	Surfaces 415
	3.1	Surface and Volume Stresses 415
	3.2	Superficial Tension of Solids 417
	3.3	Measurement of Surface Tension of Solids 418
	3.4	Heterogeneity of Solid Surfaces 418
	3.5	Roughness of Solid Surfaces 419
4	Adso	orption on Solid Surfaces 420
	4.1	General Characteristics of Adsorption 420
		4.1.1 Definition of Adsorption 420
		4.1.2 Specific Surface Area of Solids4214.1.3 Demonstration of Adsorption Phenomena at the Solid-Gas Interface421
		4.1.4 Demonstration of Adsorption Phenomena at the Solid-Liquid Interface 42
		4.1.5 The Adsorption Mechanism 421
		4.1.6 Physical Adsorption or Physisorption 422
	1.0	4.1.7 Chemical Adsorption of Chemisorption 423
	4.2	Adsorption of Gases on Solids 423
	4.3	Adsorption from Solutions 425
_	4.4	Modification of the Surface Tension of Solids by Adsorption 426
5		tact Angles on Smooth and Homogeneous Solid Surfaces 427
	5.1	Young's Model 427 5.1.1 Thermodynamic Justification of Young's Equation 428
		5.1.2 Quantities That May Come into Play in Young's Equation 428
	5.2	Vectorial Justification of Young's Equation 429
		5.2.1 Validity of Young's Vectorial Equation in the Absence of Gravity 432

6

5.3	Experimental Evidence of Young's Vectorial Model 432
5.4	Contact Angle of a Drop of Liquid on a Clean, Solid Surface,
	in a Vessel Containing No Other Gas Than the Liquid's Vapor 433
5.5	Adhesion Tension; Work of Wetting 434
5.6	Work of Adhesion; Work of Cohesion 437
5.7	Physical Significance of $W_A \circ$ and W_A 439
5.8	Spreading Coefficient S 441
5.9	Reversible and Irreversible Processes in the Case of a Moving
	Three-Phase Line 441 5.9.1 An Irreversible Process 441
	5.9.2 A Reversible Process 442
Hvs	teresis of Contact Angles on Real Solid Surfaces 443
6.1	Advancing and Receding Contact Angles 443
6.2	Surface Heterogeneity and Hysteresis 445
0.2	6.2.1 Model 1: A Horizontally-Striped Plate 445
	6.2.2 Model 2: A Vertically-striped Plate 449
	6.2.3 Model 3: A Surface of High Superficial Tension Interspersed with Small Patch
	of Low Tension 450
6.3	6.2.4 Application to Real Heterogeneous Surfaces 454 Surface Roughness and Hysteresis 454
0.5	6.3.1 Model 1: A Plate Presenting Inclined Horizontal Stripes 454
	6.3.2 Model 2: A Plate Presenting Inclined Vertical Stripes 456
	6.3.3 Application to Real Surfaces 457
6.4	Other Causes of Variation in Contact Angles: The Modifications
	of a Solid Surface after its Contact with a Liquid 458
6.5	Other Important Theories about Contact Angle Hysteresis 459
6.6	Conclusion and an Example of the Use of Results Obtained 460
	6.6.1 Experimental Details 460
	6.6.2 Experimental Results 460 6.6.3 Interpretation 461
The	Wetting Tensiometer: Analysis of a Method of Measuring
	tact Angles 462
7.1	Choice and Description of the Measuring Method 462
	7.1.1 Choice of Method 462
	7.1.2 Description of Method 463
7.2	Theoretical Analysis 464
	7.2.1 Notation and Conventions 464
	7.2.2 Nature of the Measured Forces 465 7.2.3 Height of the Meniscii 467
	7.2.4 Case of Horizontal Edges 467
7.3	Physical Significance of the Recordings 468
	7.3.1 Experimental Curves 468
	7.3.2 Theoretical Curves 471
	7.3.3 Theoretical Construction of a Curve 473
7.4	Practical Use 474
	7.4.1 Choice of Samples 474
	7.4.2 Choice and Influence of Liquid 4757.4.3 Determination of Macroscopic Heterogeneity of Surface "Pollution" 475
	7.4.4 Utilization of the Technique as a Test of Cleaning 477

8	Inter	pretation of Contact Angle Values 4//
	8.1	Existence of an Equation of State 477
	8.2	The Importance of π_e in Different Cases 478
	8.3	The Choice of Proper Experimental Results 479
	8.4	Analysis of Results 480
	8.5	Critical Analysis of Zisman's Interpretation 484
	8.6	Other Important Theories in the Literature 485
	8.7	The Author's New Interpretation 486
	8.8	Conclusions to Be Drawn from Our Interpretation 490
		8.8.1 The Expression of W_A o 490
		8.8.2 The Expression of γ_{SL} 490
		8.8.3 The Significance of γ_0 and γ_C 490
		8.8.4 The Measurement of π_e 491
	8.9	Recapitulation of Conclusions Drawn from PTFE Data 491
	8.10	Extension of the Theory to Other Solids 491
9	None	equilibrium Contact Angles 494
No	mencla	ature 495
Re	ference	es 500

Subject Index 507

Preface

This is the first volume of *Multiphase Science and Technology*, a new international series of books intended to fill an existing gap and bring together materials from different fields such as nuclear energy, chemical processing, petroleum, meteorology, civil engineering, and energetics. The objectives of the series are to provide authoritative overviews of important areas in multiphase systems. The chapters published in the series are systematic and tutorial presentations of the state of knowledge in various areas. The editors hope that the nonspecialist reader can gain an up-to-date idea of the present stage of development in a given area.

Chapter 1 deals with the spray cooling of hot surfaces and is coauthored by Professor Léon Bolle and Doctor Jean-Claude Moureau. Professor L. Bolle has been with the Catholic University of Louvain, Belgium, since 1972 and is currently working on industrial energetics. A former student of Professor L. Bolle, Doctor J. C. Moureau received his doctorate in applied sciences in 1978 and is now in charge of nuclear safety at the Belgian Ministry of Health and Welfare.

The behavior of a droplet in a carrier stream is then examined in Chapter 2, by Doctor George Gyarmathy, Manager of the Turbomachinery R & D laboratories in the Brown Boveri Company, Baden, Switzerland. Doctor G. Gyarmathy has been involved in the theory of wet steam turbine and condensation for the past twenty years and is a recognized expert in these areas.

Chapter 3 is devoted to boiling phenomena in multicomponent fluids. Doctor R. A. W. Shock, the author, works for Heat Transfer and Fluid Flow Service at Harwell, UK. He is a specialist in the design of vertical thermosiphon reboilers and in crystallization.

Wall nucleation depends upon contact angles and wettability phenomena, the subject reviewed by Doctor Jacques Chappuis, Ecole Centrale de Lyon, France, in Chapter 4. Doctor J. Chappuis is currently on a sabbatical year at the Department of Mechanical Engineering of the University of Toronto.

These four chapters constitute the first volume of *Multiphase Science and Technology*. We would like to thank all the authors and reviewers for their outstanding contributions. And we would like also to express our special indebtedness to Mrs. Pauline Wilkes, who did a careful and patient job in typing this book.

The Editors

Spray Cooling of Hot Surfaces

L. Bolle and J. C. Moureau Universite Catholique de Louvain, Belgium

1 INTRODUCTION

1.1 Main Uses of Liquid Sprays

A dispersion of small liquid drops in a continuous gaseous phase is generally called a liquid spray. This dispersion has also received various other names according to the dimensions of the droplets produced. Some authors, such as Fortier (1967), distinguish between mist and cloud. A mist is a dispersion including drops smaller than $10^{-1}~\mu\text{m}$, whereas a cloud refers to a dispersion of larger particles. Others call an aerosol a dispersion of submicrometer particles and a mist much larger drops, for example, drops with a diameter of 150 μm . It is therefore necessary to make clear that, in this chapter, we consider as liquid spray a dispersion of liquid particles with diameters ranging from about *20 μm up to about 1 mm.

A process of disintegration of the liquid phase induces an increase in the interfacial surface area between the liquid and the medium into which it penetrates. This increase can be quite important: in some instances, the initial interfacial surface area can become several hundred times larger. Atomization can thus intensify the physical or chemical processes occurring at the interface, that is, mass, momentum, and energy transfers. This advantage is used in several industrial applications.

Liquid spraying is common in various fields: air conditioning and ventilation, gas absorption, washing and cleaning, fire protection, coating of surfaces, spray drying, combustion, cooling of hot gases, cooling of hot surfaces. This chapter is devoted to the study of this last application.

It is in the steel and metal works industry that one finds the most numerous uses of atomization in order to cool hot walls: cooling of slabs, rolled products, and cylinders in classical mills, and cooling of incandescent metal immediately after its exit from the mould in continuous casting units. In most instances, the amount of heat to be extracted from the metal is large: Fig. 1 shows, for the case of continuous casting, the variation of heat flux density \dot{q}_w in the secondary cooling zone of a rectangular slab.

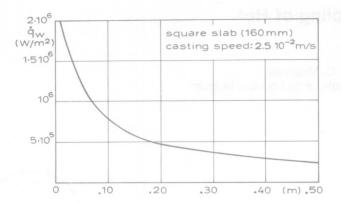


Fig. 1. Variation of the heat flux density as a function of distance to the casting level, according to Weinreich (1969).

Let us consider the typical example of the runout table of a hot strip mill. Between the last finishing stand and the coiling, cooling can be divided into three zones (Fig. 2):

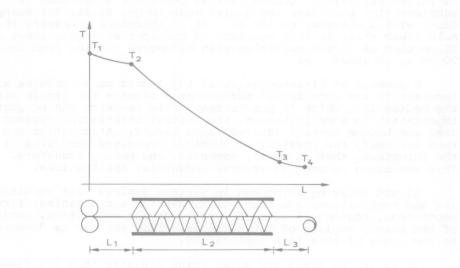


Fig. 2. Cooling zones on the runout table of a hot srip mill.

- 1. From the last mill to the beginning of the water cooling, the metal is in contact with air. Heat transfer is governed mainly by radiation with the environment, since the strip temperature is high (800 to 900° C).
- 2. Spray cooling produces an important drop in temperature along stretch L_2 . The liquid aspersion is performed differently on the upper and lower sides of the strip. Above, water nozzles are generally mounted along successive rows at a distance of about 2 m from the strip: below, since the water must flow between the supporting rolls, the nozzles are placed nearer and usually have a lower flow rate. What kind of nozzles and how many should be displayed in order to achieve the desired cooling? At what pressure should they work? What is the optimal length L_2 ? To all these questions, the answer given has sometimes been too empirical and approximate. Indeed, the fundamental problem determination of the heat transfer coefficient between a hot wall and a water spray has not been completely solved.
- 3. Between the end of the spray cooling and the coiling, the strip is again in contact mainly with air: again, radiative heat transfer is predominant.

From a metallurgical viewpoint, the velocity with which heat is extracted from the metal during water cooling is essential in order to obtain a good-quality product. It has been shown that, for low-alloy steels, high strength can be achieved without reducing ductility or weldability provided that the size of the grains can be reduced. One of the best ways to reach this goal is to control cooling during the austenite-ferrite transformation (Morgan et al., 1965, 1966).

For rolled wire rods, a drastic cooling without quenching is desirable. Furthermore, when spraying, the surface temperature risks being considerably lower than that of the center of the rod. Therefore, in order to avoid superficially quenched structures, one has to divide the spray cooling zone into several parts separated by air cooling zones. Indeed, this setup facilitates uniformization of the inside temperature of the rod. Figure 3 illustrates the method for a wire rod with a 5.5 mm diameter. Moreover, Couvreur (1971) insists on the necessity, in design calculations, of taking into account a variation of the surface heat transfer coefficient α with the temperature of the rod. If, instead, one uses an averaged constant heat transfer coefficient, large discrepancies can appear. In Fig. 3, one sees a difference of about $100\,^{\circ}\text{C}$ in the rod surface temperature when using constant and temperature-varying coefficients. This proves the usefulness of studies aiming to determine the exact parameters influencing heat transfer in such applications.

In nuclear power plants, spray cooling is one of the safety systems foreseen in case of accident. Schematically, two techniques exist: top spraying, that is, liquid spray onto the core from above; and bottom reflooding, that is, immersion from below. In the latter case, drops can sputter from the upper liquid level and impinge on hot walls. Many related publications — both theoretical and experimental — have described the phenomena occurring in various core configurations and possible incidents.

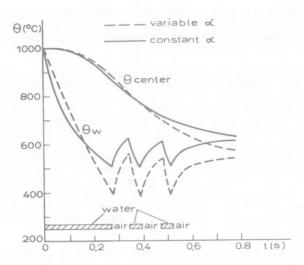


Fig. 3. Time evolution of the wire temperature, according to Couvreur (1971).

Yamanouchi (1968), for instance, has proposed a model for the evaluation of emergency spray cooling for a postulated loss of coolant accident (loca) in a boiling-water reactor. This model has been extended by several authors. Reviews of papers on spray cooling of light-water reactor cores have been published, among others, by Sawan and Carbon (1975). Moore et al. (1973) have studied spray emergency cooling of heavy-water reactors. In many of these texts, the liquid spray is considered only as a means to produce a liquid film flowing over the hot wall. It is the heat transfer between the film and the hot surface that is analyzed in detail and not the transfer due to the impacts of very many individual drops. Therefore, we shall not comment on these studies any further.

Besides the steel-making and nuclear industries, the chemical industry also uses liquid sprays in order to cool hot surfaces, for example, in the cooling of hot vessels and tanks.

Moreover, we think that liquid sprays could also be used in other fields. In 1973, Kawazoe and Kumamaru developed a new technique of spray cooling in order to improve the performance of the extrusion process of plastic-insulated telephone wires. New applications of spray cooling of hot surfaces are to be expected.

1.2 Previous Experimental Studies of Spray Cooling

One can distinguish in the literature two types of experimental work: results obtained in laboratories and measurements performed directly on industrial equipments. Theoretical models will be discussed later.

1.2.1 Laboratory Measurements

The main results published during the last 12 years are