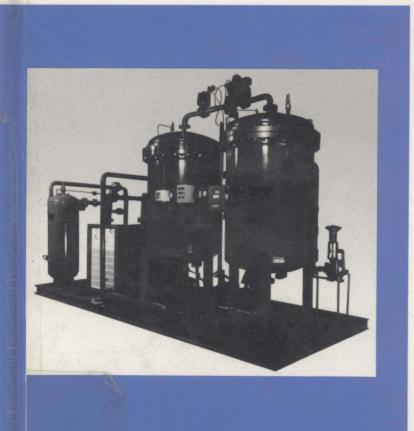
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## Pressure Swing Adsorption





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## Pressure Swing Adsorption

#### **Preface**

Although pressure swing adsorption (PSA) is not a new process, it is really only during the past decade that such processes have achieved widespread commercial acceptance as the technology of choice for more than a few rather specific applications. Nowadays, however, PSA processes are widely used, on a very large scale, for hydrogen recovery and air separation, and further important applications such as recovery of methane from landfill gas and production of carbon dioxide appear to be imminent. The suggestion for a book on this subject came from Attilio Bisio, to whom we are also indebted for his continuing support and encouragement and for many helpful comments on the draft manuscript.

The authors also wish to acknowledge the seminal contributions of two pioneers of this field, the late Frank B. Hill and Robert L. Pigford. Several of their publications are cited in the present text, but their influence is far broader than the citations alone would suggest. Suffice it to say that much of the book would not have been written without their encouragement and the stimulus provided by their widsom and insight. Several graduate students and post-doctorals have made major contributions, most of which are recognized explicitly by citations. However, they, as well as others whose work may not have been directly referenced, also contributed in a very real way by helping the authors, through discussion and argument, to understand and appreciate some of the subtleties of PSA systems. It would be remiss not to mention by name M. M. Hassan, J. C. Kayser, N. S. Raghavan, and H. S. Shin.

This book is not intended as an exhaustive review of PSA technology, neither is it a design manual. Rather, we have attempted to present a

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coherent general account of both the technology and the underlying theory. Perhaps more than in other processes the rational design and optimization of a pressure swing adsorption process requires a reasonably detailed mathematical model. The two commonly used approaches to PSA modeling, equilibrium theory, and dynamic numerical simulation are discussed in some detail in Chapters 4 and 5. Inevitably these chapters are somewhat mathematical in approach. The details may be important only to those who are involved in process design and optimization but we hope that the more general reader will still be able to gain some insight concerning the underlying principles and the strengths and limitations of the various approaches.

A three-way collaboration between authors inevitably raises some difficulties since it becomes hard to maintain consistency in style and emphasis and to avoid repetition between different sections of the text. We hope, however, that the advantages of a more authoritative treatment of the subject will more than compensate for any such deficiencies. From our perspective the collaboration has proved interesting and instructive, and we have encountered no serious disagreements amongst ourselves.

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## List of Symbols

a	sorbate activity; external area per unit volume for adsorben sample (Eq. 2.46)
A	adsorbent surface area per mole (Eq. 2.10); $A_{cs} + A'$ (Table 5.10)
41	membrane area (Eq. 8.1)
A'	cross-sectional area of column wall (Table 5.10)
$A_{\rm cs}$	internal cross-sectional area of column
$A_{\rm s}$	Helmholtz free energy (Eq. 2.11)
A(k,i)	collocation coefficient for internal (intraparticle) concentration profile (Appendix B)
AH(j,i)	collocation coefficient for velocity profile during pressurization (Appendix B)
Ax(j,i)	collocation coefficient for the external (fluid-phase) concentration profile (Appendix B)
b	Langmuir constant
$b_{0}$	pre-exponential factor $(b = b_0 e^{-\Delta U/RT})$
B	mobility coefficient (Eq. 2.29); constant in Eq. 4.76
B(k,i)	collocation coefficient for the intraparticle (internal) phase
B(10,17)	Laplacian
Bx(j,i)	collocation coefficient for the external fluid-phase Laplacian
C	sorbate concentration in gas phase
$c_{o}$	sorbate concentration in feed
C	total gas-phase concentration
$C_{\sigma}$	volumetric heat capacity of gas $(\rho C_p)$
0	ordinate mont outputtly of Eus (pon)

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volumetric heat capacity of solid  $(\rho C_p)$ Cs heat capacity of steel wall (mass basis) (Table 5.10)  $C_{p \text{ steel}}$ internal diameter of adsorbent column D diffusivity micropore or intracrystalline diffusivity  $D_{c}$ effective diffusivity De Knudsen diffusivity  $D_{\mathrm{K}}$ axial dispersion coefficient  $D_{\mathrm{L}}$ molecular diffusivity  $D_{\rm m}$  $D_{\rm p}$ pore diffusivity Ediffusional activation energy  $E_{A}$ enrichment of heavy component  $(\bar{y}/y_{AF})$  $f_{i,j}$   $f'_{j}$  Fisotherm function for component i at composition j isotherm slope  $(dq^*/dc)$  at composition j total feed volume  $F_{\rm s}$ free energy of adsorbed phase (Eq. 2.11)  $F_A, F_B$ fractions of components A, B desorbed from column during depressurization Gpurge-to-feed velocity ratio Gibbs free energy of adsorbed phase (Eq. 2.8)  $G_{\varsigma}$ h overall heat transfer coefficient  $\Delta H$ enthalpy change on adsorption J flux of sorbate k overall mass transfer (LDF) rate coefficient based on adsorbed phase concentration adsorption equilibrium constant or isotherm slope; constant in K  $K_{\rm c}$ adsorption equilibrium constant on crystal (microparticle) volume K adsorption equilibrium constant or isotherm slope based on sorbate pressure  $K_{\rm o}, K_{\rm o}'$ pre-exponential factors (Eq. 2.2) effective thermal conductivity of steel wall (Table 5.10)  $K_{\mathrm{L}}$ adsorbent bed length phenomenological coefficients  $L_B, L_A$ molecular weight; constant in quadratic isostherm expression M exponent in Freundlich isotherm expression moles of adsorbable component (Eq. 2.8) na moles of solid adsorbent (Eq. 2.8)  $n_s$ flux relative to fixed frame of reference (Eq. 2.26); total moles N (gaseous and adsorbed) in bed at time tpartial pressure of sorbate p saturation vapor pressure Ps absolute pressure (in column) P

rate of change of pressure during feed step (Eq. 4.35)

$P_{\mathrm{H}}$	high pressure (at end of pressurization)
$P_{\rm F}^{\rm n}$	feed pressure
$P_{\rm L}$	low pressure (during purge step)
$P_{\rm cH}$	high pressure for compressor
$P_{\rm cL}$	low pressure for compressor
Pe	Peclet number $(v_{oH}L/D_L)$
80	absolute pressure ratio $P_{\rm H}/P_{\rm L}$
80 1	pressure ratio $P_{\rm H}/P_{\rm F}$
& F	pressure ratio $P_{\rm F}/P_{\rm L}$
B H	pressure ratio $P_{\rm H}/P_{\rm L}$ (end of pressurization versus end of
10	blowdown)
60 c	absolute compression ratio $P_{\rm cH}/P_{\rm cL}$
q	adsorbed phase concentration
$q^*$	equilibrium value of $q$
$q_{o}$	value of q at equilibrium with feed (concentration $c_0$ )
$\bar{q}$	value of q averaged over an adsorbent particle
$q_{\mathrm{s}}$	saturation limit
Q	molar gas flow rate
r	radial coordinate in microparticle
$r_{\rm c}$	microparticle radius
$r_{\rm in}, r_{\rm out}$	inner and outer radii of column
R	radial coordinate in a microparticle; gas constant $(R_g)$ ; product recovery
$R_{p}$	macroparticle radius
$S_{\rm E}$	equilibrium selectivity $K_A/K_B$
$S_{\mathbf{k}}$	kinetic selectivity $D_A/D_B$
Sh	Sherwood number $2R_{\rm p}k_{\rm f}/D_{\rm m}$
t	time
$t^*$	adsorption or desorption time
T	temperature
$T_{\rm o}$	feed temperature
$\Delta U$	internal energy change or adsorption
U	interstitial gas velocity
$U_{o}$	interstitial gas velocity at inlet
$\overline{U}$	dimensionless interstital gas velocity $v/v_{\rm oH}$
V	volume
$W_{\rm c}$	velocity of concentration front
$w_{t}$	velocity of temperature front
$W_{\rm c}'$	velocity of shock front
X	mole fraction (of component A) in adsorbed phase; dimensionless
	adsorbed phase concentration averaged over a macroparticle $\bar{q}_i/\bar{q}_{is}$
$X_{c}$	dimensionless adsorbed phase concentration averaged over a
С	microparticle $(q/q_s)$
	1/ 4s/

X	fraction of complete purge
y	mole fraction of $A$ in gas phase
$\bar{y}_{\rm bd}$	average mole fraction (of raffinate product B) in blowdown gas
$\overline{y}_{\rm bd}$ $\overline{y}_{\rm pdt}$	average mole fraction (of raffinate product B) in high-pressure
	product stream
Z	axial distance
Z	dimensionless axial distance $z/L$

### **Greek Symbols**

- $\alpha$  permeability ratio (intrinsic separation factor);  $t_{\rm H}/(t_{\rm H}+t_{\rm L})$  (in Table 5.9)
- $\alpha'$  separation factor x(1-y)/y(1-x) or y(1-x)/x(1-y)
- $\alpha_k$  kinetic selectivity (effective)—see Eq. 2.46
- $\beta$  parameter characterizing heat effect  $[(\Delta H/C_s)(\partial q^*/\partial T)_p]$  in Eq. 2.46; adsorption selectivity parameter  $\beta_A/\beta_B$ ;  $b_iC$
- $\beta_i$  ratio of hold-up component i in void space as fraction of total hold-up  $[1 + ((1 \varepsilon)/\varepsilon)K_i]^{-1}$
- $\gamma$  ratio of gas heat capacities at constant pressure and constant volume
- $\gamma_{\rm E}$  ratio of Langmuir constants  $b_B/b_A$
- $\gamma_k$  ratio of micropore diffusivities  $D_{cB}/D_{cA}$
- $\gamma_{\rm s}$  ratio of saturation capacities  $q_{B\rm s}/q_{A\rm s}$
- $\Gamma$  dimensionless parameter  $(r_c^2/D_{Ac})(3k_f/R_p)(C/q_{As})$
- $\Gamma'$  dimensionless parameter  $(r_c/D_{Ac})(C/q_{As})k_f$
- ε voidage of adsorbent bed
- $\epsilon_{\rm p}$  porosity of adsorbent particle
- $\zeta$   $[1 + \xi P_{\rm H} y_{\rm F} \beta_{A_0} (1 \beta)]^{-1}$  (Chapter 4)
- $\eta$  mechanical efficiency of compression; dimensionless radial coordinate  $R/R_{\rm p}$
- $\theta$  adsorption selectivity parameter  $\theta_A/\theta_B$
- dimensionless concentration  $q_i/q_{is}$  (Chapters 2 and 5); parameter  $\theta_i$   $(P, y_1, y_2) = [1 + ((1 \varepsilon)/\varepsilon)((f_{i2} f_{i1})/(y_{i2} y_{i1}))(RT/P_H)]^{-1}$ , where 1 and 2 refer to arbitrary states (Chapter 4)

- $\theta_{\rm c}$  dimensionless adsorption or desorption time  $(\epsilon_{\rm p}D_{\rm p}/R_{\rm p}^2)(c_0/q_0)$   $t^*$  (for macropore control) or  $D_{\rm c}t^*/r_{\rm c}^2$  for micropore control
- $\lambda$  ratio of dead volume to column volume; non-linearity parameter  $q_{\rm o}/q_{\rm s}$
- $\mu$  chemical potential; viscosity; mean residence time in column
- $\Xi$  parameter  $((1 \varepsilon)/\varepsilon) (M_A/RT)$
- $\xi (1-\varepsilon)M_{\rm A}/\varepsilon R$
- $\rho$  density
- $\sigma^2$  variance of pulse response
- $\tau$  dimensionless time variable,  $tv_{\rm OH}/L$  (LDF model);  $tD_{\rm c}/r_{\rm c}^2$  (pore diffusion model)
- $\phi$  parameter  $\epsilon A_{cs} LP_L/\beta_A RT$
- Φ surface potential
- $\Omega$  parameter defined by Eq. 5.16; integral function used in determining recovery for pressurization with feed

## Subscripts

A, B	components $A$ (more strongly adsorbed) and $B$ (less strongly adsorbed)
В	blowdown step
c	micropore or intracrystalline
ci	component i in microparticle
C	column
DV	dead volume
ei	equivalent value (for component $i$ ) in countercurrent flow model
F	feed or feed end
G	purge-to-feed ratio
H, OH, iH	high-pressure step, at inlet during high-pressure step, and for component $i$ during high-pressure step
i	refers to species $i$ ( $A$ or $B$ ).
ip, is	species $i$ in microparticle, species $i$ at saturation
I	intermediate
L, $oL$ , $iL$	low-pressure (purge) step, at inlet during low-pressure step, and for component <i>i</i> during low-pressure step
o, oi	limiting or reference value, limiting or reference value for
	component i
O	outlet or effluent
p	macropore or macroparticle
P	product end or pressurization step
PU	purge step

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#### **SUBSCRIPTS**

R rinse step

s saturation value

S condition following pressurization step

SH shock wave w at wall

W combined blowdown and purge step effluent; waste or

byproduct

0, 1, 2 initial state, ahead of shock, and behind shock

Superscript \* is sometimes used to denote and emphasize "equilibrium

value"

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