

J. M. Sørensen

W. Arlt

LIQUID-LIQUID EQUILIBRIUM DATA COLLECTION

Ternary and Quaternary Systems



Chemistry Data Series
Vol. V, Part 3

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PREFACE OF AUTHORS

This work consists of three Parts. Part 1 deals with binary liquid-liquid equilibria and Parts 2 and 3 with ternary liquid-liquid equilibria.

The correlation and prediction of liquid-liquid equilibria (LLE) using models for liquid phase non-idealities is a subject within chemical engineering which is not yet mastered quantitatively. Model inadequacies may be one explanation for this. However, this work will show that the results may be quite good with existing models if they are used properly, i. e. if the parameter estimation procedure as well as the data base are chosen carefully.

In addition to an extensive collection of experimental binary, ternary, and quaternary data, this work contains NRTL and UNIQUAC parameters reduced from these data. For each ternary system (Parts 2 and 3) we give a specific set of NRTL and UNIQUAC parameters which emphasizes the distribution ratio of the solute at small concentrations. This makes semi-quantitative extraction calculations possible for many systems. We also include a table of UNIQUAC parameters for the A-B interaction reduced from a large number of systems with components A, B, and any third component. These parameters will usually be better for predicting multicomponent LLE than parameters based on VLE-data.

The work leading to these three books began in 1977 at Institutte for Kemiteknik, Lyngby, Denmark, where Aa. Fredenslund started a project called "A Group Contribution Method for Predicting Liquid-Liquid Equilibria". An initial step in this project was to investigate how existing molecular models (e.g. NRTL and UNIQUAC) behave in LLE calculations. For this purpose a parameter estimation procedure and a large data base were established.

The above project was close to research plans at Dortmund University, and a collaboration was initiated in 1978 with the purpose of jointly preparing this publication. The data collection was extended, and the authors have profited very much by the experience of J. Gmehling and U. Onken who started Volume I of this series („Vapor-Liquid Equilibrium Data Collection“).

Simultaneously the parameter estimation procedure was further refined under daily guidance of Aa. Fredenslund and P. Rasmussen to whom the authors are very grateful.

The parameter estimation from ternary LLE-data involves many numerical problems. The authors wish to thank M. L. Michelsen (Institutte for Kemiteknik, Lyngby) for providing the final version of the estimation procedure. Finally, we dedicate special thanks to T. Magnusson (DECHEMA, Frankfurt/Main) for many fruitful discussions and help and to colleagues and students in Lyngby and Dortmund for various kinds of assistance.

The authors hope that the data collection and parameters of this work will be of use to the industry. We also hope that the availability of the large amount of data will facilitate the testing of new models at universities.

The authors

PREFACE OF EDITORS

Subjects of the DECHEMA Chemistry Data Series are the physical and thermodynamic property data of chemical compounds and mixtures essentially for the fluid state covering PVT data, heat capacity, and entropy data, phase equilibrium data, transport and interfacial tension data.

The main purpose is to provide chemists and engineers with data for process design and development. For computer based calculations in process design appropriate correlation methods and accurate data must be used. These are only in some cases available in open literature. For that reason the most urgent requirement regarding the publication of data is to offer critically evaluated and reliable data. This will be the goal of the series.

DECHEMA gives an opportunity to authors especially from universities to publish not only their theoretical results, but also their measured or compiled data, most often a large amount.

After that a successful group contribution method for the prediction of vapor-liquid equilibria (UNIFAC) had been presented to the scientific community several years ago, the needs for a similar treatment of liquid-liquid equilibria led to a cooperation between the Dechema Data Compiler Development Group and Professor Fredenslund at the Instituttet for Kemiteknik in Lyngby, who has much experience in this field.

During this cooperation, J. M. Sørensen and W. Arlt, who is already co-author of Volume I of the Series, have collected the mutual solubility data of more than 2000 binary, ternary and quaternary mixtures of organic liquids.

This compilation is now being published as Volume V of this series, in 3 parts giving not only measured data but also evaluated correlation constants and recommended values. We hope that this gives an instrument that will allow the users to solve their problems considerably more easily and more quickly than before.

Frankfurt/Main, October 1980

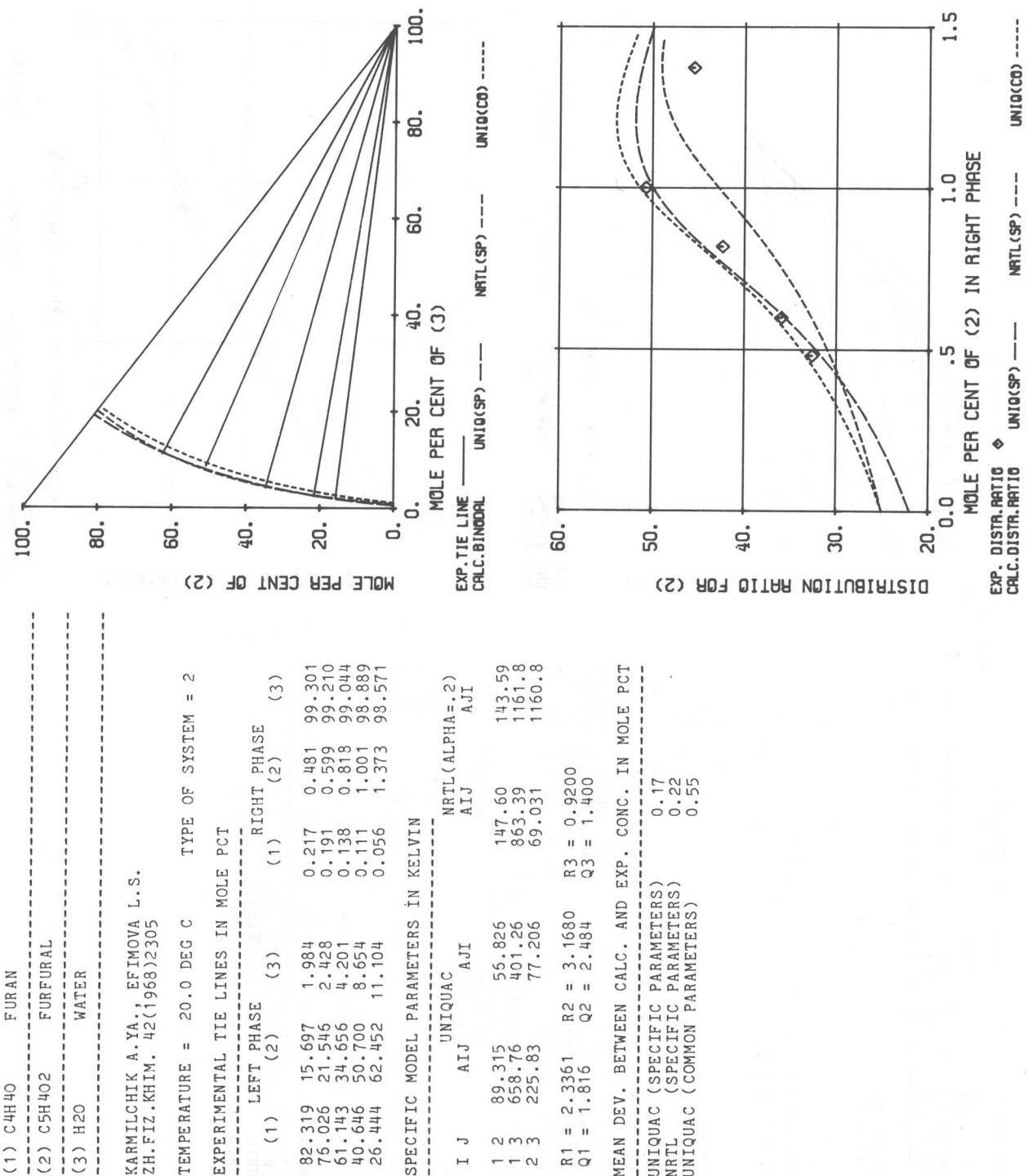
Dieter Behrens
Reiner Eckermann

CONTENTS
Vol. V, Part 3

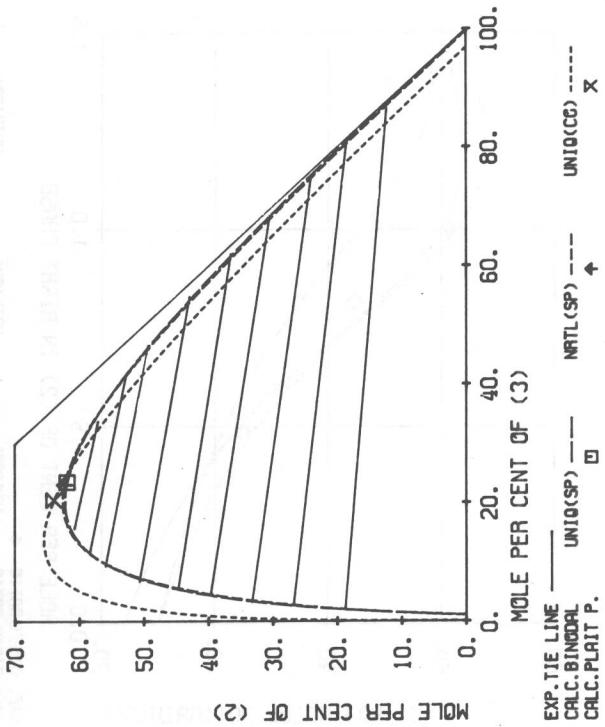
Preface of Authors	V
Preface of Editors	VI
Contents Volume V, Part 3	VII
Contents Volume V, Part 2	VIII
Guide to Tables, Figures, List of Common Parameters, and Index	IX
Ternary Tables and Figures, C ₄ —C ₉ for the smallest molecule	1
Quaternary Tables	366
List of Common UNIQUAC Parameters.....	394
Alphabetical Compound Index for Ternary Systems	446
Formula Index of Quaternary Systems	604

CONTENTS
Vol. V, Part 2

Preface of Authors	V
Preface of Editors	VI
Contents Volume V, Part 2	VII
List of Symbols	VIII
Introduction	IX
1. Ternary and Quaternary LLE Data Collection	IX
2. Thermodynamic Conditions of Multicomponent Liquid-Liquid Equilibria	XII
3. Comparison Between Different References	XIII
4. Models for Liquid-Liquid Equilibria	XIII
5. Computation of Multicomponent Liquid-Liquid Equilibria	XIV
6. Computation of Binodal Curves for Ternary Systems	XIV
7. Parameter Estimation from Ternary Liquid-Liquid Equilibrium Data	XV
8. Specific Parameters	XVI
9. Common Parameters	XVI
10. Distribution Ratios	XVII
11. Prediction of Multicomponent Liquid-Liquid Equilibria (Continued from Part 1, p. XV)	XVII
12. Examples of Predictions	XVIII
13. Prediction of Quaternary Systems	XX
14. Conclusion	XX
References to Literature	XXI
Guide to Tables, Figures, List of Common Parameters, and Index	XXII
Computer Programs	XXV
a. UNIQUAC r- and q-conversion	XXVI
b. Binodal Curve Construction	XXIX
Ternary Tables and Figures, C ₁ – C ₃ for the smallest molecule	1–625
List of Common UNIQUAC Parameters	see Part 3
Alphabetical Compound Index	see Part 3



$C_4H_8S \cdot C_4H_8O_2S$



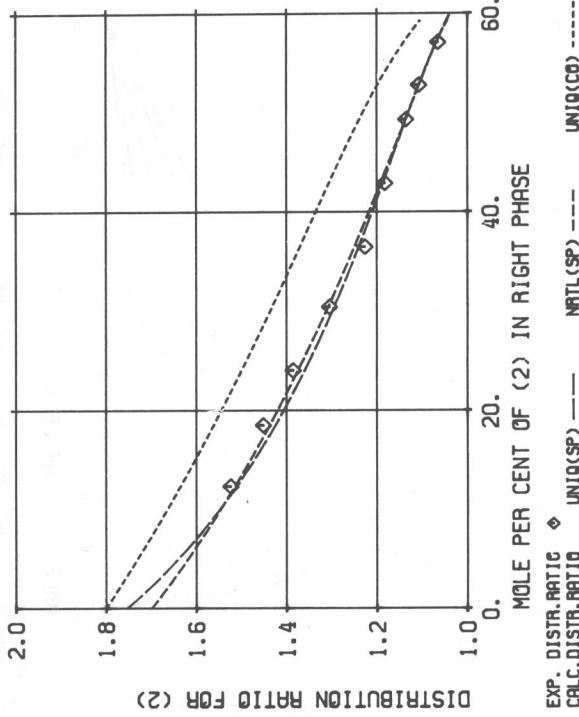
SPECIFIC MODEL PARAMETERS IN KELVIN

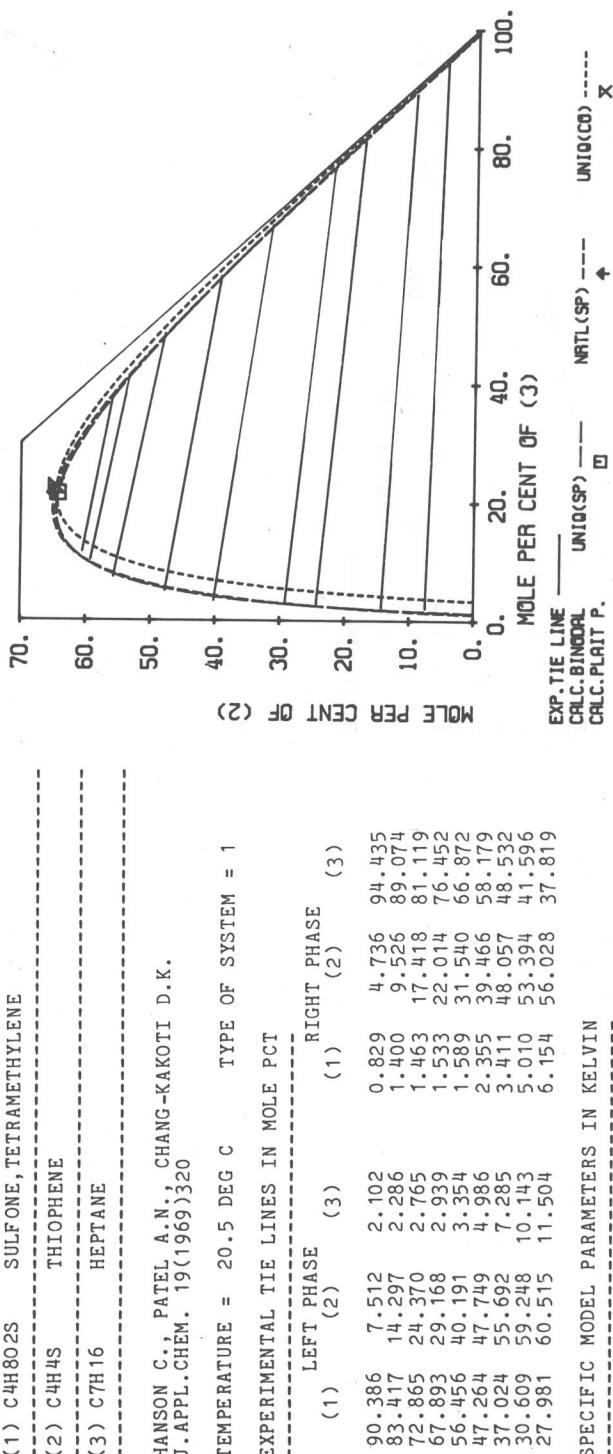
I	J	UNIQUAC	NRTL (ALPHA=2)
AJ	AJ	AJ	AJ
1 2	-30.246	-58.263	-196.89
1 3	98.540	575.52	535.19
2 3	-80.273	65.528	869.12
			122.0
			127.82

$$R_1 = 4.0358 \quad R_2 = 2.8569 \quad R_3 = 4.4998 \\ Q_1 = 3.200 \quad Q_2 = 2.140 \quad Q_3 = 3.856$$

MEAN DEV. BETWEEN CALC. AND EXP. CONC. IN MOLE PCT

UNIQUAC (SPECIFIC PARAMETERS)	0.28
NRTL (SPECIFIC PARAMETERS)	0.37
UNIQUAC (COMMON PARAMETERS)	2.52



$C_4H_8O_2S - C_4H_8O_2S$


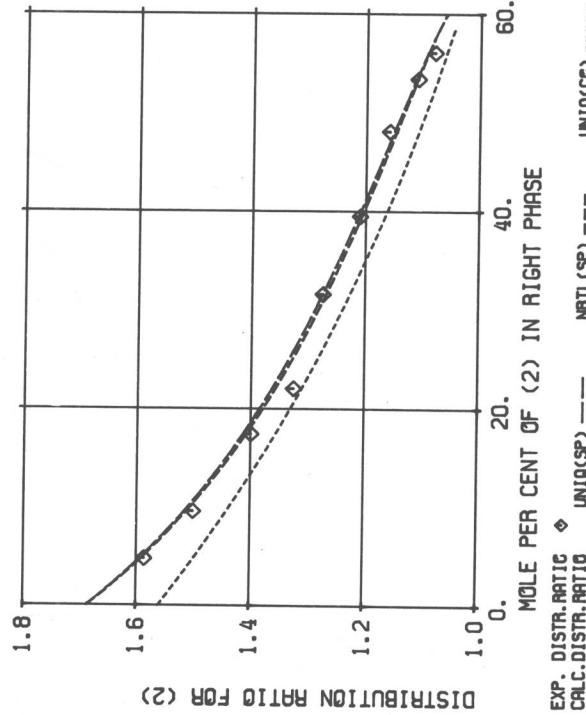
SPECIFIC MODEL PARAMETERS IN KELVIN

I	J	UNIQUAC	NRTL (ALPHA=.2)
1	2	A1J	A1J
1	3	-350.04	37.841
1	3	70.172	434.12
2	3	-67.753	-164.60
			280.30
			-442.52

$$R1 = \frac{4.0358}{3.200} \quad R2 = \frac{2.8569}{2.140} \quad R3 = \frac{5.1742}{Q3 = 4.396}$$

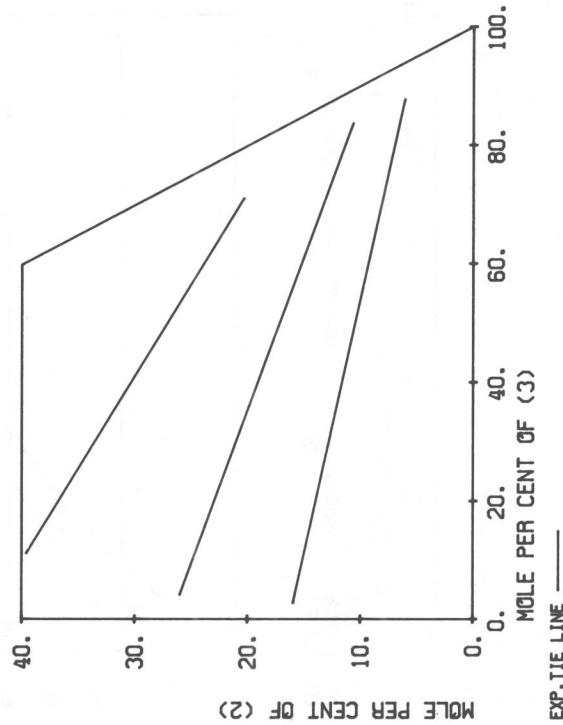
MEAN DEV. BETWEEN CALC. AND EXP. CONC. IN MOLE PCT

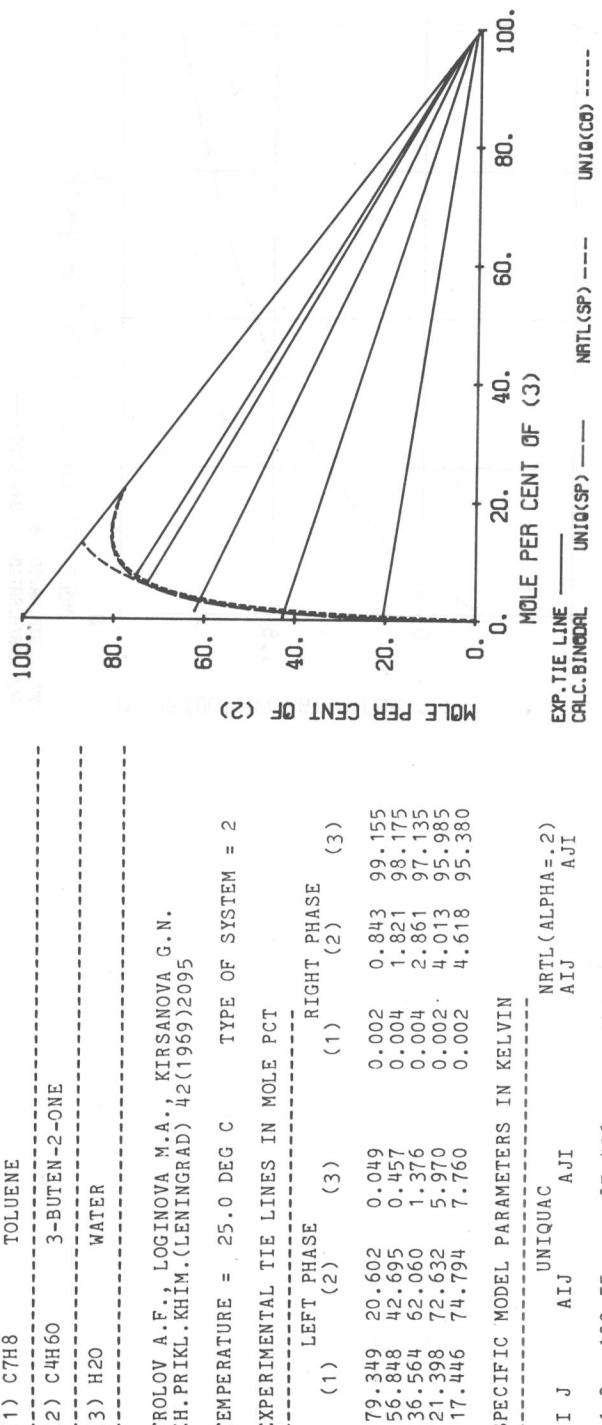
UNIQUAC (SPECIFIC PARAMETERS)	0.35
NRTL (SPECIFIC PARAMETERS)	0.34
UNIQUAC (COMMON PARAMETERS)	1.33





EXPERIMENTAL TIE LINES IN MOLE PCT			
TEMPERATURE = 50.0 DEG C TYPE OF SYSTEM = 1			
LEFT PHASE			
(1)	(2)	(3)	RIGHT PHASE
81.266	15.950	2.784	(1) (2) (3)
69.857	25.994	4.149	6.146 6.076 87.779
49.263	39.590	11.147	5.563 10.665 83.773
			8.489 20.324 71.187





SPECIFIC MODEL PARAMETERS IN KELVIN

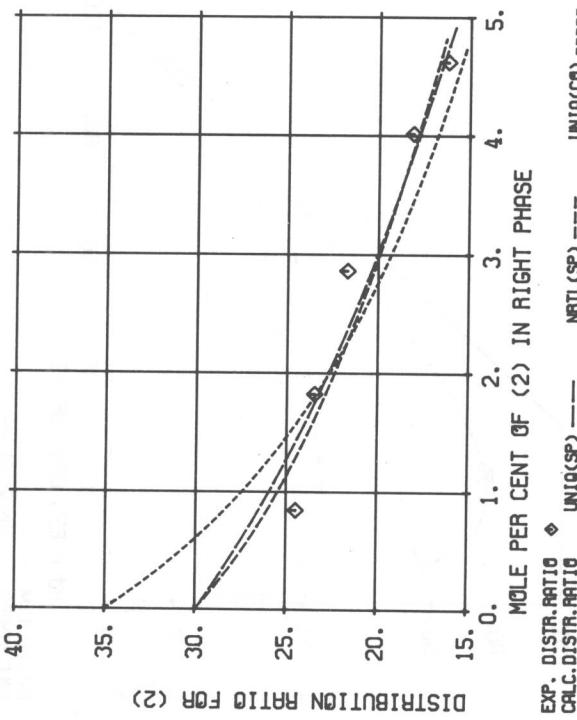
I	J	UNIQUAC	NRTL (ALPHA=.2)
		AIJ	AJI
1	2	-100.55	87.426
1	3	1277.0	714.85
2	3	410.03	0.30367

$$R1 = 3.9228 \quad R2 = 3.0178 \quad R3 = 0.9200$$

$$Q1 = 2.968 \quad Q2 = 2.664 \quad Q3 = 1.400$$

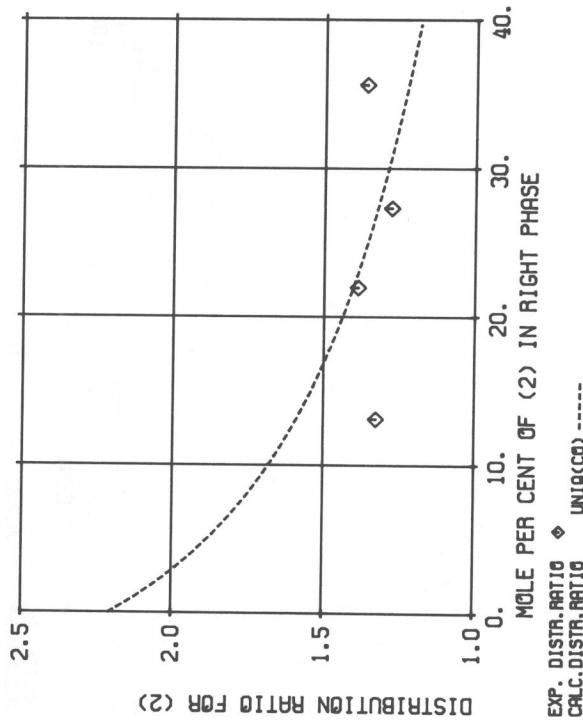
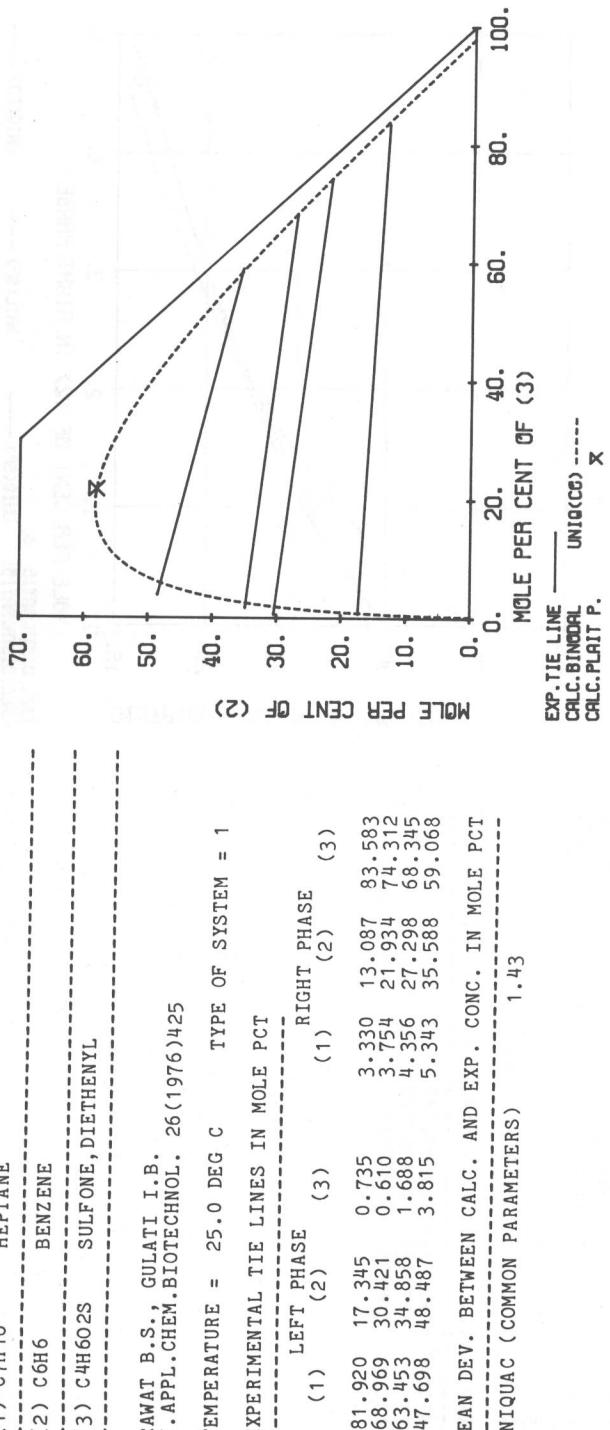
MEAN DEV. BETWEEN CALC. AND EXP. CONC. IN MOLE PCT

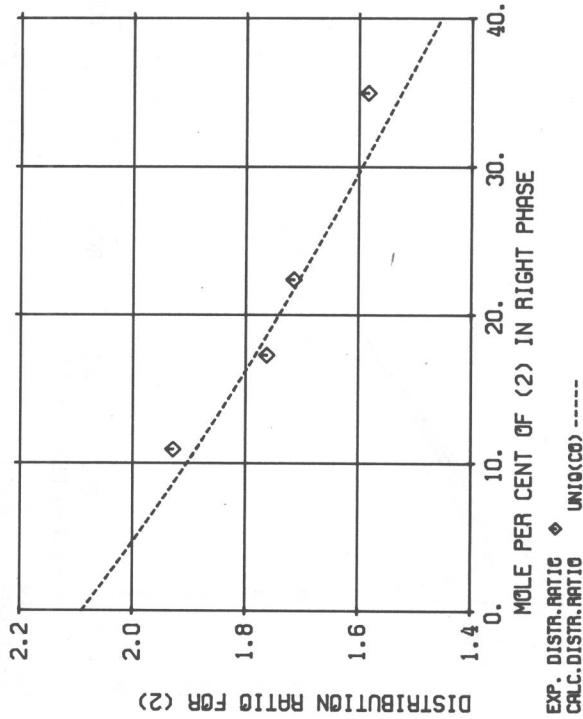
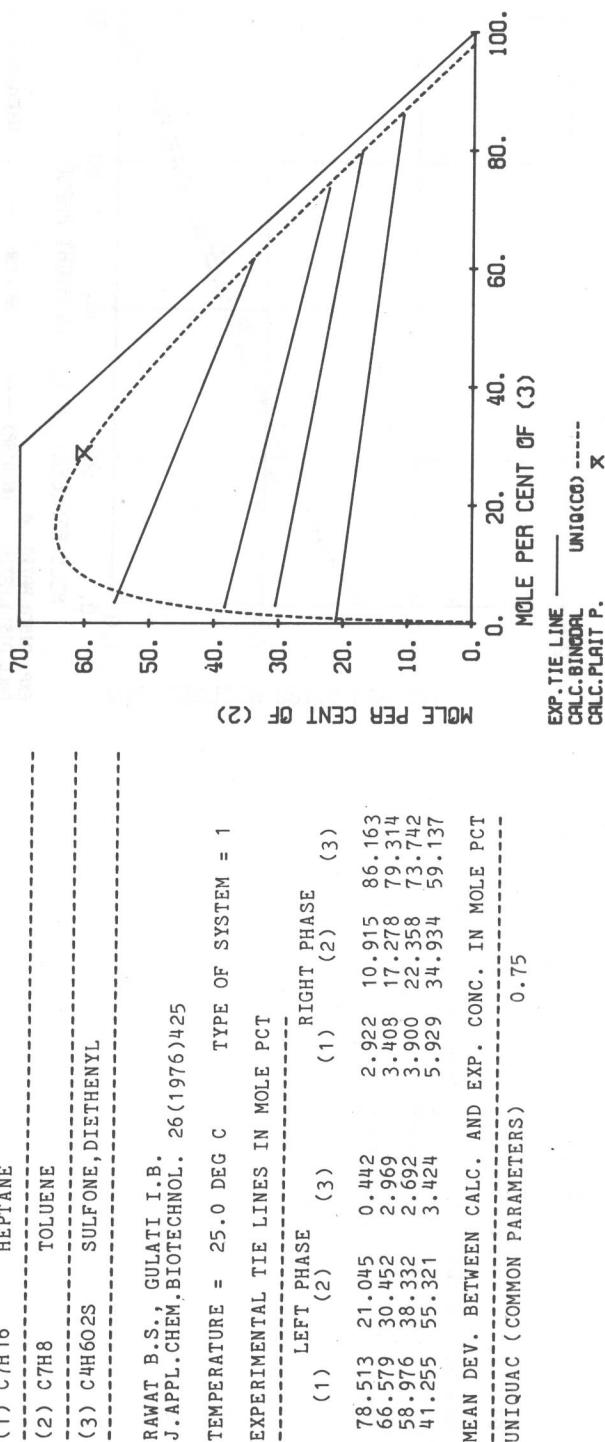
UNIQUAC (SPECIFIC PARAMETERS)	0.47
NRTL (SPECIFIC PARAMETERS)	0.56
UNIQUAC (COMMON PARAMETERS)	0.66



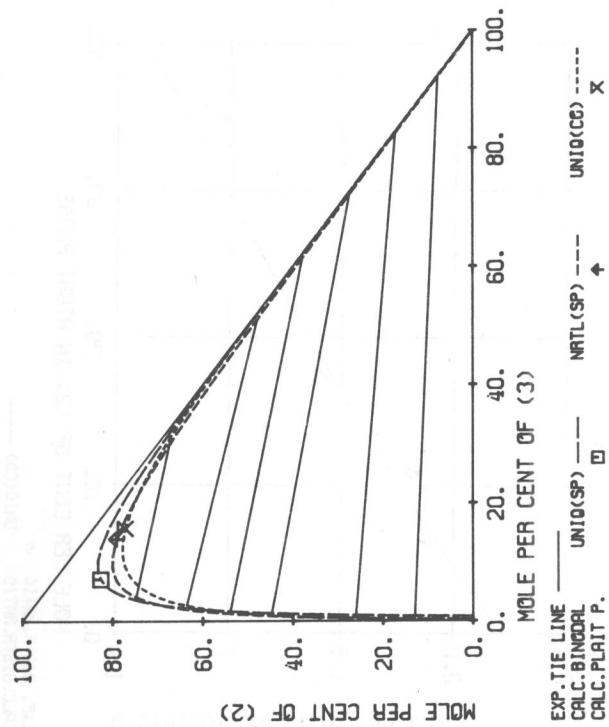


(1) C7H16 HEPTANE
 (2) C6H6 BENZENE
 (3) C4H6O2S SULFONE, DIETHENYL





EXP. DISTR. RATIO ◆ UNIQUAC -----
 CALC. DISTR. RATIO UNIQUAC -----

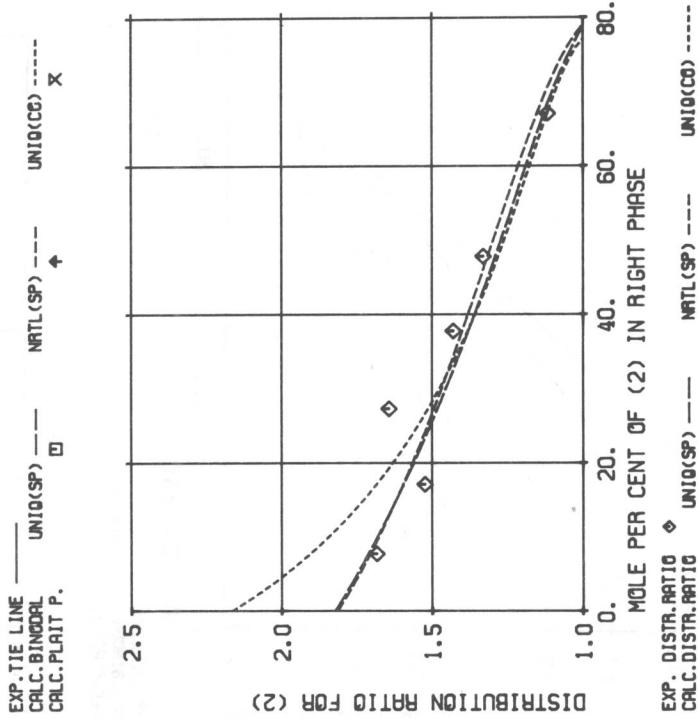
$C_4H_6O_3 \cdot C_6H_6$


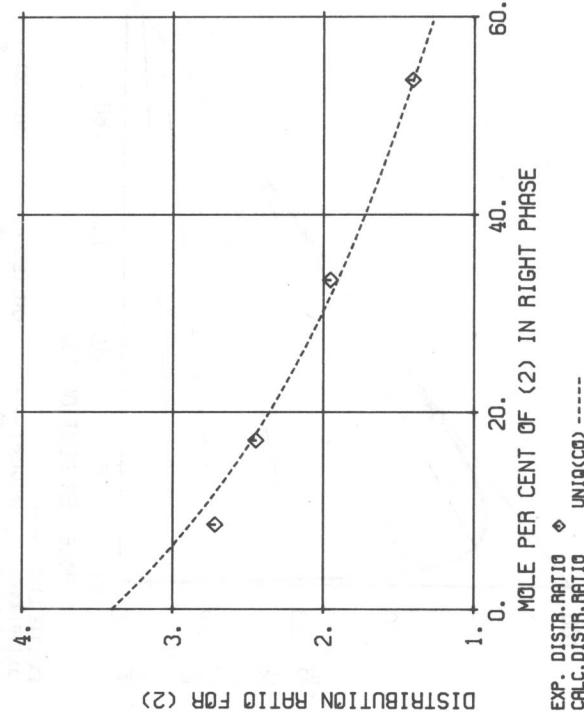
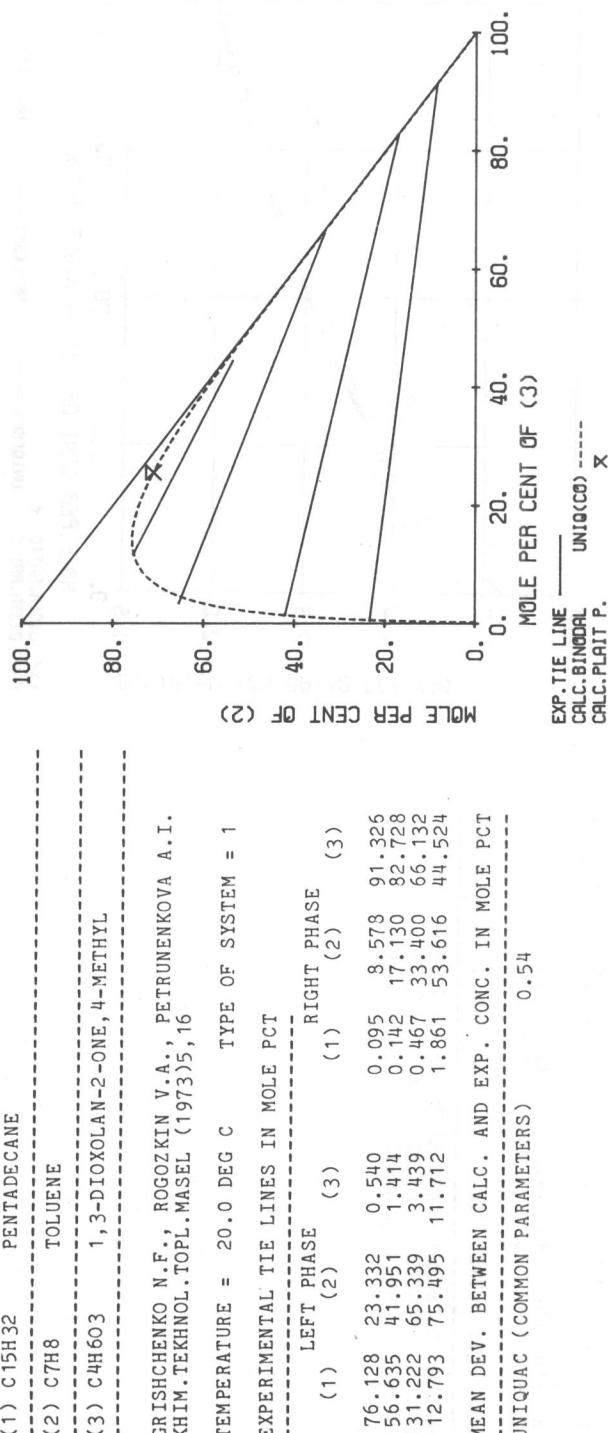
	UNIQUAC		NRTL (ALPHA=1.2)	
I J	AIJ	AJI	AIJ	AJI
1 2	165.12	-24.752	-549.56	556.34
1 3	474.27	129.98	1223.4	1410.0
2 3	236.12	-13.422	945.97	-489.64

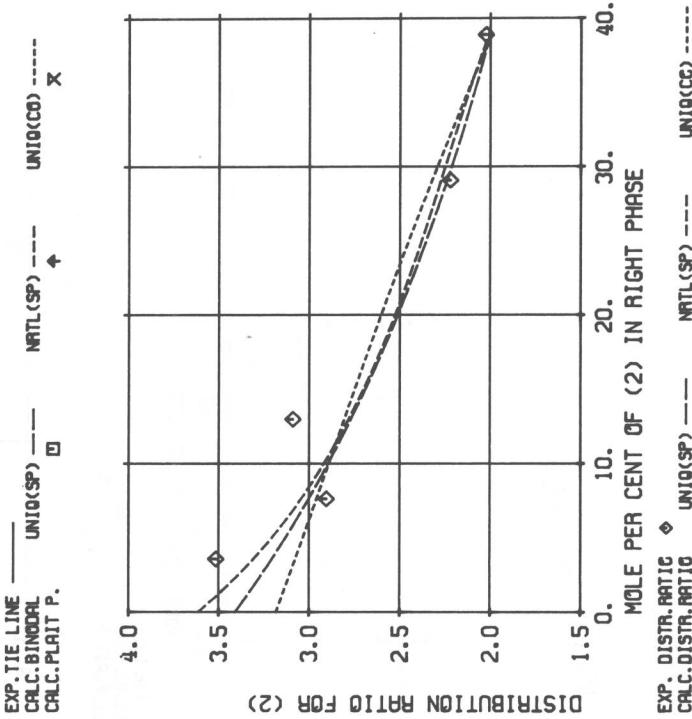
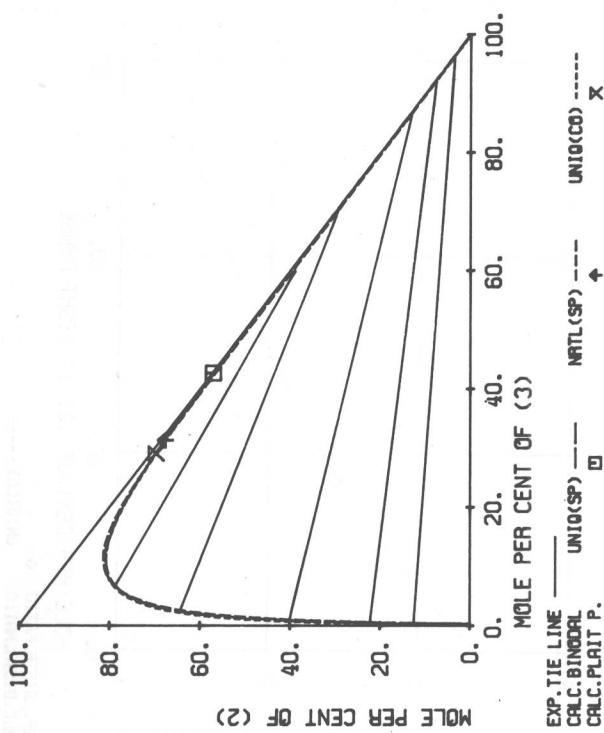
R1 = 10.5694 R2 = 3.1878 R3 = 3.2815
Q1 = 8.7116 Q2 = 2.400 Q3 = 2.736

MEAN DEV. BETWEEN CALC. AND EXP. CONC. IN MOLE PCT

UNIQUAC (SPECIFIC PARAMETERS)	0.90
NRTL (SPECIFIC PARAMETERS)	0.97
UNIQUAC (COMMON PARAMETERS)	1.07





$C_4H_6O_3-C_8H_{10}$ 

(1) C15H32	PENTADECANE
(2) C8H10	BENZENE, 1,2-DIMETHYL
(3) C4H6O3	1,3-DIOXOLAN-2-ONE, 4-METHYL KHM.TEKHNOL.TOPL.MASEL (1973)5, 16

GRISHCHENKO N.F., ROGOZKIN V.A., PETRUNENKOVA A.I.

KHM.TEKHNOL.TOPL.MASEL (1973)5, 16

TEMPERATURE = 20.0 DEG C TYPE OF SYSTEM = 1

EXPERIMENTAL TIE LINES IN MOLE PCT

SPECIFIC MODEL PARAMETERS IN KELVIN

UNIQUAC $\alpha_{12} = 0.2$

$\alpha_{13} = 0.2$

$\alpha_{23} = 0.2$

$\alpha_{11} = 0.2$

$\alpha_{22} = 0.2$

$\alpha_{33} = 0.2$

$\alpha_{123} = 0.2$

$\alpha_{132} = 0.2$

$\alpha_{213} = 0.2$

$\alpha_{231} = 0.2$

$\alpha_{312} = 0.2$

$\alpha_{321} = 0.2$

$\alpha_{111} = 0.2$

$\alpha_{222} = 0.2$

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$\alpha_{3333} = 0.2$

$\alpha_{11111} = 0.2$

$\alpha_{22222} = 0.2$

$\alpha_{33333} = 0.2$

$\alpha_{111111} = 0.2$

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$\alpha_{111111111111111} = 0.2$

$\alpha_{222222222222222} = 0.2$

UNIQUAC -----
EXP.DISTR.RATIC ◆ UNIQUAC -----
CALC.DISTR.RATIC