



1999 IEEE MTT-S INTERNATIONAL MICROWAVE **SYMPOSIUM DIGEST**)

Volume 4

June 13 - 19, 1999 Anaheim Convention Center Anaheim, California

Digest Editor Mehran Matloubian Elmira Ponti

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1999 IEEE MTT-S International Microwave Symposium



JUNE 13-19, 1999 • ANAHEIM CALIFORNIA

1999 IEEE MTT-S INTERNATIONAL MICROWAVE SYMPOSIUM DIGEST

Technical Program Schedule Thursday, June 17

1999 IEEE MTT-S International Microwave Symposium



JUNE 13-19, 1999 • ANAHEIM CALIFORNIA

1999 IEEE MTT-S INTERNATIONAL MICROWAVE SYMPOSIUM DIGEST

Technical Sessions

1999 IEEE MTT-S International Microwave Symposium



JUNE 13-19, 1999 • ANAHEIM CALIFORNIA

Session TH1A

Integrated Systems for Wireless

Chair **V. Nair**Motorola, Inc.

Co-Chair **R. Marks** NIST

This session reflects the advancement in integration for subsystems for wireless applications. Power, voltage, size, weight, and cost requirements, along with demands for multimode and multiband operation, continually push this integration to higher levels.

The first three papers cover integrated technologies for power amplifiers. The first addresses the difficult issue of integrating filters on GaAs. The second provides details on a highly integrated power amplifier on AlGaAs/GaAs. The third takes a hybrid approach but nevertheless arrives with a compact power amplifier module in GaAs on a multilayer multichip module.

The fourth paper pushes integration even further, demonstrating a complete monolithic transceiver front end for 1.9 GHz wireless applications. This includes the low noise amplifier, mixer, local oscillator, buffer, and power amplifier.

The fifth paper presents a direct conversion receiver based on a resistive FET mixer. The final paper applies a SAW delay line to a signal processing problem for spread spectrum receivers.

8:00 am - 9:40 am Thursday, June 17, 1999 Room A1

1999 Microwave Symposium Technical Program Schedule

Session TH1A Integrated Systems for Wireless

8:00 am-9:40 am		Room A1	Thursday, June 17	, 1999
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TH1A-5 9:20 am	C-Band Direct Conve S. Lin, Y. Qian and T. I	ersion Receiver Front-End Using a Resistive F (toh	ET Mixer	1409
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TH1B-4 9:00 am	A Broadband Microstrip-to-Waveguide Transition Using Quasi-Yagi Ant N. Kaneda, Y. Qian and T. Itoh	enna 1431
TH1B-5	Full Band Waveguide-to-Microstrip Probe Transitions Y.C. Leong and S. Weinreb	1439

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		Co-Chair: R. Weigel, University of Linz		
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TH1D-2 8:20 am	Production 7	Performance of a SAW Ladder-Type Filter at 3.15 GHz Us Fechnology er, A. Springer, R. Weigel, W. Ruile, R. Thomas, S. Berek and	_	1441
TH1D-3 8:40 am		Configurations and New SAW Duplexers for Single- and D Matsuura, N. Shibagaki and K. Sakiyama	ual-Band Cellular Rac	dios 1445
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TH1E-6 9:20 am		te Element Time Domain Analysis of Active Non-Linear M , R. Coccioli, Y. Qian, HB. Lee and T. Itoh	licrowave Circuits	1479

Session TH2A Intelligent Transportation Systems

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TH2B-2 10:30 am	30 GHz Tuned MEMS Switches J.B. Muldavin and G.M. Rebeiz	15	11
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Session TH2C

(Focused Session)

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TH2C-5 11:30 am	Laminated Photonic Band S M.J. Bloemer, M. Scalora and	tructures with High Conductivity and High J.P. Dowling	gh Transparency 893

Session TH2D

Superconducting Components and Subsystems

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TH2D-5 11:20 am	Cross-Coupled HTS Mic. JS. Hong, M.J. Lancaster	rostrip Open-Loop Resonator Filter on and JC. Mage	LAO Substrate	1559
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TH2E-3 10:50 am		ysis of X-Band MMIC Pre-Matched Power Cell Coccioli, B. Housmand and T. Itoh		1577
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F.A. Petz, J. Rosello-Guasch, C. Mavrocordatos and Ch.V. Narasimha Rao

Modular Design of SAR Electronics

2:00 pm

TH3A-4

2:20 pm

TH3A-5

2:40 pm

of Mines

R.J. Tan and R. Bender







1607

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Near-Field Synthetic Aperture Interferometric Microwave Radiometry for Remote Sensing

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TH3D-3 2:00 pm	Fast Hybrid Integral Equation-Neural Network Method for the Mod Transmission Lines PM. Piel, J. Griffith, TT. Lam and G.W. Pan	leling of Multiconductor 1673
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Session TH4C

(Joint with ARFTG)

Automated Characterization Techniques

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TH4C-5 4:40 pm	Communication Ap	terization of Integrated and Multilayered Dire oplications , F. Grandjean, G. Angenieux and S.A. Radiall	ectional Couplers for Wireless	1759
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Session THF1

Interactive Forum

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THF1-6 2:30 pm	NbN Hot Electron Bolometric Mixers—A New Technology for Low No. E. Gerecht, C.F. Musante, Y. Zhuang, K.S. Yngvesson, T. Goyette, J. Dicki P.A. Yagoubov, G.N. Gol'tsman, B.M. Voronov and E.M. Gershenzon	sise THz Receivers inson, J. Waldman,	1789	
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Session THF2

Interactive Forum

Biological Effects

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Session THF3

Interactive Forum

Active and Passive Phased Array Systems

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Session THF4

Interactive Forum

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Session THF5

Interactive Forum

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THF5-2 2:30 pm	Comparison of Methods for Adapter Charact J. Randa, W. Wiatr and R.L. Billinger	erization		1881
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THF5-4 2:30 pm	Effects of Moisture Desorption on Phase and PTFE/Ceramic Laminate Circuit Boards R.J. Fern and L.O. Duffy	Gain of RF Filters Made	with	Manuscript not available at time of printing
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High Efficiency and Broadband Excitation of Leaky Mode in Microstrip Structures

Y. Qian, B.C.C. Chang, T. Itoh, K.C. Chen* and C.K.C. Tzuang*

Electrical Engineering Department, University of California, Los Angeles
405 Hilgard Avenue, Los Angeles, CA 90095, USA
*Institute of Electrical Communication Engineering
National Chiao Tung University, Hsinchu, Taiwan

Abstract - This paper reports a novel efficiency technique for high and broadband excitation of the first higherorder leaky mode in microstrips. A uniplanar microstrip-to-CPS transition is employed to launch the odd leaky mode, and the mode purity is enhanced by suppressing the even fundamental mode using an optimized mode suppressor. An Xband prototype demonstrates excellent mode conversion efficiency as predicted by simulations. A record bandwidth of 20.2 % is achieved for a microstrip leaky-wave source based on this newly proposed structure.

I. Introduction

Leakage from higher-order modes in microstrips and other planar structures has attracted much attention since the pioneering work by Oliner [1]. Dispersion characteristics of the leaky modes have been analyzed with various techniques such as the spectral-domain moment method [2]. Leaky-wave microstrip antenna had been successfully demonstrated even before the nature of complex mode in the microstrip was fully characterized [3]. Recent efforts include active integrated leaky-wave antennas [4], which show great potential as

applications move towards higher microwave and MMW-wave frequencies.

One major concern with microstrip-based leaky wave structures is the simultaneous excitation of the even fundamental (quasi-TEM) mode in addition to the desired leaky mode. A slotline-fed structure should ideally excite a pure odd (leaky) mode, but the radiation efficiency was found to be inferior to a CPS-fed approach [5]. The CPS feeding, however, requires either a microstrip or CPWbased transition to realize the 180° phase difference. of the frequency Because dependence of these planar-type transitions, a substantial portion of even mode will be especially relatively excited. when a broadband design is required.

This paper reports our recent effort in developing broadband leaky mode launching structure for microstrip antenna applications. By using a uniplanar microstrip-to-CPS transition in combination with a mode suppressor consisting of optimized periodic slots, excellent mode conversion efficiency has been obtained. An X-band prototype was fabricated and tested, which gave satisfactory results. In a simple demonstration, a record bandwidth of 20.2 % (VSWR<2) was achieved for a microstrip leaky-wave source based on this new leaky mode launcher.

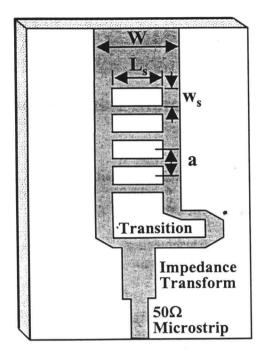


Fig. 1. Proposed microstrip leaky mode launcher with a broadband microstrip-to-CPS transition and transverse slots for even mode suppression.

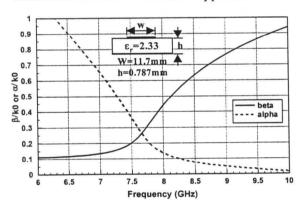


Fig. 2. Dispersion Characteristics of the first higher-order leaky mode in a 11.7 mm wide microstrip on Duroid substrate with ε_r =2.33 and thickness of 0.787mm.

II. DESCRIPTION OF STRUCTURE AND SIMULATION RESULTS

Fig. 1 shows the schematic of the proposed structure. A uniplanar microstrip-to-CPS transition is used to convert the quasi-TEM

mode from the 50 Ω feeding line into an odd mode which feeds the two edges of the leaky microstrip of width W. The transition has inherently very broad bandwidth, as we have demonstrated previously [6]. For a leaky microstrip with dimensions shown in Fig. 2, the calculated attenuation constant (α) indicates that it can serve as a proper leaky wave source in the frequency range of approximately 8 to 10 GHz. Accordingly, the two arms following the T-junction of the transition in Fig. 1 are designed to have 180° phase difference at around 9 GHz.

Meanwhile, in order to suppress the possible excitation of the fundamental even mode and enhance the purity of the desired leaky mode, a periodic structure of transverse slots cut in the microstrip, as proposed originally by Menzel in [3], is employed.

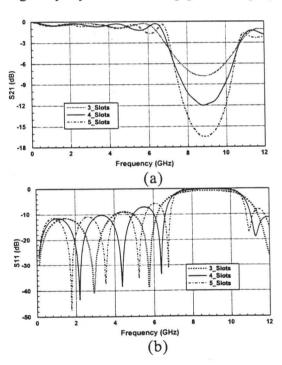


Fig. 3. FDTD simulation results for transmission (S21) and reflection (S11) of the fundamental mode in the microstrip with optimized transverse slots.