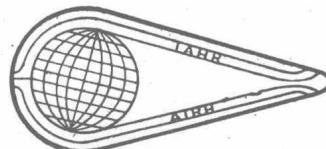


ASSOCIATION INTERNATIONALE
DE RECHERCHES HYDRAULIQUES

INTERNATIONAL ASSOCIATION
FOR HYDRAULIC RESEARCH

NEUVIEME ASSEMBLEE GENERALE
NINTH CONVENTION

Dubrovnik 1961
Yougoslavie



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INTRODUCTION

La Neuvième Assemblée Générale de l'Association Internationale de Recherches Hydrauliques a eu lieu à Dubrovnik (Yougoslavie) du 4 au 7 Septembre 1961. L'organisation du Congrès a été confié à l'Association Yougoslave de Recherches Hydrauliques, membre de l'Union Yougoslave des Ingénieurs et Techniciens. Au Congrès assistaient 241 participants et 56 dames de 33 pays. Le programme du Congrès comprenait:

A. THEMES PRINCIPAUX

1. Effets de turbulence sur des constructions hydrau-hydrauliques (27 mémoires)
2. Mécanique des courants d'eaux souterraines (37 mémoires)
3. Problèmes hydrauliques pour les machines à calculer (43 mémoires)
4. Modifications de courants naturels causées par des ouvrages (27 mémoires)

B. CONFERENCES GENERALES

1. Problèmes hydrauliques du Karst
2. Ecoulement en trois dimensions à travers la couche de limite
3. Transformation de l'énergie dans les zones de séparation

C. SEMINAIRES

1. Hydraulique de petites constructions dans l'irrigation et le drainage (10 abrégés)
2. Hydrodynamique fondamentale des écoulements à surface libre et des écoulements non uniformes (38 abrégés)

D. SYMPOSIUM

- Machines hydrauliques

E. SEANCE ADMINISTRATIVE

- Rapports concernant l'activité de l'AIRH entre les deux dernières Assemblées et l'élection des nouveaux conseils d'administration et d'exécution

Le Congrès a été ouvert le 4 Septembre à 10h 00 par le Président du Comité d'organisation Prof. Bogić Knežević. A la séance d'ouverture les congressistes étaient salués par le délégué du Conseil Exécutif Fédéral Yougoslav, M. Vinko Hafner et le maire de la ville de Dubrovnik, M. Vinko Betica. Les discours d'ouverture ont été prononcés par le président de l'AIRH, Dr. Arthur Ippen et le secrétaire Dr. J. H. Schoemaker.

Les séances du Congrès ont été tenues dans deux salles: les conférences générales, les mémoires relatifs aux thèmes 1 à 4 avec leur discussions et la Séance administrative ont eu lieu dans la grande salle, tandis que les deux séminaires et le Symposium se déroulaient dans la salle de séminaire.

Après la clôture du Congrès deux excursions — »A« et »B« — ont été organisées. La première, excursion »A«, comprenait la visite de l'aménagement hydroélectrique »Trebišnjica«, du port maritime de Bar, des aménagements hydroélectriques »Perućica« et »Bistrica«, du barrage »Kokin Brod« et du Laboratoire d'Hydraulique situé au pied du mont Avala, près de Beograd. La seconde, excursion »B«, consistait en visites des aménagements hydroélectriques »Split« et »Peruča«, de l'Institut de l'Hydrodynamique Maritime de Zagreb et du Laboratoire Hydraulique de la Faculté Technique de Ljubljana.

Ces Comptes-rendus contiennent les mémoires selon les thèmes principaux avec leur discussions, conférences générales, rapport généraux sur les abrégés de deux séminaires ainsi que leur registres, et le rapport sur le Symposium.

La publication de ces Comptes-rendus a été possible grâce à la subvention du Conseil Exécutif Fédéral Yougoslav, de l'AIRH, de l'UNESCO et de diverses institutions et entreprises hydrauliques yougaslavies.

Le Comité d'organisation tient à exprimer sa profonde gratitude à tous ceux qui ont contribué au succès de la Neuvième Assemblée Générale de l'AIRH.

INTRODUCTION

The Ninth Convention of the International Association for Hydraulic Research was held from September 4 to 7, 1961, in Dubrovnik (Yugoslavia). The Yugoslav Association for Hydraulic Research, a member of the Yugoslav Union of Engineers and Technicians, was in charge of its organisation. The Congress was attended by 241 participants and 56 ladies from 33 countries. The Program of the Congress was as follows:

A. MAIN SUBJECTS

1. Effect of turbulence on hydraulic structures (27 papers)
2. Mechanics of groundwater flow (37 papers)
3. Hydraulic problems for computers (43 papers)
4. Modifications of natural streams by engineering structures (27 papers)

B. GENERAL LECTURES

1. Hydraulic problems of the Karst
2. Three-dimensional boundary layer flow
3. Energy transformation in the zones of separation

C. SEMINARIES

1. Hydraulics of small structures in irrigation and drainage systems (10 concise communications)
2. Fundamental hydrodynamics of free surface flow and unsteady flow (38 concise communications)

D. SYMPOSIUM

- Hydraulic machinery

E. BUSINESS MEETING

- Reports concerning the activity of the IAHR between the last two congresses and the election of the new executive and administrative boards.

The Ninth Convention was opened by the president of the Organizing Committee, Prof. Bogić Knežević, on September 4th at 10.00 a. m. At the opening session the Congress was addressed and welcomed by the delegate of the Federal Executive Council, Mr. Vinko Hafner and the mayor of the city of Dubrovnik, Mr. Vinko Betica. The introductory speeches were delivered by the president of the IAHR, Dr. Arthur Ippen and the secretary, Dr. H. J. Schoemaker.

The Congress sessions were held in two halls. The general lectures and the papers involving subjects 1 to 4 were presented and discussed in the main hall where the business meeting was also held, while the seminars and the symposium took place in the seminary room.

After the close of the Congress two excursions — »A« and »B« — were organized. The first one, excursion »A«, included visits to the hydroelectric power plant »Trebišnjica«, the seaport of Bar, hydroelectric power plants »Perućica« and »Bistrica«, the barrage »Kokin Brod« and the Laboratory of Hydraulics, situated at the foot of Avala Hill, near Beograd. The second one, excursion »B«, included visits to the hydroelectric power plants »Split« and »Peruča«, the Institute of ship hydrodynamics near Zagreb and the Hydraulic Laboratory in Ljubljana.

This Congress publication contains papers on the main subjects together with their discussions, general lectures, general reports of the chairmen of the two seminars, registers of the concise seminary communications and the report on the symposium.

The publication of the Proceedings of the Ninth Convention was financially supported by the Yugoslav Federal Executive Council, IAHR und UNESCO, as well as by several Yugoslav hydraulic institutes and enterprises.

The Organizing Committee gratefully acknowledges the services of all those who contributed to the success of the Ninth Convention.

Conseil de l'AIRH

Le Conseil pour la période 1er janvier 1962 — 31 décembre 1963 a été élu conformément aux articles 17—21 des Statuts précédents et l'article 15 des Statuts approuvés par l'assemblée général à Dubrovnik au 7 septembre 1961.

Les membres du Conseil élu sont:

Président:	A. T. Ippen	(Etats-Unis)
Vice-présidents:	D. V. Joglekar F. H. Allen L. Escande	(Inde) (Grande-Bretagne) (France)
Secrétaire:	H. J. Schoemaker	(Pays-Bas)
Membres:	R. Boucher J. P. Duport P. Canisius B. V. Proskouriakov M. Hom-ma A. Schlag O. J. Maggiolo Campus	(Canada) (France) (Allemagne) (U.R.S.S.) (Japon) (Belgique) (Uruguay)

Council of AIRH

The Council for the period January 1st, 1962 — December 31st, 1963 has been elected, according to the articles 17—21 of the former Constitution and the article 15 of the Constitution adopted by the general assembly at Dubrovnik on September 7th, 1961.

The members of the elected Council are:

President:	A. T. Ippen	(U.S.A.)
Vice-president:	D. V. Joglekar F. H. Allen L. Escande	(India) (U. K.) (France)
Secretary:	H. J. Schoemaker	(Netherlands)
Members:	R. Boucher J. P. Duport P. Canisius B. V. Proskouriakov M. Hom-ma A. Schlag O. J. Maggiolo Campus	(Canada) (France) (Germany) (U.S.S.R.) (Japan) (Belgium) (Uruguay)

TABLE DE MATIERE — TABLE OF CONTENTS

THEME 1

EFFECTS DE TURBULENCE SUR DES CONSTRUCTIONS HYDRAULIQUES THE EFFECTS OF TURBULENCE ON HYDRAULIC STRUCTURES

N. V. Chandrasekhara Swamy	
TURBULENT FLOW IN OPEN CHANNELS	1
N. S. Govindra Rao	
N. Rajaratnam	
ON THE INCEPTION OF AIR-ENTRAINMENT IN OPEN CHANNEL FLOWS	9
E. Razvan	
L'ETUDE DE L'ECOULEMENT MACROTURBULENT EN AVAL DES EVACUATEURS DES CRUES	13
Rex A. Elder	
MODEL — PROTOTYPE TURBULENCE SCALING	24
T. E. Unny	
THE SPATIAL HYDRAULIC JUMP	32
Jiří Kališ	
DIMINUTION DE LA TURBULENCE DERRIERE LE RESSAUT	43
Petr Hoření	
PRESSURE FLUCTUATIONS IN THE MIXING CHAMBER OF AN EJECTOR	50
K. Haindl, L. Doležal	
TURBULENT PRESSURE FLUCTUATIONS IN A COMPLEX HYDRAULIC STRUCTURE	56
Pavel Novák	
INFLUENCE OF BED LOAD PASSAGE ON SCOUR AND TURBULENCE DOWNSTREAM OF A STILLING BASIN	66
Anton Grzywienski	
THE EFFECT OF TURBULENT FLOW ON MULTI-SECTION VERTICAL LIFT GATES	76

P. S. Eagleson, F. E. Perkins	
A TOTAL HEAD TUBE FOR THE BROAD-BAND MEASUREMENT OF TURBULENT VELOCITY FLUCTUATIONS IN WATER	86
Jean Pantelopoulos	
INFLUENCE DE LA TURBULENCE SUR LA REPARTITION DE LA FORCE TRACTRICE ENTRE LES MATERIAUX D'UN FOND MOBILE	98
J. W. Daily, J. D. Lin, R. S. Broughton	
TURBULENCE AND STATIC PRESSURE IN RELATION TO INCEPTION OF CAVITATION	110
Mikio Hino	
ON THE MECHANISM OF SELF-AERATED FLOW ON STEEP SLOPE CHANNELS. APPLICATIONS OF THE STATISTICAL THEORY OF TURBULENCE	123
J. J. Lévy	
EFFET DYNAMIQUE D'UN COURANT A HAUTE TURBULENCE SUR DES OUVRAGES HYDRAULIQUES ET SUR LE LIT DES RIVIERES	133
S. Angelin; K. Flagestad	
VIBRATION OF ARCHED STOP-LOGS IMMERSED IN STREAMING WATER	141
Harold M. Martin, William E. Wagner	
EXPERIENCE IN TURBULENCE IN HYDRAULIC STRUCTURES	153
Praxitelis A. Argyropoulos	
THE HYDRAULIC JUMP AND THE EFFECT OF TURBULENT ON HYDRAULIC STRUCTURES. CONTRIBUTION TO THE RESEARCH OF THE PHENOMENON	173
O. Györke	
ENERGY DISSIPATION IN PROTECTED BEDS DOWNSTREAM OF RIVER BARRAGES IN THE CASE OF SHALLOW STILLING POOLS	184
I. V. Nagy	
INVESTIGATIONS INTO THE DISTRIBUTION OF SUSPENDED SEDIMENT	197
G. H. Toebe	
HYDROELASTIC FORCES ON HYDRAULIC STRUCTURES DUE TO TURBULENT WAKE FLOWS	205
Jozef Procházka	
THE EFFECT OF TURBULENCE ON CURRENT METER	222
Z. Szigyártó	
EFFECT OF TURBULENCE ON THE CALIBRATION ACCURACY OF HYDRAULIC STRUCTURES	227
Zivko Vladislavljević-Medak	
QUELQUES ASPECTS QUANTITATIFS DU MOUVEMENT TURBULENT	239

J. Čabelka, T. Horsky

- CONTRIBUTION A L'ETUDE DE L'AMORTISSEMENT DE L'ENERGIE
CINETIQUE D'UN COURANT D'EAU SUR LES DEVERSOIRS DE HAUTS
BARRAGES ET DE LA CHARGE DU RADIER 244

F. R. Brown

- FLUCTUATION OF CONTROL GATES 258

R. Curtet, F. Ricou

- INFLUENCE DES CONDITIONS A L'ENTREE DE LA CHAMBRE SUR LES
CARACTERISTIQUES MOYENNES ET DE TURBULENCE D'UN JET DE
REVOLUTION EN PRESENCE D'UNE VITESSE AMBIANTE DANS UNE
CHAMBRE CYLINDRIQUE 270

T H E M E 2

MECANIQUE DES COURANTS D'EAUX SOUTERRAINES

MECHANICS OF GROUNDWATER FLOW

S. D. L. Luthra, D. V. Joglekar

- UPLIFT PRESSURE BELOW HYDRAULIC STRUCTURES ON STRATI-
FIED, PERMEABLE FOUNDATIONS 279

R. O. Bullen

- AN ELECTRICAL ANALOGUE INVESTIGATION OF THE STANDPIPE
FIELD PERMEABILITY TEST 287

J. Zeller

- THE SIGNIFICANCE OF AQUIFER POROSITY IN NON-STEADY SEEPAGE
FLOW WITH FREE SURFACE 299

J. Zaoui

- DETERMINATION DES CARACTERISTIQUES HYDRODYNAMIQUES DES
MILIEUX POREUX 308

A. Preissman, R. Brepson, M. L. Clement

- ECOULEMENT EN MILIEUX POREUX DE PROFONDEUR FINIE SOUS UN
RADIER PROTEGE A L'AMONT ET A L'aval PAR DES ECRANS D'ETAN-
CHEITE-PROCEDE NUMERIQUE DE DETERMINATION DE LA REPRESEN-
TATION CONFORM 317

Selim Yalin, Lehn Franke

- EXPERIMENTAL INVESTIGATION OF THE LAWS OF FILTER FLOW 324

Vitalie Pietraru

- CONTRIBUTIONS A L'ETUDE DES INFILTRATIONS NON PERMANENTES
A NIVEAU LIBRE 332

Harold A. Weggel

- MECHANICS OF GROUND-WATER FLOW THROUGH LAVA BED AREA
ADJACENT TO A RESERVOIR 341

V. I. Aravin	
EXPERIMENTAL STUDIES OF PERCOLATION THROUGH REGIONS INFLUENCED BY RAISING OF GROUND-WATER TABLE DUE TO HYDRAULIC STRUCTURES	350
M. Szalay	
EFFECT OF INCOMPLETE SHEET PILINGS AND IMPERMEABLE AP-RONS ON FILTRATION FLOW UNDER PRESSURE	360
L. Bernell	
NON-STATIONARY GROUNDWATER FLOW THROUGH EMBANKMENTS	364
Aasmund Tveiten	
WATER FLOW THROUGH PEAT	371
G. Öllöös	
INVESTIGATION INTO BOUNDARY CONDITIONS OF SEEPING SYSTEMS AND THEIR SMALLEST FLOW CROSS-SECTION	377
František Slepčík	
THE LAWS OF FILTRATION AND LIMITS OF THEIR VALIDITY	383
František Slepčík	
HYDRAULIC FUNCTION OF A CYLINDRICAL WELL IN AN ARTESIAN AQUIFER WITH REGARD TO NEW RESEARCH ON FLOW THROUGH POROUS MEDIA	395
Václav Zajíček	
APPLICATIO OF THE HYDROLOGICAL METHOD FOR THE EVALUA-TION OF NON-PERMANENT FLOW OF ALLUVIAL GROUND WATER	400
Miroslav Knežek	
DETERMINATION OF THE SEEPAGE CAPACITY OF INFILTRATION RESERVOIRS AT FINITE DEPTH OF AN IMPERMEABLE BASE	408
S. Irmay	
UNSTEADY FLOW THROUGH POROUS MATERIALS	414
L. Šuklje	
FACTEURS GOUVERNANT LES GRADIENTS CRITIQUES DANS LA BASE D'EXCAVATION	428
Giorgio Noseda	
ECOULEMENT D'INFILTRATION A TRAVERS UN BARRAGE EN TERRE SUR ALLUVIONS PERMEABLES	437
Borivoje Mijatović	
SOME CHARACTERISTICS OF THE HYDRAULIC MECHANISM OF THE UNDERGROUND WATERS IN DISSOLUTION FRACTURES AND CHANNELS OF THE CALCAREOUS ROCKS	446

W. C. Bischoff Van Heemskerck	
INVESTIGATION OF EXCESS WATER-PRESSURE UNDER THE ASPHALT FACING OF SAND-CORED DYKES	455
Kâzim Çeçen	
SEEPAGE ONTO THE SLOPES IN ISOTROPIC AND ANISOTROPIC SOILS	468
G. Öllös	
POSSIBILITIES OF MODEL INVESTIGATIONS INTO WATER MOVEMENTS OCCURRING IN FISSURED ROCKS	485
Charles-Sébastien Gerber, Daniel Manry	
ETUDE EXPERIMENTALE DES PHENOMENES SUPERFICIELS EN MILIEU PORREUX	495
Mladen Boreli, B. Batinić	
CONSIDERATION SUR LA LOI NON-LINEAIRE DE FILTRATION REPAR- TITION DE VITESSES DE FILTRATION AU VOISINAGE DU POINT DE SORTIE	506
M. Boreli, D. Jovašević	
CLOGGING OF THE POROUS MEDIA	518
Milan Vuković	
METHODES DE TRAITEMENT DES ECOULEMENTS DANS UN MILIEU STRATIFIE	522
Václav Hálek	
LA SIMULATION DES PROCESSUS NATURELS ET LEUR UTILISATION DANS LA SOLUTION DES REGIMES DES COURANTS D'EAUX SOUTER- RAINES DANS DES REGIONS ETENDUES	529
Vladimirescu I., Lates M.	
RECHERCHES EXPERIMENTALES SUR LA FILTRATION EN REGIME NONPERMANENT, AVEC APPLICATION AUX DIGUES ET BARRAGES EN TERRE	539
Sukejuki Shima	
ON THE SO-CALLED DIFFUSION PHENOMENA OF SEEPAGE FLOW	550
G. Karádi, I. V. Nagy	
INVESTIGATIONS INTO THE VALIDITY OF THE LINEAR SEEPAGE LAW	556
Ján Benetin, Otto Mišút	
DEFORMATION OF THE PERMEABILITY OF ANISOTROPIC SOIL	567
K. Ubell	
VERTICAL-VELOCITY CURVE FOR GROUND-WATER FLOW BY SMALL GRADIENT	574
Boleslaw Kordas	
CONTRIBUTION A L'ETUDE DES PUITS A DRAINS RAYONNANTS	581

Josip A. Grčić

MODEL TEST OF STEADY FLOW TOWARD A WELL

591

J. Riarez, R. Gallea

REMARQUE SUR LES ECOULEMENTS NON PERMANENTS DANS LES SOTS: VIDANGE RAPIDE DE BARRAGE — INJECTION DANS UN SOT NON SATURE

601

T H E M E 3

PROBLEMES HYDRAULIQUES POUR LES MACHINES A CALCULER
HYDRAULIC PROBLEMS FOR COMPUTORS

Armando Balloffet, Arnold Kupferman

SURGES DUE TO PARTIAL BLOCKAGE OF A TAILRACE TUNNEL 613

R. M. Advani

IMPORTANCE OF ELECTRONIC COMPUTERS AND SIMILAR OTHER
DEVICES IN THE FIELD OF HYDRAULIC ENGINEERING

622

N. J. Kendall

ANALISYS OF PIPE NETWORKS BY ELECTRONIC DIGITAL COMPUTERS 626

R. Sabljak, W. H. Doran

HYDRAULIC ANALYSIS OF A SURGE SHAFT SYSTEM BY DIGITAL
COMPUTER 639

A. Preissmann, J. Cunge

CALCUL DES INTUMESCENCES SUR MACHINES ELECTRONIQUES 656

M. Normand

L'ELECTRONIQUE AU SERVICE DE L'HYDROLOGIE 665

E. Biro

ETUDE DU COUP DE BELIER DANS DES CONDUITES A CARACTERI-
STIQUES MULTIPLES. 673

M. F. Gohin

ETUDE DES DENIVELATIONS ET DES COURANTS DUS A LA MAREE
EMPLOI DE MACHINES A CALCULER 680

F. Biesel, B. Ranson

CALCULS DE DIFFRACTION DE LA HOULE 688

J. Zaoui

QUELQUES APPLICATONS DES ORDINATEURS AUX PROBLEMES
D'ECOULEMENTS SOUTERRAINS 700

B. Ranson

CALCUL DES ECOULEMENTS IRROTATIONNELS A SYMETRIE
CILINDRIQUE 707

George Bugliarello	
TOWARD A COMPUTER LANGUAGE FOR HYDRAULIC ENGINEERING	714
J. E. Nash	
A LINEAR TRANSFORMATION OF A DISCHARGE RECORD	730
G. N. Gvazava	
APPLICATION OF THE ELECTRONIC ANALOG COMPUTER FOR CALCULATION OF UNSTEADY FLOW IN CONDUITS AND SURGE TANKS OF HYDROELECTRIC PLANTS	732
Taizo Hayashi	
WATER-HAMMER IN BIFURCATING PIPE-LINES	740
Tojiro Ishihara, Yasuo Ishihara	
RUNOFF ANALYSIS BY ANALOG COMPUTER	749
C. W. Thomas, P. F. Enger	
USE OF AN ELECTRONIC COMPUTER TO ANALYZE DATA FROM STUDIES OF CRITICAL TRACTIVE FORCES FOR COHESIVE SOILS	760
J. Van Den Berg	
CALCULATION OF RUN OFF FROM RAINFALL FIGURES	772
G. Pistilli, G. Savastano	
THE STUDY OF LEVEL'S OSCILLATIONS IN CYLINDRICAL SURGE TANKS WITH THE DIGITAL DIFFERENTIAL ANALIZER OF THE UNIVERSITY OF NAPLES	775
P. Canisius, F. K. Rubbert	
THE APPLICATION OF ELECTRONIC COMPUTERS TO THE PREDICTIVE CALCULATION OF RIVER TIDES	790
C. Thirriot	
ETUDE DES INTUMESCENCES EN VALEURS ADMENSIONNELLES	793
C. Thirriot	
ETUDE THEORIQUE DES PHENOMENES PNEUMATIQUES DANS UNE GALERIE DE FUITE D'USINE SOUTERRAINE	803
Jean Piquemal	
APPLICATION DE L'ANALOGIE A L'ETUDE DES SURPRESSION DANS LES CONDUITES FORCES A CARACTERISTIQUES MULTIPLES	813
M. T. Guyot, J. Nougaro, Cl. Thirriot	
ETUDE NUMERIQUE DES REGIMES TRANSITOIRES DANS LES CANAUX	820
R. Bonnefille, F. Voyer	
CALCUL DE LA PROPAGATION DE LA MAREE DANS UNE ZONE COTIERE	832

J. Faure, N. Nahas	
DEUX PROBLEMES DE MOUVEMENTS NON PERMANENTS A SURFACE LIBRE RESOLUT SUR ORDINATEURS ELECTRONIQUES	854
R. P. Sijbesma, M. de Vries	
COMPUTATIONS OF BOUNDARY CONDITIONS OF A RIVER MODEL WITH MOVABLE BED	870
M. de Vries	
COMPUTATIONS ON GRAIN — SORTING IN RIVERS AND RIVER MODELS	876
Guy Thibessard	
LA SIMULATION DU COUP DE BELIER SUR CALCULATEUR NUMERIQUE	881
M. F. Biesel	
OPTIMISATION DE LA RECETTE D'UNE USINE MAREMOTRICE	891
M. F. Biesel, M. P. Arnaud	
RECHERCHE DE LA REPARTITION ECONOMIQUE DES DIAMETRES DANS UN RESEAU DE DISTRIBUTION RAMIFIE	899
G. Ransford, B. Ranson	
FREQUENCY REGULATION BY A HYDROELECTRIC PLANT SUPPLIED FROM A FREE-SURFACE CHANNEL	906
M. Bouvard, J. Zaoui	
LA DETERMINATION DU MOUVEMENT DES MATERIAUX EN ECOULEMENT TURBULENT (SUSPENSION ET DECANTATION) SUR MACHINES ELECTRONIQUES	913
J. Murillo	
APPLICATION D'UN ORDINATEUR A UN PROBLEME DE CHAMBRE D'EQUILIBRE	926
H. Van Wijngaarden, R. P. Sijbesma	
COMPUTATIONS OF WATER LEVELS AT HIGH DISCHARGES ALONG THE MAIN DIKES OF THE RIVER RHINE AND ITS BRANCHES IN THE NETHERLANDS	931
Romolo Pasquali, Giorgio Rossi	
RESOLUTION DE PROBLEMES HYDROLOGIQUES PAR LE CALCULATEUR ELECTRONIQUE	947
Hans Mogens Jensen	
STATEMENT OF SOME METHODS FOR CALCULATION OF HEAD LOSSES AT CHANNELS, BACKWATERS AND CANALS USED AT THE SWEDISH STATE BOARD	956
L. Borel	
ETUDE GENERALE DE L'ECOULEMENT DE L'EAU EN REGIME VARIABLE DANS UNE CONDUITE DE SECTION VARIABLE	965

L. Bonny	
DETERMINATION PRATIQUE DES PARAMETRES HYDRAULIQUES FONDAMENTAUX D'UNE TURBINE	979
E. O. Macagno, Matilde Macango	
PRESSURE WAVE ANALYSIS FOR VARIABLE LENGTH OF A FLUID COLUMN	993
Torben Sørensen, Ian Larsen	
HYDRAULIC CALCULATION OF STORM FLOOD LEVELS IN CONNECTED SHALLOW BASIN WITH SPECIAL REFERENCE TO THE LIMFJORD, DENMARK	1003
Geza L. Bata, Petar B. Madich	
SOLUTION FOR MULTIPLE SURGE-TANK SYSTEMS WORKED OUT ON REPETITIVE DIFFERENTIAL ANALYZER	1011
D. Rose	
THE INFLUENCE OF THE CLOSED SEA-ARMS ON THE WATER LEVEL AND CURRENT BEFORE THE COAST OF THE NETHERLANDS AND IN THE NEW WATERWAY	1024
 T H E M E 4	
MODIFICATIONS DE COURANTS NATURELS CAUSES PAR DES OUVRAGES	
MODIFICATIONS OF NATURAL STREAMS BY ENGINEERING STRUCTURES	
Z. Hankó	
INVESTIGATIONS TO DETERMINE THE NECESSARY LENGTH OF THE LINING FOLLOWING THE STILLING BASIN OF THE BOTTOM DROPS ON SMALL WATER COURSES	1029
L. Muszkalay	
EFFECT OF PUMPING PLANT ON THE FLOW CONDITIONS OF THE RIVER	1043
A. H. Blysowski	
MODIFICATION OF NATURAL STREAMS BY ENGINEERING STRUCTURES	1051
W. Kresser	
INFLUENCE D'INJECTION DE LIQUIDES SUR LE COURANT D'EAU AUTOOUR D'UNE PILE	1055
Enzo Levi, Humberto Luna	
DISPOSITIFS POUR REDUIRE L'AFFOUILLEMENT AU PIED DES PILES DE PONTS	1061
D. R. P. Farleigh	
CHANNEL — MOVEMENTS RESULTING FROM CONSTRUCTION OF NEW BRIDGE ABUTMENTS AT CONWAY, N. WALES	1070

Al. Maruta	
L'EFFET DES RETENUES A SEUIL SUR LES MODIFICATIONS DES LITS DES RIVIERES	1080
S. Hincu, I. Lupu	
SUR LA SIMILITUDE DES AFFOUILLEMENTS LOCAUX DANS LA ZONE DES CONSTRUCTIONS HYDROTECHNIQUES	1087
O. J. Maggiolo	
ETUDE SUR LE MODELE REDUIT DE L'EROSION DU LIT ROCHEUX EN aval du deversoir du barrage de „RINCON DEL BONETE“ — (URUGUAY)	1094
A. K. Ananian	
DETERMINATION DE LA FORMATION DU LIT RIVIERES, CREE PAR SUITE DE L'ABAISSEMENT DE LA COTE LEURS BASES D'EROSION	1102
S. V. Isbash, I. V. Lebedev	
CHANGE OF NATURAL STREAMS DURING CONSTRUCTION OF HIDRAU- LIC STRUCTURES	1114
T. Horsky	
L'AMORTISSEMENT DE L'ENERGIE MECHANIQUE PAR COLLISION DES LAMES DEVERSANTES	1122
Jean Pantelopoulos	
QUELQUES RESULTATS EXPERIMENTAUX SUR L'ENGRAVEMENT ET LES POSSIBILITES DE DEGRAVEMENT D'UNE RETENUE FORMEE PAR UN BARRAGE EN LIT DE RIVIERE	1128
Jaroslav Martinec, Jaroslav Urban	
FLOW CONDITIONS ABOVE A HIGH DAM	1134
Walenty Jarocki	
EFFECTS OF PIERS ON WATER STREAMS AND BED FROM	1147
J. Valembois	
ESTIMATION DE LA DISTANCE DE REMONTEE DU REMOUS D'UN OBSTACLE DANS UNE RIVIERE EN CRUE	1153
C. J. Posey, J. H. Sybert	
EROSION PROTECTION OF PRODUCTION STRUCTURES	1157
J. S. Burgess	
SCOUR DOWNSTREAM OF A COMPOUND MEASURING WEIR	1163
A. De Leeuw	
MODIFICATIONS OF NATURAL WATERCOURSES BY ENGINEERING STRUCTURES IN DESERT OF SOUTHERN ISRAEL	1172
Mushtaq Ahmad, Abid Ali	
EFFECT OF BARRAGES ON THE REGIME OF RIVERS OF INDUS BASIN	1177

L. Ivicsics		
SCALE MODEL INVESTIGATION OF SEDIMENTATION OVER REACHES LYING UPSTREAM OF BARRAGES	1195	
L. Escande, J. Nougaro, L. Castex, H. Barthet		
INFLUENCE DE QUELQUES PARAMETRES SUR UNE ONDE DE CRUE SUBITE A L'aval D'UN BARRAGE	1198	
Mihailo Vojinović		
MODIFICATIONS DES COURANTS D'EAU CAUSEES PAR DES PRISES D'EAU SANS BARRAGES	1207	
J. Chabert, M. Remilieux, I. Spitz		
APPLICATION DE LA CIRCULATION TRANSVERSALE A LA CORRECTION DES RIVIERS ET A LA PROTECTION DES PRISES D'EAU	1216	
Slavoljub Jovanović		
ADAPTATION DE L'OUVRAGE DE SEPARATION POUR LA PROTECTION DES RETENUES CONTRE ENSABLEMENT	1224	
Isao Akikusa, Hideo Kikkawa		
HYDRAULIC BEHAVIOR OF THE GROINS IN THE STREAMS	1234	
CONFERENCES GENERALES		
GENERAL LECTURES		
Bogić Knežević		
LES PROBLEMES HYDRAULIQUES DU KARST	1247	
H. Schlichting		
THREE-DIMENSIONAL BOUNDARY LAYER FLOW	1262	
Hunter Rouse		
ENERGY TRANSFORMATION IN ZONES OF SEPARATION	1291	
SEMINAIRE „A“ — SEMINAR „A“		
SEMINAIRE „B“ — SEMINAR „B“		
Živko Vladisavljević-Medak		
HYDRAULIQUE DE PETITES CONSTRUCTIONS DANS L'IRRIGATION ET LE DRAINAGE	1305	
John McNown		
FUNDAMENTAL HYDRODYNAMICS OF FREE-SURFACE FLOW AND OF UNSTEADY FLOW	1314	
J. V. Daily		
SIMPOSIUM ON HYDRAULIC MACHINERY	1318	
LISTE DES AUTEURS — LIST OF AUTHORS	1320	
LISTE DES PARTICIPANTS — LIST OF PARTICIPANTS	1332	

TURBULENT FLOW IN OPEN CHANNELS

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The velocity distribution in open channels has been analytically studied by dividing the flow region into three zones — (i) the upper zone where the eddy viscosity due to turbulence is predominant, (ii) the intermediate zone where the eddy and the kinematic viscosities are of the same order, (iii) the lower zone where the eddy viscosity is negligible and only the kinematic viscosity and wall shear are the controlling factors. Series solutions have been derived for the first two zones and are found to agree with the Prandtl Universal Logarithmic distribution as well as experiment. The lower zone corresponds to the well-defined region of the turbulent boundary layer. Approximate limits have been indicated for the extent of the three zones.

Distribution des vitesses en canaux ouverts est analytiquement étudiée par la division de la région de l'écoulement en trois zones:

(1) zone supérieure où la viscosité du tourbillon due à la turbulence est prédominante;

(2) zone intermédiaire où la viscosité cinétique et celle du tourbillon sont du même ordre;

(3) zone inférieure où la viscosité du tourbillon étant négligeable, la viscosité cinétique et la traction à la paroi sont les seuls facteurs de contrôle.

Une suite de solutions en dérivent pour les deux premières zones, s'accordant avec la Distribution logarithmique universelle de Prandtl tout aussi bien qu'avec les expériences. La zone inférieure correspond à la zone bien définie de la couche limite turbulente. Des limites approximatives sont indiquées pour l'extension des trois zones.

INTRODUCTION

The application of the theories of turbulence to problems in hydraulics has been instrumental in solving many as yet unsolved problems in hydraulics. Hydraulics has till now been an empirical science, lacking in the conciseness and richness of the more logical sciences. Most problems of everyday occurrence in hydraulics have been studied only empirically without any analytical background. This has led to several controversies which could easily be averted if the subject is studied from a more rational point of view.

One such controversy in the field of hydraulics is the extent of a hydraulic jump. It is known that a hydraulic jump gets formed when a supercritical flow encounters a sub-critical flow. But what exactly is the extent of this jump has been a disputable point. Innumerable empirical formulae are available

and are being proposed periodically which all the more confuses the practical designer. The reason for this state of affairs is that our knowledge of the phenomena occurring inside a hydraulic jump is negligible. Rouse, Siao and Nagarathnam [1] have made certain turbulence measurements in the hydraulic jump. On the basis of this work, the author has given an expression for the extent of a hydraulic jump [2], which has agreed well with experiments. This was made possible by incorporating certain basic ideas regarding turbulent flow into the mathematics of the hydraulic jump.

Another interesting but as yet unexplored field of research in hydraulics is the velocity distribution in an open channel. Even though a large amount of work has been done on the resistance to flow in open channels for smooth or rough conditions, it is surprising that very little attention seems to have been paid

The fundamental problem of velocity distribution in open channels. The universal logarithmic velocity distribution of Prandtl and von Karman based on the momentum transfer theory has been modified by Vanoni [3] for the case of an open channel in the form

$$u = V + \frac{1}{K} \sqrt{gys} \left(1 + 2.3 \log_{10} \frac{y'}{y} \right) \quad (1)$$

where u is the velocity at any height y' from the bed, y the depth of flow in the channel, V the mean velocity for the entire section of flow and K is von Karman's constant having a value of 0.40. The agreement between the experimental values and equation (1) was found to be very close except near the bed where the logarithmic law fails. But this is not a rational analysis of the problem.

The present author [4] attempted to solve this problem of open channel flow by resorting to the fundamental Navier-Stokes equations of motion and simplifying them to a certain extent by making the usual assumptions of turbulent shear flow. The problem was attacked in two ways — (i) by considering the entire depth of flow to be governed by a single law, (ii) the flow region being divided into two regions, the upper portion with predominant eddy viscosity and the lower one with predominant kinematic viscosity. Even though the velocity distributions obtained agreed fairly well with experiment and the universal logarithmic velocity distributions, the analysis contained some serious short-comings. The fundamental aspect of turbulence is momentum transfer which was not taken into considerations in the previous work.

In this paper, the problem has been attacked by an entirely different method by dividing the channel into three distinct regions. It is a well established fact that turbulent flow gives rise to an eddy viscosity which is not an intrinsic property of the fluid like the kinematic viscosity. Also, the eddy viscosity is not constant like the kinematic viscosity for any fluid at any given temperature, but happens to vary widely over the flow field. Inspite of these complications, the eddy viscosity is a useful concept which has been often used in studies on turbulence.

In the case of an open channel, the eddy viscosity and the kinematic viscosity play important roles in any region depending upon the location of that region with respect to the boundary. Very near the boundary, the eddy viscosity is small and we can consider

only the kinematic viscosity. On the other hand, near the free surface, the eddy viscosity is much more predominant. In between, there is a region where both the viscosities are of the same order. On this basis, we divide the region of flow in an open channel into three distinct parts:

- (1) Region of high viscosity near the bed (Lower region).
- (2) Region of low viscosity near the free surface (upper region).
- (3) Region where the kinematic and eddy viscosities are of the same order (intermediate region).

It is the object of this paper to study these three regions separately by using the fundamental equations of motion.

EQUATIONS OF MOTION

We assume that the Navier-Stokes equation holds good for both the mean — and turbulent — velocity components. We also assume the fluid to be incompressible. To eliminate density from the equation, kinematic quantities are used (5).

The Navier-Stokes equations are given in the tensorial form by

$$\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} = - \frac{\partial p}{\partial x_i} + \nu \nabla^2 u_i \quad (2)$$

where repeated indices denote summation from 1 to 3. Both the indices i and j range from 1 to 3. The velocities u_i and u_j and the pressure p can be considered to be made up of the mean and the turbulent components. Let

$$u_i = U_i + u'_i \quad (3a, b, c)$$

and

$$p = P + p'$$

where U_i , U_j and P are the mean components, and u'_i , u'_j and p' are the turbulent components. Substituting this in equation (2), we have

$$\begin{aligned} & \frac{\partial}{\partial t} (U_i + u'_i) + (U_j + u'_j) \frac{\partial}{\partial x_j} (U_i + u'_i) \\ &= - \frac{\partial}{\partial x_i} (P + p') + \nu \nabla^2 (U_i + u'_i) \end{aligned} \quad (4)$$