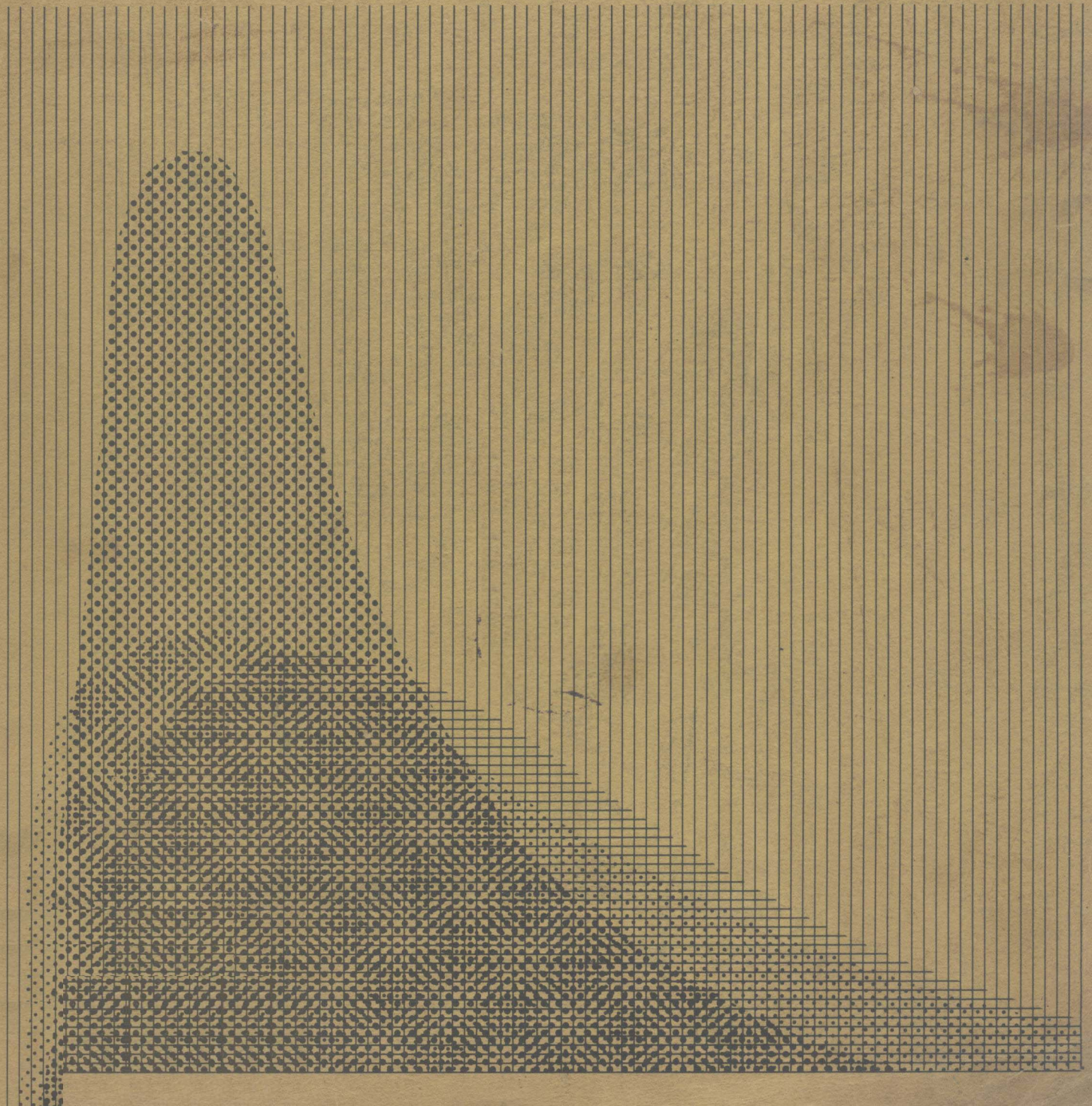


# **Polymer Reactor Engineering**





## POLYMER REACTOR ENGINEERING

A symposium sponsored jointly by the Macromolecular  
Sciences Division of the Chemical Institute of Canada  
and the Canadian Society for Chemical Engineering at  
the 55th Chemical Conference and Exhibition of the  
Chemical Institute of Canada, Quebec City, Quebec,  
June 4 - 7, 1972

SYMPOSIUM ON  
POLYMER REACTOR ENGINEERING

Laval University, Quebec City

Monday, June 5, 1972

PROGRAMME:

Morning Session

- A. POLYMERIZATION KINETICS - Chairman : K. F. O'Driscoll  
University of Waterloo
- 9.00 Mathematical Modelling Techniques : W. H. Ray  
State University of New York  
at Buffalo
- 9.30 Branch Formation During Polymerization : W. W. Graessley  
Northwestern University
- 10.00 Copolymerization : K. F. O'Driscoll  
University of Waterloo
- 10.30 Mechanism of Emulsion Polymerization : J. L. Gardon  
M. & T Chemicals Inc.  
Rahway, N.J.
- 11.00 Gel Effect in Vinyl Polymerization : A. E. Hamielec  
McMaster University

Afternoon Session

- B. REACTOR DESIGN, SIMULATION AND OPTIMIZATION -  
Chairman : A. E. Hamielec  
McMaster University
- 1.30 Mixing in Polymer Reactors : E. B. Nauman  
Union Carbide Corp.  
Bound Brook, N.J.
- 2.00 Polymerization in Tubular Reactors : J. A. Biesenberger  
Stevens Institute  
Hoboken, N.J.
- 2.30 Continuous Emulsion Polymerization : G. W. Poehlein  
Lehigh University
- 3.00 Design of Polymer Reactors : B. Brasie,  
Dow Chemical Co.  
Midland, Michigan
- 3.30 Optimization of Polymer Reactors : C. M. Crowe  
McMaster University

## "Mathematical Modelling Techniques"

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Department of Chemical Engineering  
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## Chapter 1 Introduction

As commercially produced polymers become more of a commodity product, rather than a speciality product, there is a growing need for a more detailed understanding of the phenomena taking place in the polymer reactor. One quantitative form of this process understanding is the mathematical model, which can represent the detailed behaviour of a polymer reactor. The mathematical model is an invaluable tool for developing the optimal design and optimal control system for these reactors.

Because polymerization reactions are usually very complex in nature, a reasonable amount of mathematical sophistication is required for detailed modelling. This paper will be devoted to reviewing some of the mathematical techniques which prove useful in constructing these models.

The second chapter deals with methods of producing the molecular weight distribution (MWD) of both homopolymer and copolymer systems by analysis of the kinetic mechanism. The third chapter discusses the less detailed characterization of the polymer available through MWD moments, and develops straightforward methods for deriving the moment equations. Chapter four considers the prediction of copolymer composition distributions and chain sequence distributions from the kinetic scheme. A number of practical examples are given in Chapter five in order to emphasize to the reader that all of these mathematical manipulations are in fact practical. Finally, a number of more complicated polymerization reactor systems - some of which require further work to produce an adequate model are discussed.



## Chapter 2 Techniques for the Calculation of Differential Molecular Weight Distributions

### 2.1 Differential Distributions

The distribution of molecular weights in a polymeric material may be represented as a density function or "differential" distribution. For example, the concentration of polymer of chain length  $n$ ,  $P_n$  is shown as a discrete differential distribution in Figure 2-1. Although there are no values of  $P_n$  except for integer values of  $n$ , a smooth curve results from the numerous points on the graph. Thus we shall use a continuous graph to represent the differential distributions in this paper.

There are a number of differential distributions which fall under the generic title "molecular weight distributions". The plot of  $P_n$  vs  $n$  shown in Figure 2-1 is more precisely the "number chain length distribution" (NCLD), because it represents the chain length distribution with respect to the number of molecules (per unit volume). Similarly, the "weight chain length distribution" (WCLD), shown in Figure 2-2, represents the chain length distribution with respect to the weight of molecules (per unit volume),  $nwP_n$ . There is also a "number molecular weight distribution" (NMWD), shown in Figure 2-3, in which the number of molecules/unit volume,  $P_n$ , is given as a function of molecular weight. Finally, the "weight molecular weight distribution" (WMWD) is shown in Figure 2-4.

These distributions become rather more complicated for copolymerization systems where there are two or more chain lengths



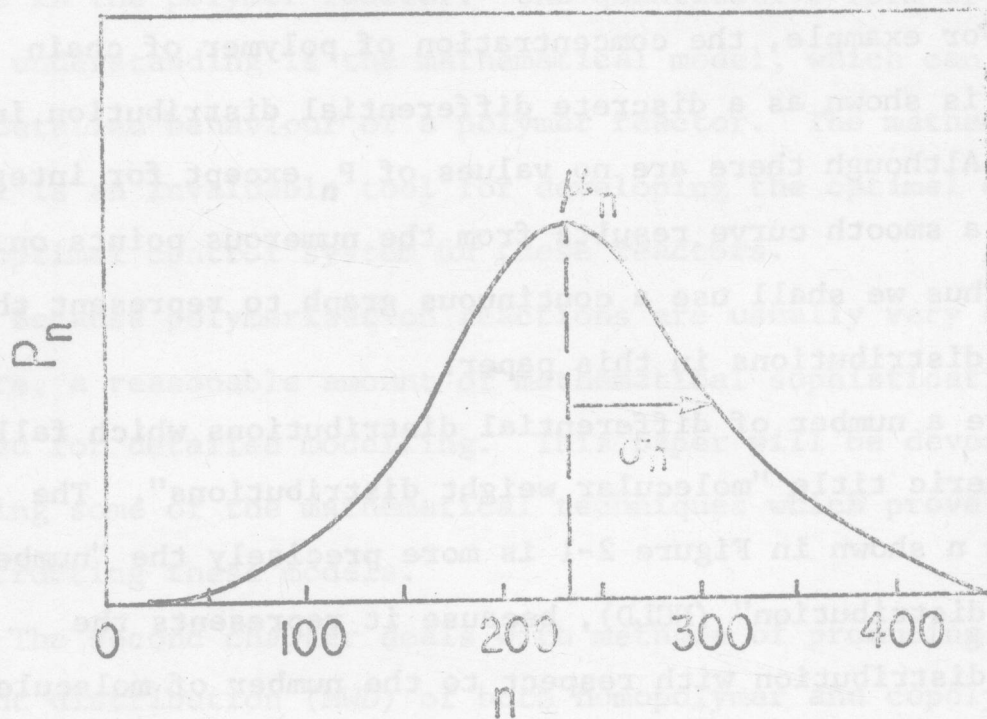


Figure 2.1 The number chain length distribution (NCLD)

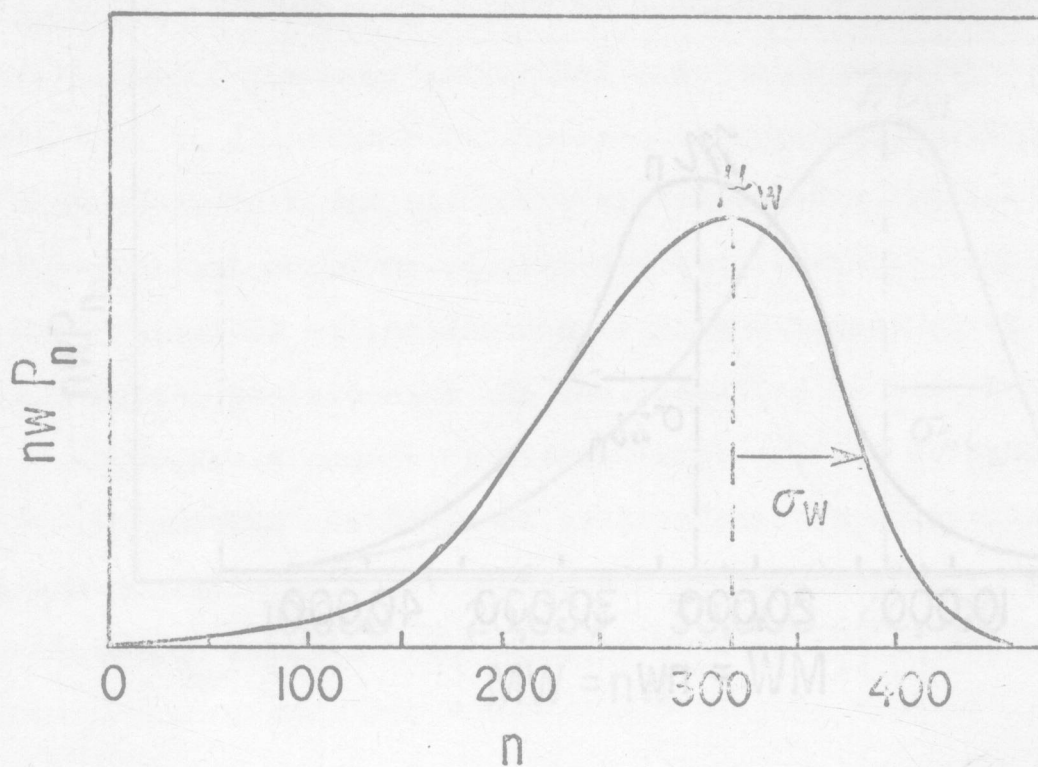


Figure 2.2 The weight chain length distribution (WCLD)



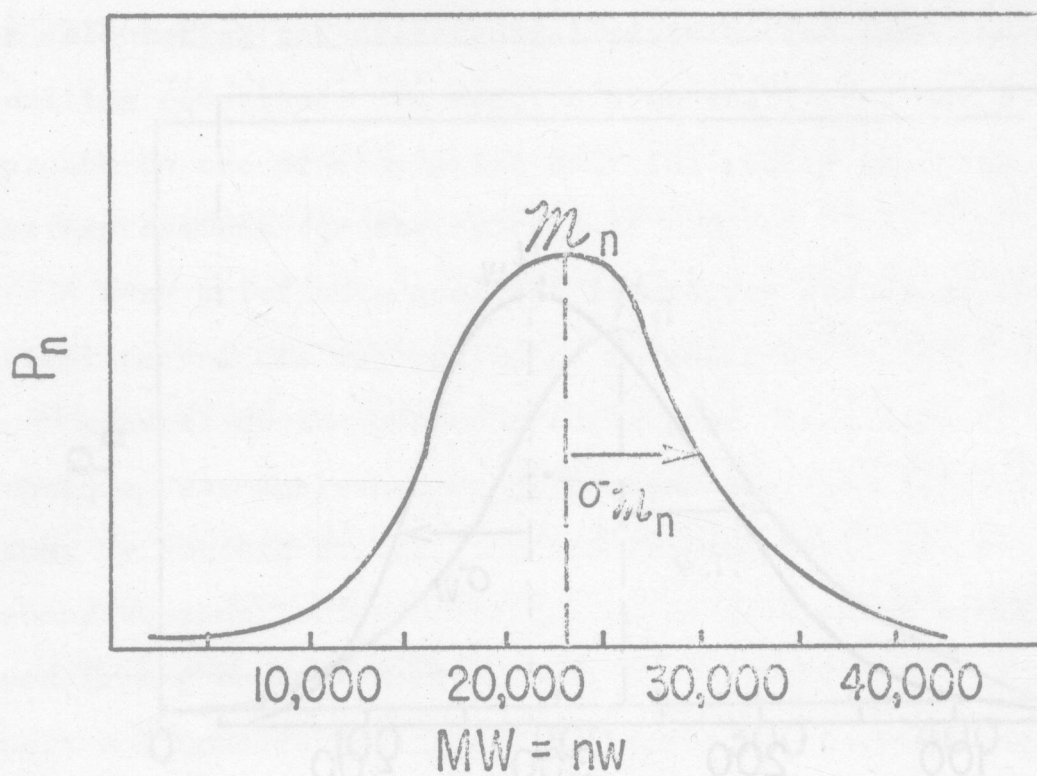


Figure 2.1 The number chain length distribution (NCLD)

Figure 2.2 The weight chain length distribution (WCLD)

Figure 2.3 The number molecular weight distribution (NMWD)

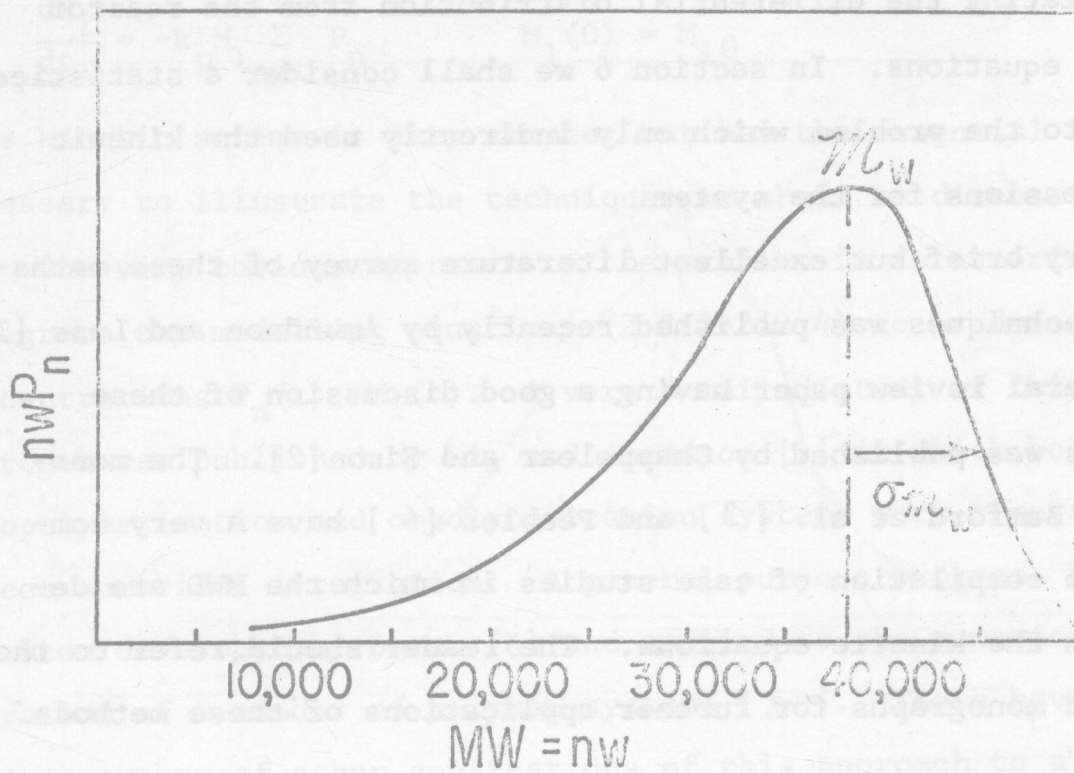


Figure 2.4 The weight molecular weight distribution (WMWD)



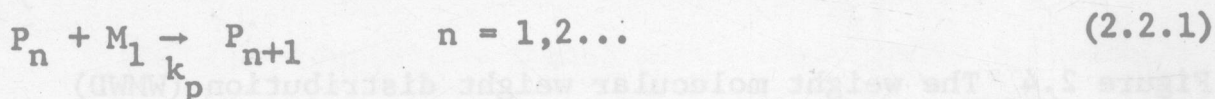
and molecular weights of interest. These systems will be discussed in more detail in section 7 of this chapter.

The next few sections will deal with a number of techniques for calculating the differential distribution from the reactor modelling equations. In section 6 we shall consider a statistical approach to the problem which only indirectly used the kinetic rate expressions for the system.

A very brief but excellent literature survey of these mathematical techniques was published recently by Amundson and Luss [1]. A more general review paper having a good discussion of these techniques was published by Chappellear and Simon [2]. The monographs by Bamford et al. [3] and Peebles [4] have a very comprehensive compilation of case studies in which the MWD are derived from the kinetic equations. The reader should refer to these papers and monographs for further applications of these methods.

## 2.2 Numerical Integration

Let us consider the very simple mechanism which might arise in anionic polymerization with very rapid initiation.



where  $P_n$  represents the growing polymer chain and  $M_1$  is the monomer. The polymer material balances for a batch reactor yield the equations

$$\frac{dP_1}{dt} = -k_p M_1 P_1 \quad P_1(0) = P_{10} \quad (2.2.2)$$

$$\frac{dP_n}{dt} = -k_p M_1 (P_n - P_{n-1}) \quad P_n(0) = 0 \quad (2.2.3)$$

with the additional monomer balance

$$\frac{dM_1}{dt} = -k_p M_1 \sum_{n=1}^{\infty} P_n \quad M_1(0) = M_{10} \quad (2.2.4)$$

This kinetic scheme is very simple, but has the essential features necessary to illustrate the techniques we shall be discussing.

One very obvious approach to the problem is to numerically integrate the modelling equations (2.2.2-2.2.4) to produce the concentrations  $P_n(t)$ ,  $M_1(t)$ . A very detailed study of this approach was published by Liu and Amundson [5] in which both homopolymerization and copolymerization systems were simulated by direct numerical integration. A general purpose program, REMECH, has been developed by Detar [6] and applied to the numerical integration of a number of polymer systems [7-8]. There have been a large number of other applications of this approach to a wide variety of polymer systems (eg; 9-11).

A simplification arises when Eq'ns 2.2.2-2.2.3 are summed to produce

$$\frac{dP}{dt} = 0 \quad (2.2.5)$$

where  $P = \sum_{n=1}^{\infty} P_n$ . Thus for this problem  $P = P_{10}$  at all times. The fact that  $P$  can be determined independently means that Eqn's (2.2.2-2.2.3) can now be solved sequentially rather than requiring simultaneous solution. This type of simplification can be applied to most polymerization systems and has been overlooked in a number of the papers cited above.



Another transformation which is useful is the stretching of the time variable by the relation

$$\tau = \int_0^t k_p M_1 dt \quad (2.2.6)$$

This reduces 2.2.2-2.2.3 to

$$\frac{dP_1}{d\tau} = -P_1 \quad P_1(0) = P_{10} \quad (2.2.7)$$

$$\frac{dP_n}{d\tau} = -(P_n - P_{n-1}) \quad P_n(0) = 0 \quad n \geq 0 \quad (2.2.8)$$

which can be solved in terms of the stretched variable  $\tau$ . The influence of monomer changes, temperature variations, etc. only appear in the relationship (2.2.6) between  $\tau$  and batch time,  $t$ .

One could now solve Eq'ns (2.2.7,2.2.8) sequentially for  $n$  as large as desired. A detailed example of this approach will be given in Chapter 5.

### 2.3. Generating Functions

An approach which has wide use in polymer kinetics and which can be used to produce the differential MWD is the generating function technique. Scanlan [12] appears to be the first to suggest it's use in polymer systems. Bamford and Jenkins [13] and Liu and Amundson [14] give rather good discussions of its application to polymerization.

Let us consider the system (2.2.7,2.2.8) written in terms of  $t$  (we suppress the tau for the moment).

$$\frac{dP_1}{dt} = -P_1 \quad P_1(0) = P_{10} \quad (2.3.1)$$

$$\frac{dP_n}{dt} = -P_n + P_{n-1} \quad P_n(0) = 0 \quad n \geq 2 \quad (2.3.2)$$

The generating function for this system is defined as

$$G(s,t) = \sum_{n=1}^{\infty} s^n P_n(t) \quad (2.3.3)$$

The equations for  $G(s,t)$  in the batch reactor for the simple system (2.3.1-2) can be gotten by multiplying each equation by  $s^n$  and summing over  $n$  to yield

$$\frac{dG(s,t)}{dt} = (s-1) G(s,t) ; \quad G(s,0) = sP_{10} \quad (2.3.4)$$

This can be immediately solved to yield

$$G(s,t) = \exp(-t) sP_{10} \exp(st) \quad (2.3.5)$$

which when expanded in a power series in  $s$  gives

$$G(s,t) = P_{10} \exp(-t) \sum_{n=1}^{\infty} \frac{(t)^{n-1}}{(n-1)!} s^n \quad (2.3.6)$$

by comparison of this with the definition (2.3.3) one gets

$$P_n(t) = P_{10} \exp(-t) \frac{(t)^{n-1}}{(n-1)!} ; \quad n \geq 1 \quad (2.3.7)$$

It is not always necessary to expand  $G(s,t)$  in a power series to get the solution  $P_n(t)$  because a table of generating functions and their inverses can be found in Erdelyi [15].

A number of recent papers have used generating functions to generate the differential distribution [eg. 16-17]. Some further applications of this technique will be discussed later in this paper.



## 2.4. Z Transforms

A technique which is nearly identical to the generating function technique involves the use of Z transforms [18] which are defined as

$$F(z) = \sum_{n=0}^{\infty} P_n z^{-n} \quad (2.4.1)$$

and which can be applied in the same way as the generating function. If we consider again the simple example (2.3.1-2), then by taking the Z-transform one obtains

$$\frac{dF(z,t)}{dt} = \left(\frac{1}{z} - 1\right) F(z,t) ; \quad F(z,0) = \frac{P_{10}}{z} \quad (2.4.2)$$

whose solution is

$$F(z,t) = \frac{P_{10}}{z} \exp(-t) \exp\left(\frac{t}{z}\right) \quad (2.4.3)$$

expanding into a power series in  $1/z$

$$F(z,t) = P_{10} \exp(-t) \sum_{n=1}^{\infty} \frac{(t)^{n-1}}{(n-1)!} z^{-n} \quad (2.4.4)$$

and comparing coefficients, one obtains the differential distribution

$$P_n(t) = P_{10} \exp(-t) \frac{(t)^{n-1}}{(n-1)!} ; \quad n \geq 1 \quad (2.4.5)$$

One possible advantage of Z-transforms over the generating function is the existence of more extensive tables of the Z-transform and inverses [18]. Abraham [19-20] and Kilkson [21-22] have applied this method to a number of practical problems. The most interesting recent application of this method was reported by Chen and Spencer [23]. Their work shows that it is possible to extract numerical