# 南京航空航天大等



(二〇〇九年) 第30册

材料科学与技术学院(第2条系)

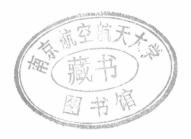
南京航空航天大学科技部编 二〇一〇年五月

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# 材料科学与技术学院



## 材料科学与技术学院

061 系

062 系

063 系

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序号	姓名	职称	单位	论文题目	刊物.会议名称	年、卷、期	类别
79	钟 杰	硕士	061	Fabrication of functionally graded Ti(C,	Int. Journal of	2009.27.3	
	郑勇	教授	061	N)-based cermets by double-glow plasma	Refractory		
	袁 泉	硕士	061	carburization	Metals & Hard		
	张一欣	硕士	061		Materials		
	余立新	高工	外单位				
80	袁 泉	硕士	061	Synthesis of nanocrystalline Ti(C,N)	Int. Journal of	2009.27.1	
	郑勇	教授	061	powders by mechanical alloying and	Refractory		
	于海军	硕士	061	influence of alloying elements on the	Metals & Hard		
				reaction	Materials		
81	袁 泉	硕士	061	Mechanism of synthesizing	Int. Journal of	2009.27.4	
	郑勇	教授	061	nanocrystalline TiC in different milling	Refractory		
	于海军	硕士	061	atmospheres	Metals & Hard		
					Materials		
82	庞旭明	硕士	061	Effect of Mn on valence -electron	Int. Journal of	2009.27.4	
	郑勇	教授	061	structure and properties of hard phase in	Refractory		
	王少刚	副教授	061	Mo2FeB2-based cermets	Metals & Hard		
	王秋红	硕士	061		Materials		
83	张一欣	硕士	061	Effect of carbon content and cooling	Int. Journal of	2009.27.6	
	郑勇	教授	061	mode on the microstructure and	Refractory		
	钟 杰	硕士	061	properties of Ti(C,N)-based cermets	Metals & Hard		
	袁 泉	硕士	061		Materials		
	吴 鹏	硕士	061				
84	郑建智	硕士	061	烧结工艺和碳加入量对 Mo <sub>2</sub> FeB <sub>2</sub> 基金	机械工程材料	2009.33.3	
	承 新	硕士	061	属陶瓷显微组织和性能的影响			
	郑勇	教授	061				
	严永林	硕士	061				
	赵能伟	硕士	061				
85	郑建智	硕士	061	Mo <sub>2</sub> FeB <sub>2</sub> 基金属陶瓷烧结过程中显微	硬质合金	2009.26.2	
	郑勇	教授	061	组织和力学性能的变化			
	庞旭明	硕士	061				
	承 新	硕士	061				
	江赛华	学士	061				
	林新刚	学士	061				
86	钟 杰	硕士	061	功能梯度 Ti(C, N)基金属陶瓷制备技术	复合材料学报	2009.26.3	
	郑勇	教授	061				
	张一欣	硕士	061				
87	张一欣	硕士	061	冷却方式对 Ti(C,N)基金属陶瓷显微组	硬质合金	2009.26.1	
	郑勇	教授	061	织和力学性能的影响			
	郑建智	硕士	061				
	赵永乐	硕士	061				

序	姓名	职称	单位	论文题目	刊物.会议名称	年、卷、期	类别
号	Eth 🛧	硕士	061	功能梯度硬质合金与金属陶瓷制备技	机械工程材料	2009.33.2	
88	钟 杰 郑 勇	教授	061	术的研究进展	77 47 77 77 77 77 77 77 77 77 77 77 77 7	2007.00.12	
	严永林	硕士	061	NET OF STAR			
	庞旭明	硕士	061				
89	庞旭明	硕士	061	Mn 对 Mo <sub>2</sub> FeB <sub>2</sub> 基金属陶瓷组织和力学	中国有色金属	2009.19.9	
09	郑勇	教授	061	性能的影响	学报		
	王少刚	副教授	061	THURANAMA	3 364		
	王秋红	硕士	061				
90	王慧	博士	061	Effects of Ga-Ag, Ga-Al and Al-Ag	Journal of	2009. 20.12	
	華松柏	正高	061	additions on the wetting Characteristics	Materials		
	陈文学	硕士	061	of Sn-9Zn-X-Y lead-free solders	Science:		
	12.7	127			Materials in		
					Electronics		
91	王慧	博士	061	Effects of Ga, Al, Ag, and Ce	Rare Metals	2009.28.6	
	薛松柏	正高	061	multi-additions on the wetting			
	陈文学	硕士	061	characteristics of Sn-9Zn lead-free solder			
92	张亮	博士	061	Effects of rare earths on properties and	Journal of	2009. 20.8	
	薛松柏	正高	061	microstructures of lead-free solder alloys	Materials		
	皋利利	博士	061		Science:		
	曾广	硕士	061		Materials in		
	盛重	硕士	061		Electronics		
	陈燕	工程师	外单位				
93	张亮	博士	061	Effects of trace amount addition of rare	Journal of		
	薛松柏	正高	061	earth on properties and microstructureof	Materials	2009.20.12	
	皋利利	博士	061	Sn-Ag-Cu alloys	Science:		
	陈燕	工程师	外单位		Materials in		
	禹胜林	正高	061		Electronics		
	盛重	硕士	061				
	曾广	硕士	061				
94	张亮	博士	061	Determination of Anand parameters for	Modelling and	2009.17.7	
	薛松柏	正高	061	SnAgCuCe solder	Simulation in		
	皋利利	博士	061		Materials		
	曾广	硕士	061		Science and		
	盛重	硕士	061		Engineering		
	陈燕	工程师	外单位				
95	张 亮	博士	061	Effects of cerium on Sn-Ag-Cu alloys	Journal of Rare	2009.27.1	
	薛松柏	正高	061	based on finite element simulation and	Earths		
	陈燕	工程师	外单位	experiments			
	韩宗杰	博士	061				
	王俭辛	博士	061				
	禹胜林	正高	061				
	卢方焱	硕士	061				

序号	姓名	职称	单 位	论 文 题 目	刊物.会议名称	年、卷、期	类别
96	韩宗杰	博士	061	Laser Soldering of Fine Pitch QFP	Journal of	2009.131.2	
	薛松柏	正高	061	Devices Using Lead-Free Solders	electronic		
	王俭辛	博士	061		packaging		
	张 昕	硕士	061				
	禹胜林	博士	061				
	张亮	博士	061				
97	王俭辛	博士	061	Effects of rare earth Ce on	Journal of alloys	2009.467.1	
	薛松柏	正高	061	microstructures, solderability of	and	-2	
	韩宗杰	博士	061	Sn-Ag-Cu and Sn-Cu-Ni solders as well	compounds		
	禹胜林	博士	061	as mechanical properties of soldered			
	陈燕	工程师	外单位	joints			
	史益平	硕士	061				
	王 慧	博士	061				
98	王慧	博士	061	Ga、Al 对 Sn-Zn 钎料耐蚀及高温抗氧	稀有金属材料	2009.38.12	
	薛松柏	正高	061	化性能的影响	与工程		
	陈文学	硕士	061				
99	陈文学	硕士	061	Solderability and intermetallic	Rare Metals	2009.28.6	
	薛松柏	正高	061	compounds formation of Sn-9Zn-xAg			
	王 慧	博士	061	lead-free solders wetted on Cu substrate			
	王俭辛	博士	061				
	韩宗杰	博士	061				
100	赖忠民	博士	061	Effects of Ga and In on the properties of	China Welding	2009.18.4	
	薛松柏	博士	061	AgCuZn cadmium-free filler metal			
	卢方焱	博士	061				
-	顾立勇	工程师	外单位				
	顾文华	高工	外单位				
101	王 慧	博士	061	Effects of Al, Ga, and Ag on the surface	China Welding	2009. 18.2	
	薛松柏	正高	061	properties and wetting reactions of			
	陈文学	硕士	061	Sn-9Zn-X solders			
102	肖正香	硕士	061	CuCGA 器件焊点热疲劳行为数值模拟	焊接学报	2009.30.12	
	薛松柏	正高	061				
	金春玉	硕士	外单位				
	张 亮	博士	061				
	皋利利	博士	061				
103	叶 焕	硕士	061	CSP 器件无铅焊点可靠性的有限元分	焊接学报	2009.30.11	
	薛松柏	正高	061	析			
	张亮	博士	061				
	王慧	博士	061				
104	盛重	硕士	061	QFP 器件微焊点可靠性分析	焊接学报	2009.30.10	
	薛松柏	正高	061				
	张亮	博士	061				
	皋利利	博士	061				

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号							
105	朱宏	博士	061	合金元素对 6063 铝合金阶梯焊中温钎	焊接学报	2009. 30.8	
	薛松柏	正高	061	料性能的影响			
	盛重	硕士	061		THE LAW AND		
106	盛重	硕士	061	QFP 器件微焊点热疲劳行为分析	焊接学报	2009.30.12	
	薛松柏	正高	061				
	张 亮	博士	061				
	皋利利	博士	061				
107	朱 宏	博士	061	6063 铝合金氧化膜与 CsF-AlF3 及	焊接学报	2009. 30.9	
	薛松柏	正高	061	KF-AIF3 钎剂的反应机制			
	盛重	硕士	061				
108	朱 宏	博士	061	6063 铝合金阶梯焊中温钎料腐蚀性能	焊接学报	2009.30.10	
	薛松柏	正高	061	分析			
	盛重	硕士	061				
109	戴玮	硕士	061	不同阵列 PBGA 器件焊点可靠性分析	焊接学报	2009.30.9	
	薛松柏	正高	061				
	张 亮	博士	061				
	盛重	硕士	061				
110	戴玮	硕士	061	基于田口法的 PBGA 器件焊点可靠性	焊接学报	2009.30.11	
	薛松柏	正高	061	分析			
	张 亮	博士	061				
	姬 峰	硕士	061				
111	王 慧	博士	061	复合添加 Ga、Al、Ag 对 Sn-9Zn 钎料	焊接学报	2009.30.6	
	薛松柏	正高	061	性能的影响			
	陈文学	硕士	061				
112	王慧	博士	061	不同钎剂对 Sn-Zn 系无铅钎料润湿特性	焊接学报	2009. 30.1	
	薛松柏	正高	061	的影响			
	陈文学	硕士	061				
	王检辛	博士	061				
113	胡玉华	硕士	061	Sn-9Zn-xAg 钎料在 Cu 基材上润湿性	材料工程	2009.6	
	薛松柏	正高	061	能及界面组织的研究			
	陈文学	硕士	061				
	王慧	博士	061				
114	张 亮	博士	061	基于蠕变模型细间距器件焊点疲劳寿	机械工程学报	2009. 45.94	
	薛松柏	正高	061	命预测			
	卢方焱	硕士	061				
	韩宗杰	博士	061				
	禹胜林	博士	061				
115	张 亮	博士	061	铈对 SnAgCu 钎料的显微组织和性能影	中国稀土学报	2009. 27.2	
	薛松柏	正高	061	响	4 475	7.160	
	曾广	硕士	061				
	皋利利	博士	061				
	陈燕	工程师	外单位				

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号	姓名		于业		100 100 100 100 100 100 100 100 100 100		30,77
116	陈文学	硕士	061	Sn-9Zn-xAg 无铅钎料润湿性能及焊点	焊接学报	2009.30.6	
	薛松柏	正高	061	力学性能			
	王 慧	博士	061			2	
	王俭辛	博士	061				
117	卢方焱	硕士	061	镓对 AgCuZn 钎料组织和性能的影响	焊接学报	2009. 30.1	
	薛松柏	正高	061				
	张 亮	博士	061				
	赖忠民	博士	061				
	顾立勇	工程师	外单位				
	顾文华	高工	外单位				
118	姫 峰	硕士	061	QFN 封装焊点可靠性的有限元分析	焊接学报	2009.30.10	
	薛松柏	正高	061				
	张 亮	博士	061				
	王 慧	博士	061				
119	薛松柏	正高	061	航空器制造中的焊接技术	航空制造技术	2009.17	
	张 亮	博士	061				
	皋利利	博士	061				
	韩宗杰	博士	061				
	禹胜林	博士	061				
	朱 宏	博士	061				
120	肖正香	硕士	061	微量元素对 Sn-Zn 系钎料性能和组织的	电焊机	2009.39.11	
	薛松柏	正高	061	影响			
	张 亮	博士	061				
	皋利利	博士	061				
121	叶 焕	硕士	061	稀土元素对 SnAgCu 钎料性能的影响	电焊机	2009.39.10	
	薛松柏	正高	061				
	张 亮	博士	061				
	皋利利	博士	061				
	曾广	硕士	061				
122	王慧	博士	061	Ag对 Sn-9Zn 无铅钎料耐蚀性能影响的	焊接	2009. 增刊	
	薛松柏	正高	061	研究		1	
	陈文学	硕士	061				
	胡玉华	硕士	061				
123	皋利利	博士	061	微量元素对 Sn-Ag-Cu 系钎料以及焊点	焊接	2009. 增刊	
	薛松柏	正高	061	的影响		1	
	张 亮	博士	061				
	盛重	硕士	061				
124	薛松柏	正高	061	Sn-Zn 系无铅钎料研究中的几个热点	第十七届全国		
	王慧	博士	061		钎焊及特种连		
	陈文学	硕士	061		接技术交流会		
	顾立勇	工程师	外单位		议		
	顾文华	高工	外单位				

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125	赖忠民	博士	061	合金元素对 Ag-Cu-Zn 系钎料影响的研	第十七届全国		
	张亮	博士	061	究现状及发展趋势	钎焊及特种连		
	薛松柏	正高	061		接技术交流会		
	卢方焱	硕士	061		议		
126	张 满	博士	061	锌基中温铝钎料的研究现状及发展趋	第十七届全国		
	薛松柏	正高	061	势	钎焊及特种连		
	王慧	博士	061		接技术交流会		
					议		
127	马 骋	博士	061	Ti(C,N)基金属陶瓷与 45 号钢真空钎焊	第十七届全国		
	薛松柏	正高	061	研究	钎焊及特种连		
	吴铭方		外单位		接技术交流会		
	陈健		外单位		议		
128	薛松柏	正高	061	微电子组装焊点可靠性研究进展	焊接	2009. 增刊	
	张亮	博士	061			1	
	盛重	硕士	061				
	皋利利	博士	061				
129	李 勇	副教授	061	BMI-QC130 双马树脂拉挤工艺	复合材料学报	2009.26.5	
	肖 军	教授	061				
	谭永刚	硕士	061				
	原永虎	硕士	061				
130	李 勇	副教授	061	X-cor 夹层结构压缩性能研究	航空学报	2009.30.3	
	肖 军	教授	061				
	谭永刚	硕士	061				
	原永虎	硕士	061				
	党旭丹	博士	061				
131	罗海燕	硕士	061	复合材料自动辅带技术研究——曲面	航空学报	2009.30.9	
	李 勇	副教授	061	辅带轨迹算法			
	肖 军	教授	061				
	还大军	博士	061				
132	叶 进	硕士	061	复合材料自动辅带技术——曲面辅带	宇航材料工艺	2009.0.4	
	文立伟	副教授	061	CAM 技术			
	李 勇	副教授	061				
	肖 军	教授	061				
133	李 勇	副教授	061	完善工程训练体系 培养高素质人才	实验室研究与	2009.28.5	
	黄炳辉	研究员	机关		探索		
	殷凯	助工	机关				
134	唐正霞	博士	061	Preparation of high quality	Thin Solid Films	2009.517.1	
	沈鸿烈	教授	061	polycrystalline silicon thin films by		9	
	黄海宾	博士	061	aluminum-induced crystallization			
	鲁林峰	博士	061				
	尹玉刚	博士	061				
	蔡 红	博士	061				

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135	唐正霞	博士	061	Polycrystalline silicon thin film prepared	Journal of	2009.11.8	
	沈鸿烈	教授	061	by aluminum-induced crystallization with	Optoelectronics		
	鲁林峰	博士	061	native silicon oxide at the aluminum and	and Advanced		
	江丰	博士	061	silicon interface	Materials		
	郭艳	硕士	061				
	沈剑沧	工程师	外单位				
136	李 丹	硕士	061	电沉积法制备 ZnO 薄膜的结构与光电	压电与声光	2009.31.3	
	沈鸿烈	教授	061	性能研究			
	鲁林峰	博士	061				
	黄海宾	博士	061				
	李斌斌	副教授	061				
137	蔡 红	博士	061	The effects of porous silicon on the	Journal of	2009.70.6	
	沈鸿烈	教授	061	crystalline properties of ZnO thin films	Physics and		
	尹玉刚	硕士	061		Chemistry of		
	鲁林峰	博士	061		Solids		
	沈剑沧	工程师	外单位				
	唐正霞	博士	061				
138	黄海宾	博士	061	Effects of hydrogen dilution ratio on	Journal of	2009.11.11	
	沈鸿烈	教授	061	properties of Boron-doped germanium	Optoelectronics		
	张 磊	博士	061	films by hot-wire Chemical vapor	and Advanced		
	吴天如	博士	061	deposition	Materials		
	鲁林峰	博士	061				
	唐正霞	博士	061				
	沈剑沧	工程师	外单位				
139	唐正霞	博士	061	Fractal growth of amorphous silicon	Journal of	2009.11.11	
	沈鸿烈	教授	061	crystallization induced by aluminum	Optoelectronics		
	黄海宾	博士	061		and Advanced		
	鲁林峰	博士	061		Material		
	蔡 红	博士	061				
	沈剑沧	工程师	外单位				
140	徐江	教授	061	Improving the corrosion wear resistance	Journal of	2009.42	
	卓城之	硕士	061	of AISI 316L stainless steel by	Physics D:		
	陶杰	教授	061	particulate reinforced Ni matrix	applied physic		
	蒋书运	教授	外单位	composite alloying layer			
	刘林林	硕士	061				
141	徐 江	教授	061	Erosion—corrosion behavior of	Corrosion	2009.51.5	
	卓城之	硕士	061	nano-particle-reinforced Ni matrix	Science		
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	陶杰	教授	061	surface treatment in aqueous slurry			
	刘林林	硕士	061	environment			
	蒋书运	教授	外单位				

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				Film by Double Cathode Glow Discharge			
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	陶杰	教授	061	deposited by double glow plasmas	Technological		
	蒋书运	教授	外单位	technique	Sciences		
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	姚正军	教授	061	及其性能			
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				synthesized by double glow plasma	Metals Society		
				surface alloying technology	of China		

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	姚正军	教授	061	乃是性能	(自然科学版)		
155	周金堂	硕士	061	回收 PP 增韧性能的初步探索	材料科学与工	2009.27.2	
	姚正军	教授	061		程学报		
156	孟召辉	硕士	061	聚丙烯的共混改性研究	气和工艺与材	2009.11	
	姚正军	教授	061		料		

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### Fabrication of functionally graded Ti(C, N)-based cermets by double-glow plasma carburization

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#### ABSTRACT

Functionally graded Ti(C, N)-based cermets were prepared via vacuum liquid sintering and subsequent double-glow plasma carburization. The microstructure was characterized using scanning electron microscope (SEM), electron probe microanalysis (EPMA) and X-ray diffraction (XRD). It was found that a surface zone enriched in titanium, molybdenum, tungsten, carbon and nitrogen, deficient in nickel was introduced by double-glow plasma carburization. The high carbon activity in the surface region drove titanium, molybdenum and tungsten elements inside the substrate to diffuse outwards, consequently the nickel-rich binder was forced to transport inwards. The formation of the binder-deficient layer was controlled by the diffusion of the alloy elements and the growing rate did not follow the parabolic law.

#### 1. Introduction

Ti(C, N)-based cermets are used as cutting tools for the high hardness, good thermal stability, excellent creep and wear resistance [1,2], but the appreciably low strength restricts their use. This issue could be commendably solved by introducing graded structure into the materials [3].

Over the past years, many approaches were suggested to prepare functionally graded hardmetals and cermets, such as coating and heat-treatment in nitrogen [4,5]. Coating could greatly enhance the surface wear resistance by depositing a layer of hard material on the tough bulk [6]. Since the coating process is usually carried out at high temperature, cracks are formed ineluctably due to different thermal expansion coefficients between coatings and substrate [7]. During machining, the cracks propagated through the entire coating and resulted in catastrophic failure. These cracks could be avoided by heat-treatment in nitrogen [8]. However, due to tiny solubility of nitrogen in the nickel binder, the gradient layer was limited, although a long heat-treatment time was applied [3].

It was found that the formation of the graded structure resulted from the differences of the affinity between nitrogen and different alloy elements during nitriding [9]. As there is also a remarkable difference of the affinity between carbon and these metallic elements, a gradient is also anticipated by carburization. However there is no report on the issue till now.

The double-glow plasma surface alloying technology (known as Xu-Tec process or DG technology) was developed in 1980, and had been successfully used in surface modification of metal materials [10]. The Xu-Tec process is a unique and hybrid technique using a double-glow discharge phenomenon inside a vacuum chamber, which has evolved from both plasma nitriding and sputtering techniques [11]. In general, any metallic or metalloid element could be alloyed into the surface of the conductive substrates. In the present study, functionally graded Ti(C, N)-based cermets were prepared via vacuum liquid sintering and subsequent double-glow plasma carburization. Then the microstructure and composition distribution of the carburized cermets were investigated. In addition, the forming mechanism of the graded layer was also discussed.

#### 2. Experimental procedure

The schematic presentation of double-glow plasma surface alloying equipment is shown in Fig. 1. There are three electrodes in the vacuum chamber of the double-glow plasma surface alloying apparatus: one anode and two negatively charged members [12]. The negatively charged members include cathode (workpiece) and the source electrode.

In the present experiment, the source electrode was made up of carbon. The cathode and source electrode were surrounded by glow discharge, one glow discharge heated the substrate to be alloyed and the second glow struck the source electrode [11], which was known as double-glow discharge. During carburization, the cermets were heated to a designed temperature by plasma bombardment and carbon was sputtered by the second glow from

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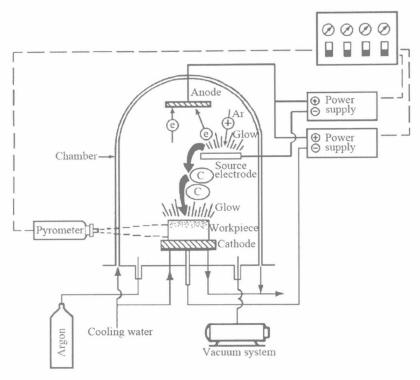


Fig. 1. Sketch map of equipment for double-glow plasma carburization [11].

Table 1
Chemical composition and mean particle size of initial powders.

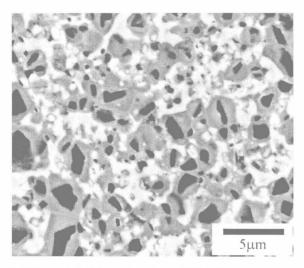
Particle size (µm)	Chemical composition (wt.%)
0.51	0 ≤ 1.21
0.52	0 ≤ 1.10
0.85	$C_{free} \le 0.025, O \le 0.21$
1.70	$C_{free} \le 0.03, O < 0.22$
2.60	$C_{free} \leqslant 0.0012$ , $O \leqslant 0.10$
	0.51 0.52 0.85 1.70

the source electrode, then flied towards and subsequently diffused into the substrate surface to form a gradient layer.

The characteristics of the initial powders are summarized in Table 1. The compositions of the two kinds of cermets with different nickel content considered in the present study are TiC-10 wt.% TiN-21 wt.% Ni-16 wt.% Mo-8.4 wt.% WC and TiC-10 wt.% TiN-32 wt.% Ni-16 wt.% Mo-8.4 wt.% WC, respectively.

The powder mixtures were ball milled in alcohol for 24 h, the mass ratio of ball to material was 7:1 and the rotational speed was 260 rpm. The bar specimens with a dimension of 40.0 mm  $\times$  8.0 mm  $\times$  6.5 mm were dry pressed and then sintered in vacuum at 1430 °C for 1 h. The as-sintered specimens were polished and carburized at 1100 °C and 1200 °C. At each temperature, different samples were carburized for 90 min, 120 min, 150 min and 180 min, respectively. The discharged gas was pure argon.

The microstructures of the as-sintered as well as carburized material were observed by scanning electron microscope operated at 20 kV (SEM QVANTA200, FEI) in backscattered-electron (BSE) mode. Compositional depth profiles of the as-sintered and the carburized materials were acquired using electron probe microanalysis (EPMA 8705QH2) combined WD/ED microanalyzer operated at 20 kV, the line scans were 100  $\mu m$  wide. Phase identification of the materials was determined by X-ray diffraction (Bruker D8 ADVANCE X-ray diffractometer), Cu K $\alpha$  radiation, 20° < 2 $\theta$  < 110°



**Fig. 2.** BSE micrograph of the as-sintered material. The hard phase appears black core-grey rim and white core-grey rim, the binder phase appears white and distributes between the ceramic grains.

angular range,  $0.02^{\circ}$  angle step. The microhardness was tested on the cross section of the specimen.

#### 3. Results and discussion

#### 3.1. Microstructure

The microstructure of the as-sintered material shows that the carbonitride grains, often with a core-rim structure, are embedded in a tough metallic binder phase, typically in Ti(C, N)-based cermet, as displayed in Fig. 2.

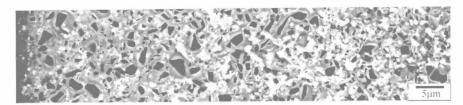


Fig. 3. BSE micrograph of the material carburized at 1200 °C for 180 min. The surface is at the left side.

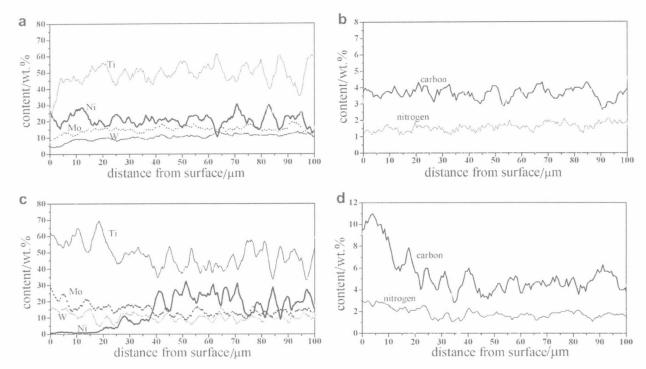


Fig. 4. Compositional line distributions of the as-sintered and carburized: (a, b) as-sintered and (c, d) carburized at 1200 °C for 180 min.

The cores were undissolved Ti(C, N) from the raw powder. The rim, which was introduced by reprecipitation of the carbonitride phases (Ti, Mo, W) (C, N) on the core at different sintering stage, could be divided into inner rim and outer rim. The inner-rim was formed during solid state sintering and enriches in molybdenum and tungsten. The outer rim appearing gray in BSE model was formed during liquid state sintering and contains less molybdenum and tungsten than inner rim [9].

The microstructure of the cermets treated by double-glow plasma carburization at 1200 °C for 180 min is shown in Fig. 3. The binder content decreased abruptly in the surface zone down to about 20  $\mu m$  depth, then gradually increased inwards, there was a notable increase in the binder content between about 40  $\mu m$  and 70  $\mu m$  below the surface. The typical core-rim structure in the surface was reserved after carburization. However the rim became thicker in the area where the binder content was reduced as compared to the as-sintered material.

The EMPA depth profiles are shown in Fig. 4. The results revealed that the elements distributions were constant from surface to bulk in the as-sintered material. After carburization, a notable increase in the contents of carbon, nitrogen, titanium, molybdenum and tungsten was found down to about 40  $\mu$ m, and the increase ratio in carbon was quite higher than the other elements. The nickel content dropped to near zero in the surface area down to nearly 20  $\mu$ m, then increased and reached a summit between

about 40  $\mu m$  and 70  $\mu m$  depth and finally fell to a stable value, which was consistent with distribution of the binder phase.

Since diffusion was substantially faster in the nickel binder than in carbonitride, the binder would act as the main transport medium during carburization. Considering the strong affinity between carbon and titanium, tungsten and molybdenum, reaction occurred as soon as carbon diffused into the nickel binder at high temperature. Here, the reaction could be expressed as follows:

$$C + (Ni, Ti, Mo, W) \rightarrow (Ti, Mo, W)C + Ni$$
 (1)

The reaction decreased the concentration of titanium, molybdenum and tungsten in the alloy binder, caused these metallic elements to transport outwards and forced nickel to transfer inwards. The new formed carbides precipitated on original carbonitride grains preferentially, thus, the thickness of the out rim was increased. Since nickel content decreased in the surface area, the binder content was reduced correspondingly. It should also be noted that the relatively high nitrogen content close to the surface resulted from the great decrease in the binder.

#### 3.2. Phase constitution

The XRD patterns of as-sintered and carburized cermets are shown in Fig. 5. Two kinds of phases were observed in the as-sintered samples, the  $\delta$  phase and  $\gamma$  phase. The  $\delta$  phase was the carbo-

nitride grains while the  $\gamma$  phase was the binder. Only  $\delta$  phase was observed at surface of the carburized cermets. Even at 5  $\mu m$  below the surface, no  $\gamma$  phase was observed. A small quantity of binder was observed at about 23  $\mu m$  depth. Fig. 6 shows that the (200) diffraction peaks of the  $\delta$  phase of the carburized cermets at surface and 5  $\mu m$  below the surface were left-shifted, while it kept almost unchanged at 23  $\mu m$  depth as compared with the as-sintered material. It is reasonable to estimate that the shift of the  $\delta$  phase diffraction peaks was caused by the increase of carbon in the carbonitride. As the carbonitride of the as-sintered cermets was always nonstoichiometric because of decarbonization and denitrification during sintering [6], carbon atoms filled the interstitial sites of carbonitride during carburization which could be simply expressed as follows:

$$C + (Ti, W, Mo)(C_x, N_1 - x)_y \rightarrow (Ti, W, Mo)(C_{x'}, N_{1-x'})_{y'}$$
 (2)

#### 3.3. Performance

The microhardness along the depth is shown in Fig. 7. It was found that the hardness of the surface area was greatly increased

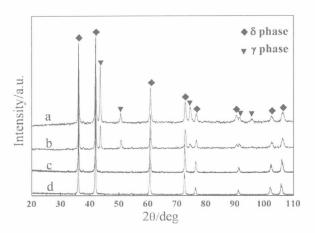


Fig. 5. XRD patterns of (a) as-sintered material, (b) 23 μm below the surface of the carburized material, (c) 5 μm below the surface of the carburized material and (d) the surface of the carburized material.

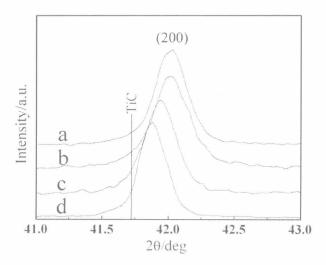


Fig. 6. XRD patterns around the area of the (200) diffraction peaks of (a) assintered material, (b) 23  $\mu m$  below the surface of the carburized material, (c) 5  $\mu m$  below the surface of the carburized material and (d) the surface of the carburized material.

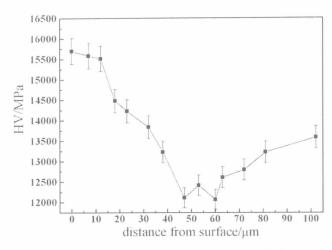


Fig. 7. Hardness distribution on the cross section of the carburized sample.

by double-glow plasma carburization while the TRS  $(1816^{+102}_{-122} \, \mathrm{MPa})$  was hardly changed, comparing with the as-sintered material (the hardness was  $13.550^{+420}_{-380} \, \mathrm{MPa}$  and the TRS was  $1798^{+133}_{-124} \, \mathrm{MPa}$ ).

In general, the surface hardness was increased by inducing a carbonitride-rich layer in the surface zone after carburization. In the meantime, a binder-rich area was formed in the near surface during carburization, which was beneficial to the binding between the surface zone and the substrate.

#### 3.4. Development of the binder-deficient layer

During double-glow plasma carburization, carbon diffused from the surface to interior of cermets, reacted with the metallic elements and drove nickel inwards. As a result, a binder-deficient layer with binder content near zero in the surface zone was formed. Because the binder was nickel-based alloy, it was reasonable to determine the thickness of the binder-deficient layer roughly by measuring the nickel content at different positions of a graded cermet. The experimental results are shown in Fig. 8.

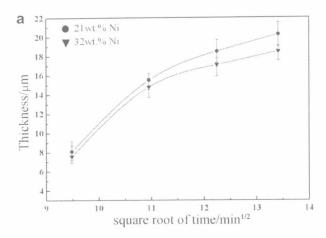
Since the diffusion rate of carbon was much faster than metallic elements, the formation of the binder-deficient layer was mainly controlled by the diffusion of metallic elements and should follow the parabolic law [5]:

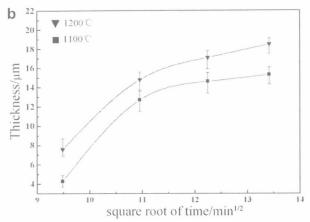
thickness 
$$\propto \sqrt{\text{time}}$$
 (3)

Fig. 8a shows that the growth rate of the binder-deficient layer of the cermet with lower nickel content was faster under the same carburization condition, which is in accord with the rule that the formation of the graded layer is controlled by the diffusion of metallic elements. However, the growth of the binder-deficient layer did not follow the parabolic law exactly, it could be ascribed to the great change of diffusion coefficient of the alloy elements under ion bombardment [13].

Vacancy mechanism played the most important role in the substitutional diffusion process. By ion bombardment, supersaturated vacancies were introduced to the material [14], which increased the diffusion probability of the atoms. On the other hand, the diffusion activation energy was reduced in the surface area as the vacancy activation energy could be provided by ion bombardment.

The vacancies annihilated soon when encountered with interstitial atoms, dislocations or grain boundaries during migration, thus, a concentration gradient of vacancy was formed. The diffusion coefficient of the alloy elements changed as a function of vacancy concentration which induced the development of the binder-deficient layer to deviate from the parabolic law. A higher





**Fig. 8.** Thicknesses of the hard phase-rich layer vs square root of time. (a) Materials with different nickel content carburized at 1200 °C; (b) materials with 32 wt.% nickel content carburized at different temperature.

diffusion coefficient was obtained at 1200 °C since the concentration and activity of vacancies were higher at a higher temperature, which is in accord with the result shown in Fig. 8b.

#### 4. Conclusions

(1) A 40  $\mu m$  surface zone enriched in carbon, titanium, molybdenum, tungsten and nitrogen and deficient in nickel was introduced by double-glow plasma carburization, while the microstructure was influenced down to about 70  $\mu m$  below the surface.

- (2) The differences of affinity between carbon and the metallic elements caused titanium, tungsten and molybdenum to transport towards the surface and nickel inwards during carburization.
- (3) The hardness of the surface area was increased after carburization, while the TRS was hardly changed.
- (4) The formation of the binder-deficient layer was controlled by the diffusion of the metallic elements but deviates from the parabolic law. Abundant supersaturated vacancies introduced by the ion bombardment enhanced the diffusion coefficient of the elements.

#### Acknowledgements

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