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总主编 顾诵芬

Reliability Analysis of Dynamic Systems: Efficient Probabilistic Methods and Aerospace Applications

动态系统可靠性分析: 高效方法及航空航天应用(英文版)

Bin Wu 吴 斌著







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内容提要

本书针对动态系统的可靠性分析,阐述了一种新的优化技术,即针对低频率谐振动力载荷下的工程产品结构可靠性问题,使用综合的快速概率方法,也即"扰动算法+蒙特卡洛方法"。在针对两个航空航天实际工程案例的应用中发现,运用此方法能快速准确地解决失效面高非线性、大量计算强度和动态系统高复杂度等原有概率方法的应用困难。本书的出版填补了国际上对高效快速概率方法的研究空白。

本书可供从事民用飞机结构可靠性安全性工程设计分析、试验、管理的技术人员和相关专业的研究生使用。

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Dedication

To my family

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Deterministic analysis approaches/tools have dominated the whole aerospace industry for many years. It has been widely accepted, however, that the relevant non-deterministic analysis methods, either probabilistic or possiblistic, will be eventually adopted to some extent in this area. This process has been very slow, partly due to the conservative nature of the industry and partly due to some difficulties in applying these methods, which are now being addressed by both academia and industry.

Within the last decade in the engineering field, possibilistic approaches have been widely studied and applied to the reliability analysis of dynamic systems. During this period, there has been a lack of research interest in delivering efficient probabilistic methods. This book presents a novel technique that applies probabilistic methods to reliability analysis of engineering systems under harmonic loads in the low-frequency range. The aim was to overcome certain problems of applying probabilistic methods. The problems that need to be overcome were the nonlinearity of the failure surface, the intensive computational cost, and the complexity of the dynamic system.

A perturbation analysis algorithm was developed based on a modal approximation model. Since the resonance cases are of most concern, the optimized model simplifies the complexity of the dynamic systems by only concentrating on the resonance dominating terms in the response element (expressed in terms of modal coordinates). This optimization and later newly defined parameters transform the original failure surface into an approximate but smooth and linear one. Finally, the statistical information of the new parameters can be derived from that of the original variables by solving only once the eigen problem on the mean values of the original variables. An efficient reliability method, such as FORM, can then be applied.

However, for a given 2D frame structure, the FORM method failed to accurately predict the probability of failure. The Monte Carlo simulation method was later adopted to replace the FORM method. The Monte Carlo simulations were only performed for the new random parameters that were obtained through one execution of an eigen solver. Thus the overall efficiency of this combined approach, i.e. perturbation approach plus Monte Carlo simulation method, is high. Both accuracy and efficiency were achieved when this combined approach was applied to the 2D structure, as well as to a complex 3D helicopter model. Finally the response surface method was

employed to derive the statistical information of the stiffness matrix from that of the original property random variables.

Low modal overlap factor, responses near resonance, low statistical overlap and small changes in eigenvalues and Gaussian distribution of the original variables are the conditions required for this approach to work.

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Dr. Bin Wu COMAC, China March 2013

(Nomenclature)

ABBREVIATIONS

| ACSR | Active control of structural response |
|-------------|---------------------------------------|
| AVS | Active vibration suppression |
| AVC | Active vibration control |
| BG | Bubnov-Galerkin |
| DOF | Degree of freedom |
| FE | Finite element(s) |
| FEA | Finite element analysis |
| FEM | Finite element method |
| FFEM | Fuzzy finite element method |
| FORM | First-order reliability method |
| FRF | Frequency response function |
| GOE | Gaussian orthogonal ensemble |
| HHC | Higher harmonic control |
| IBC | Individual blade control |
| jpdf | Joint probability density function |
| MC | Monte Carlo (simulation method) |
| MCS | Monte Carlo simulation (method) |
| pdf | Probability density function |
| PDE | Partial differential equation |
| RS | Response surface |
| RSM | Response surface method |
| SEA | Statistical energy analysis |
| SFE | Statistical finite element |
| SORM | Second-order reliability method |
| SRBM | Stochastic reduced basis method |
| TEF | Trailing edge flap |
| | |

NOTATION AND SYMBOLS

| M | Mass matrix |
|----------|--|
| K | Stiffness matrix |
| A | Area |
| E | Modulus of elasticity (Young's modulus) |
| L | Length |
| β | Safety index |
| ρ | Property density |
| η | Loss damping factor |
| ω | Radian frequency/excitation frequency |
| f | Cyclic frequency (Hz)/excitation frequency |
| | |

| $[\Phi]$ | Mass-normalized modal matrix |
|--------------|---|
| ϕ_i | jth column vector of mass-normalized modal matrix |
| ω_i | ith undamped natural frequency |
| $\{\psi_i\}$ | ith mode shape |
| $P(\)$ | Probability |
| f_x | Pdf of random variable x |
| μ_x | Mean value of random variable x |
| σ_x | Standard deviation of random variable x |
| E(x) | Expected value of random variable x |
| D(x) | Variance of random variable x |
| $C_x(Cov_x)$ | Covariance matrix of random variable x |
| C | Confidence level |
| α | Fuzzy confidence level |
| Φ | Standard normal distribution function |

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