





# 机电学院

052 系



序号	姓名	职 称 或学历	单位	论文题目	刊物、会议名称	年、卷、期
1	陈劲松 黄因慧 刘志东 田宗军	博士生 教 授 副教授 副教授	052	Jct Electrodeposited Cu-Al2O3 Nanocomposite Coatings	2007微纳系统集成及商业化 应用国际学术会议	2007
2	范 晖 黄因慧 田宗军 刘志东 陈劲松	博士生 教 授 副教授 副教授 博士生	52	A Study on the Electrodeposited Cu- Al2O3 Composites Coating With Laser Treatment	2007微纳系统集成及商业化 应用国际学术会议	2007
3	洪淑文 黄因慧 田宗军 刘志东 陈劲松	硕士生 教 授 副教授 副教授 博士生	052	喷射电沉积喷嘴流场的数值分析	电镀与环保	2007. 27 (2)
4	刘志东 陈 勇 朱 军 黄因慧 田宗军	副教授 硕士生 硕士生 教 授 副教授	052	45钢喷射电镀Ni层激光重熔温度场 数值模拟及其性能研究	应用激光	2007. 27 (2)
5	刘志东	副教授	052	高精度高速走丝线切割机床大锥度 机构的实现	航空精密制造技术	2007. 43 (5)
6	刘志东 俞容亨	副教授	052	高速走丝电火花线切割机床多次切 割的实现	中国机械工程	2007. 18 (20)
7	刘志东	副教授	052	基于复合工作液的电火花线切割技 术研究	中国机械工程学会特种加工 学术会议	2007
8	刘志东 陈 勇 黄因慧 何静波 田宗军	副教授 硕士生 教 授 硕士生 副教授	052	喷射电镀Ni镀层激光重熔温度场的 数值模拟	中国机械工程	2007. 18 (23)
9	刘志东	副教授	052	以复合工作液为放电介质的低速走 丝电火花线切割可行性研究	航空精密制造技术	2007. 43 (4)
10	沈理达 黄因慧 田宗军 花国然	博士生 教 授 副教授 副教授	052	Laser Sintering of Nano-Al2O3 Powders on Plasma Sprayed Ceramic Based Coatings	2007微纳系统集成及商业化 应用国际学术会议	2007
11	沈理达 田宗军 黄因慧 刘志东 花国然	博士生 副教授 教 授 副教授 副教授	052	激光烧结PSZ纳米陶瓷团聚体粉末 的试验研究	应用激光	2007. 27 (5)
12	沈理达 黄因慧 田宗军 花国然	博士生 教 授 副教授 副教授	052	Direct Fabrication of Bulk Nanostructured Ceramic from Nano-AL2O3 Powders by Selective Laster Sintering	Key Engineering Materials	2007. 329
13	田宗军 黄因慧	副教授 教 授	052	Preparation and Magnetic Properties of the Exchange Coupling NdFeB Nanocomposited Permanent Magnets	2007微纳系统集成及商业化 应用国际学术会议	2007
14	田宗军	副教授	052	基于JSP的远程教学平台的设计与 实现	计算机与信息技术	2007

15	王东生 黄因慧 田宗军 刘志东	博士生 教授 副教授 副教授	052	TiAl合金表面涂层技术研究现状	材料导报	2007. 21 (11)
16	王东生 黄因慧 田宗军 刘志东 朱 军	博士生 教授 副教授 副教授 硕士生	052	激光重熔喷射电沉积纳米晶镍涂层 微观结构	电加工与模具	2007 第5期
17	王东生 黄因慧 田宗军 刘志东 朱 军	博士生 教授 副教授 副教授 硕士生	052	脉冲喷射电沉积纳米结构镍涂层研 究	纳米科技	2007. 4 (3)
18	王东生 田宗军 沈理达 刘志东 邱明波 黄因慧	博士生 副教授 博士生 副教授 博士生 教授	052	钛合金表面激光重熔等离子喷涂 MCrAlY涂层温度场数值模拟	应用激光	2007. 27 (6)
19	王桂峰 黄因慧 田宗军 刘志东 陈劲松 高雪松	博士生 教授 副教授 副教授 博士生 博士生	052	分形结构二维金属镍枝晶的制备与 分析	电镀与涂饰	2007. 26 (11)
20	王桂峰 黄因慧 田宗军 刘志东 陈劲松 高雪松	博士生 教授 副教授 副教授 博士生 博士生	052	金属镍电沉积中枝晶分形生长的研 究	电镀与环保	2007. 27 (3)
21	王桂峰 黄因慧 田宗军 刘志东 陈劲松 高雪松	博士生 教授 副教授 副教授 博士生 博士生	052	温度对金属镍电沉积中枝晶分形 生长的影响	电镀与环保	2007. 27 (6)
22	赵 丹 刘志东 田宗军 黄因慧 沈理达 王东生	硕士生 副教授 副教授 教授 博士生 博士生	052	钛合金表面激光重熔高温抗氧化涂 层温度场仿真	热处理技术与装备	2007. 28 (6)
23	赵阳培 黄因慧 刘志东 田宗军 赵剑峰 花国然	副教授 教授 副教授 副教授 教授 副教授	052	脉冲射流电铸纳米晶铜的组织与性 能	机械工程材料	2006. 30 (6)
24	李曙生 徐九华 肖 冰 严明华 傅玉灿 徐鸿钧	博士生 教授 副教授 硕士生 教授 教授	052	Performance of Brazed Diamond Cup-type Wheels with Defined Grain Pattern in Grinding Cemented Carbide	南京航空航天大学学报 (英 文版)	2007, 24(1)



25	杨志波 徐九华 傅玉灿 徐鸿钧	博士生 教授 教授 教授	052	钢基体上镍基钎料激光钎焊金刚石磨粒的界面结构	机械工程材料	2007, 31(5)
26	杨志波 徐九华 徐鸿钧 傅玉灿	博士生 教授 教授 教授	052	镍基钎料激光钎焊金刚石磨粒的试验研究	粉末冶金技术	2007, 25(4)
27	杨志波 徐九华 傅玉灿 徐鸿钧	博士生 教授 教授 教授	052	连续扫描激光钎焊温度场有限元分析	应用激光	2007, 27(4)
28	丁文锋 徐九华 周来水 傅玉灿 肖冰 苏宏华	博士后 教授 教授 教授 副教授 副教授	052	立方氮化硼超硬磨料与45钢钎焊接头残余应力有限元分析	机械工程学报	2007, 43(5)
29	丁文锋 徐九华 傅玉灿 苏宏华 肖冰	博士后 教授 教授 副教授 副教授	052	基于残余应力分布优选钎焊CBN磨粒出露高度	中国机械工程	2007, 18(10)
30	丁文锋 徐九华 傅玉灿 苏宏华 肖冰 周来水	博士后 教授 教授 副教授 副教授 教授	052	单层钎焊立方氮化硼砂轮工作面磨粒包埋深度的确定	中国有色金属学报	2007, 17(3)
31	丁文锋 徐九华 沈敏 傅玉灿 肖冰 苏宏华	博士后 教授 硕士生 教授 副教授 副教授	052	Development and performance of monolayer brazed CBN grinding tools	International Journal of Advanced Manufacture Technology	2007, 34
32	丁文锋 徐九华 傅玉灿 苏宏华 肖冰	博士后 教授 教授 副教授 副教授	052	Effects of the Embedding Depth on the Residual Stresses in the Brazed Cubic Boron Nitride Abrasive Grain	The International Symposium on Advanced Abrasive Technology会议论文集	美国 Dearborn, 2007年9月
33	卢金斌 徐九华	博士生 教授	052	真空钎焊金刚石界面碳化物的形貌	中国有色金属学报	2007, 17(7)
34	徐九华 丁文锋 傅玉灿	教授 博士后 教授	052	Fabrication and Characterization of Brazed CBN Wheels with Rhythmed Grain Distribution	The International Symposium on Advanced Abrasive Technology会议论文集	美国 Dearborn, 2007年9月
35	葛英飞 徐九华 杨辉 罗松保 傅玉灿	博士生 教授 教授 教授	052	碳化硅增强颗粒含量和尺寸对铝基复合材料超精密车削表面的影响	机械工程材料	2007, 31(6)
36	葛英飞 徐九华 杨辉 傅玉灿 罗松保	博士生 教授 教授 教授	052	SiCp / Al复合材料超精密车削表面质量的影响因素	机械工程材料	2007, 31(10)

37	葛英飞 傅玉灿 徐九华	博士生 教授 教授	052	Experimental Study on High Speed Milling of $\gamma$ -TiAl Alloy	Key Engineering Materials	2007, 339
38	徐正亚 徐鸿钧 傅玉灿	博士生 教授 教授	052	基于模糊控制的感应钎焊金刚石系统研究	中国机械工程	2007, 18(10)
39	赵建社 徐家文 王福元	讲师 教授 副教授	052	整体构件数控电解加工数字化仿真技术	南京航空航天大学学报	2007,39(3)
40	赵建社 徐家文 朱永伟	讲师 教授 副教授	052	Design Optimization of Cathode's Feeding Path of NC-Electrochemical Machining Based on Computer Simulation of Shaping Process	Proceedings of the 15th International Symposium on Electromachining	2007,4
41	张伟 徐家文	硕士 教授	052	铝合金薄壁整体的数控电解加工试验研究	电加工与模具	2007, 4
42	王伟波 徐家文 赵建社	硕士 教授 讲师	052	微小整体构件加工技术的现状和探索	电加工与模具	2007, 4
43	杨卫平 徐家文	博士生 教授	052	用表面粗糙度测量仪测量材料微小去除量	工具技术	2007, 1
44	徐家文 郑健新 丁仕燕	教授 博士生 博士生	052	The Basic Experimental Research On the NC-Creep Feed Ultrasonic Assisted Grinding Ceramics	ISEM-XV	2007, 4
45	朱永伟 徐 峰 沈建良	教授 讲师 硕士生	052	Study on the Modification of Nanodiamond with DN-10	Journal of Material Science and Technology	2007,23(5)
46	沈建良 朱永伟	硕士生 教授	052	固结磨料抛光垫作用下的材料去除速率模型	中国科技论文在线	2007年4月17日
47	钟磊 卢文壮 王鸿翔 徐峰 左敦稳	硕士 副教授 博士生 讲师 教授	052	小型化金刚石膜沉积设备控制系统研究	硅酸盐通报	2007, 26(6)
48	卢文壮 左敦稳 徐峰	副教授 教授 讲师	052	“机械制造技术”课程的网络学习系统构建	电化教育研究	2007
49	何 宁 李 亮 赵 威 苏 宇	教授 副教授 讲师 博士生	052	难加工材料高性能加工的冷却润滑技术	航空制造技术	2007,7
50	苏 宇 何 宁 李 亮 徐 胜	博士生 教授 副教授 硕士生	052	新型切削用冷风发生装置的研制及性能测试	中国机械工程	2007,18(10)
51	苏 宇 何 宁 李 亮 A. Iqbal	博士生 教授 副教授 博士生	052	Refrigerated cooling air cutting of difficult-to-cut materials	International Journal of Machine Tools & Manufacture	2007,47(6)
52	苏 宇 何 宁 李 亮 徐 胜	博士生 教授 副教授 硕士生	052	INFLUENCE OF COLD NITROGEN GAS AND OIL MIST IN MACHINING NICKEL-BASE K424 ALLOY WITH CERAMIC CUTTING TOOLS	Transactions of Nanjing University of Aeronautics & Astronautics	2007,24(2)



53	汪通悦 何 宁 李 亮	博士生 教授 副教授	052	薄壁件铣削加工的振动模型	机械工程学报	2007,43(8)
54	汪通悦 何 宁 李 亮	博士生 教授 副教授	052	VIBRATION IN HIGH-SPEED MILLING OF THIN-WALLED COMPONENTS	Transactions of Nanjing University of Aeronautics & Astronautics	2007,24(2)
55	杨吟飞 李 亮 何 宁	博士生 副教授 教授	052	一种新的刀具磨损面图像边界提取 方法	南京航空航天大学学报	2007,39(6)
56	李多生 左敦稳 陈荣发 相炳坤 赵礼刚	博士生 教 授 副教授 讲 师 学 生	052	大尺寸金刚石膜生长中等离子体弧 源的稳定性	南京航空航天大学学报	2007, 9(3)
57	李多生 左敦稳 陈荣发 相炳坤 赵礼刚 王 珉	博士生 教 授 副教授 讲 师 学 生 教 授	052	直流等离子体CVD金刚石薄膜微观 结构分析	稀有金属材料与工程	2007, 36(4)
58	李多生 左敦稳 周贤良 华小珍 陈荣发 赵礼刚	博士生 教 授 教 授 教 授 副教授 学 生	052	Microdistortion behavior of Al alloy reinforced by sicp	Trans. Nonferrous Met. Soc. China	2007, 133(17)
59	徐 锋 左敦稳 卢文壮 王 珉	讲 师 教 授 副教授 教 授	052	Effect of Grid Bias on Deposition of Nanocrystalline Diamond films	TRANSACTION of NUAA	2007, 24(4)
60	徐 锋 左敦稳	讲 师 教 授	052	关于机械制造技术课程改革的探索 与实践	高校教育管理	2007, 1(4)
61	徐 锋 左敦稳 卢文壮 李 磊 王 珉	讲 师 教 授 硕士生 教 授	052	HFCVD 衬底三维温度场有限元模型	机械工程学报	2007, 43(6)
62	李 磊 左敦稳 徐 锋 黎向锋 卢文壮	硕士生 教 授 讲 师 副教授 副教授	052	HFCVD 系统中衬底接触热阻的研究	人工晶体学报	2007, 36(1)
63	张海余 左敦稳 徐 锋 闫 静	硕士生 教 授 讲 师 副教授	052	基于ANSYS的HFCVD金刚石厚膜的热 应力分析	人工晶体学报	2007, 36(1)
64	左敦稳 Kawano Yoshihi re	教 授	052	Application projection image of end mill to monitor its behaviour	Int. J. Computer Applications in Technology	2007, 28(1)
65	郭 魂 左敦稳 唐国兴	教 授	052	面向应用的“机电系统控制技术” 课程本科教学改革初探	装备制造技术	2007, (10)
66	于守鑫 孙玉利 左敦稳	硕士生 博士生 教 授	052	不同温度下单晶硅硬度的测试分析	扬州大学学报	2007, 1

67	于守鑫 左敦稳 卢文壮	硕士生 教授 副教授	052	硬质合金上镀铜	电镀与涂饰	2007, 26(1)
68	陈荣发 左敦稳 徐 锋 李多生 王 珉	博士生 教授 讲师 博士生 教授	052	Diamond Film Synthesis with a DC Plasma Jet: Effect of the Contacting Interface between Substrate and Base on the substrate Temperature	J. Mater. Sci. Technol	2007, 23(4)
69	陈荣发 左敦稳 孙玉利 卢文壮 李多生 王 珉	副教授 教授 博士生 副教授 博士生 教授	052	Investigation on the Machining of Thick Diamond Films by EDM Together with Mechanical Polishing	Advanced Materials Research	2007, 24-25
70	孙玉利 左敦稳 朱永伟 徐 锋 王 珉	博士生 教授 教授 讲师 教授	052	连续刚度法对单晶硅片的力学性能 的表征	硅酸盐学报	2007, 35(11)
71	孙玉利 左敦稳 朱永伟 王 珉	博士生 教授 教授 教授	052	Surface Formation of Single Silicon Wafer Polished with Nano-sized Al <sub>2</sub> O <sub>3</sub> Powders	CHINSE JOURNAL OF CHEMICAL PHYSICS	2007, 20(6)
72	孙玉利 左敦稳 朱永伟 陈荣发 李多生 王 珉	博士生 教授 教授 副教授 讲师 教授	052	Experimental study on Cryogenic Polishing Single Silicon Wafer with Nano-sized Cerium Dioxide Powders	Advanced Materials Research	2007,24-25
73	孙玉利 左敦稳 朱永伟 徐 锋 王 珉	博士生 教授 教授 讲师 教授	052	CHARACTRIZATION OF SURFACE LAYER OF SILICON WAFER BY USING NANO INDENTER	Proceodings of the International conference on Intergration and Commercialization of MNC 2007	2007
74	谢清华 谷 安 王梦珂	硕士生 讲师 硕士生	052	基于新型触须传感器的外形检测	自动化仪表	2007,02
75	谢清华 王梦珂 谷 安	硕士生 硕士生 讲师	052	位置敏感探测器(PSD)信号调理电路的改进	青岛科技大学报(自然科学版)	2007,01
76	但春华 谷 安 章 勇	硕士生 讲师 硕士生	052	机床数控系统掉电保护的研究与应用	电加工与模具	2007,S1
77	谢清华 谷 安 但春华	硕士生 讲师 硕士生	052	基于PSD的机器人触须传感器系统	机电一体化	2007,02
78	谷 安 谢清华	讲师 硕士生	052	机器人触须传感器动态工作机理的研究	传感器与微系统	2007,05
79	谷 安 谢清华	讲师 硕士生	052	机器人触须传感器工作机理的研究	仪器仪表学报	2007,S1
80	章 勇 谷 安 项甫根	硕士生 讲师 硕士生	052	基于DXF文件的低速走丝线切割加工自动编程系统的开发	电加工与模具	2007,05



81	朱 荻 王 昆 曲宁松	教 授 博士生 副教授	052	Micro Wire Electrochemical Cutting by Using In Situ Fabricated Wire Electrode	CIRP Annals - Manufacturing Technology	2007,56(1)
82	朱增伟 朱 荻 曲宁松 雷卫宁	博士生 教 授 副教授 教 授	052	Electrodeposition of bright nickel coating under perturbation of hard particles	Materials & Design.	2007, 28(6)
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## JET ELECTRODEPOSITED Cu-Al<sub>2</sub>O<sub>3</sub> NANOCOMPOSITE COATINGS

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### ABSTRACT

A jet electrodeposition device was carried out to prepare Cu-Al<sub>2</sub>O<sub>3</sub> nanocomposite coatings. The influence of the concentration of Al<sub>2</sub>O<sub>3</sub> in the electrolyte and parameters, such as cathodic current density, the electrolyte temperature as well as the electrolyte jet velocity, on the content of the Al<sub>2</sub>O<sub>3</sub> in the deposit were investigated. The coatings ingredient and microstructure was measured by the scanning electron microscope (SEM) with energy dispersive analyzer system (EDX), the microhardness tests were conducted on a microhardness tester. The results show that the jet electrodeposition can form fine crystalline particles. The copper deposited layers have nanocrystalline microstructure with grain size of about 50nm. The amount of Al<sub>2</sub>O<sub>3</sub> in composites first increased and then decreased with an increase in the concentration of Al<sub>2</sub>O<sub>3</sub>, current density, temperature and jet velocity. The composite with optimum atomic percent of Al<sub>2</sub>O<sub>3</sub> (14.4 at%) can be obtained at the concentration of 30 g/l, cathodic current densities 300 A/dm<sup>2</sup>, temperature 30°C, and electrolyte jet velocity 8 m/s. The addition of Al<sub>2</sub>O<sub>3</sub> in copper increases the microhardness of the electrodeposited coatings.

Keywords: jet, electrodeposition, nanocrystalline, current density, grain size, nanocomposite coatings

Metal-matrix nanocomposites are materials in which the properties of a metallic host material are modified with the addition of a second phase. Electrodeposition of nanocomposite coatings, based on second phase hard particles dispersed in a metallic matrix, is gaining importance for potential engineering applications. The second phase can be hard oxide (Al<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub>, SiO<sub>2</sub>) or carbides particles (SiC, WC). However, the very low depositing rate of the conventional electrodeposition has limited the practical application of electrodeposition as a means to prepare the composite materials. Then, the jet electrodeposition as a new technique with the special flow characteristics, has been used for local coating reaction on an unmasked cathode. During the jet electrodeposition process, the electrolyte is jetted on a cathode surface directly because of the existence of electric field between the cathode and anode located in the jet nozzle, as the electric current travels along the jet stream to the cathode, the deposition takes place only on the local cathode surface area where the jet impinges on. Thus, jet electrodeposition possesses high depositing rate. In addition, the grain size refining effect of jet electrodeposition is more efficient because a much higher overpotential of cathodic substrate can be used with much higher current density. The articles reported that the deposit layer has crystalline microstructure.

### 1. INTRODUCTION

### 2. EXPERIMENT



## 2-1. Experimental principle

The schematic representation of the equipment and measurement circuit of jet electrolyte conducted in the cell are shown in Fig. 1. The electrolyte was pumped from the vessel with invariable temperature electrolyte, and then reflowed to the vessel from the output of electrodepositing room via the bump of filter, and the flowmeter. The electrolyte temperature was measured by the heater and temperature transducer. the jet velocity was adjusted by control valve.

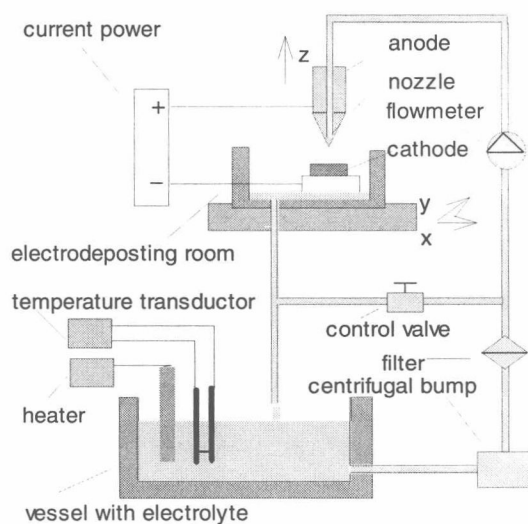


Fig.1. Diagram of measurement circuit applied for jet electrodepositing .

## 2-2. Electrolyte ingredient and experimental parameters

A initially device was designed for the fabrication of composite coatings. A electrolyte was used to deposition on the flat stainless steel substrate under the following condition:

electrolyte:	$\text{Cu}_2\text{SO}_4 \cdot 5\text{H}_2\text{O}$ (250 g/l); $\text{H}_2\text{SO}_4$ (50 g/l)
concentration of $\text{Al}_2\text{O}_3$ (50 nm):	10-40 g/l
current densities:	200-500 A/dm <sup>2</sup>
jet velocity:	4 -10 m/s
temperature:	20-40 °C
pH:	4.0

## 2-3. Composition analysis

The composites ingredient and microstructure was measured by using a field emission scanning electron microscope with energy dispersive analyzer system (EDX). The SEM samples were vibrated by ultrasonic vibrator and washed in distilled water and alcohol. Vickers microhardness tests were conducted on an HXS-1000A microhardness tester using a load of 50 g, applied for 10 s. Each hardness value was an average of five measurements.

## 3. RESULTS

### 3-1. Effect of concentrations and current density

The incorporation of  $\text{Al}_2\text{O}_3$  in the copper deposit with different contents (10–40 g/L) of  $\text{Al}_2\text{O}_3$  particles suspended in the electrolyte at current densities 300 A/dm<sup>2</sup>, 30 °C and jet velocity 8 m/s , pH 4.0 is shown in Fig. 2(a). According to the data obtained, the at% of  $\text{Al}_2\text{O}_3$  in the deposit increases sharply with increasing the concentration of  $\text{Al}_2\text{O}_3$  in the electrolyte and attains the optimum values at 14.4 at% at 30 g/l  $\text{Al}_2\text{O}_3$  suspension in the bath. With further additions, the amount of  $\text{Al}_2\text{O}_3$  slightly decreases. These phenomena play an especially considerable role in particle codeposition with copper, due to the high adsorption affinity of copper for the solid particles. The data obtained in this investigation can be explained in terms of adsorption of  $\text{Al}_2\text{O}_3$  on the cathode surface. With increased amount of  $\text{Al}_2\text{O}_3$  in the electrolyte copper will be deposited with a higher amount of  $\text{Al}_2\text{O}_3$  and a large area of the cathode surface covered. The optimum value of  $\text{Al}_2\text{O}_3$  (14.4 at%) means that the all surface area of the cathode is approximately covered with  $\text{Al}_2\text{O}_3$  and copper ions.

The current density on the cathode surface is a measure of the volume of  $\text{Al}_2\text{O}_3$  in the deposit. The effect of current density on the at% of the  $\text{Al}_2\text{O}_3$  incorporation in the deposits at 30 g/l  $\text{Al}_2\text{O}_3$ , pH 4.0, 30 °C. particles in the bath is shown in Fig. 2(b). It was found that, the at% of  $\text{Al}_2\text{O}_3$  increases with increasing current densities and maximum incorporation (14.0 at%) could be achieved at 400 A/dm<sup>2</sup>. With further increase in the current densities than 400 A/dm<sup>2</sup>, the extent of codeposition of  $\text{Al}_2\text{O}_3$  decreases to 12.0 at% at 500 A/dm<sup>2</sup>. As the current density increases the solution in the vicinity of the cathode tends to become depleted of metallic ions and polarization increases and codeposition rate increases, the content of  $\text{Al}_2\text{O}_3$  adsorbed on the cathode increases. The maximum current density is reached when the rate of movement of metallic ions and  $\text{Al}_2\text{O}_3$  particles from the bulk solution to the

cathode surface is equal to the rate of deposition. At current density above  $500 \text{ A/dm}^2$ , the metal is being deposited under conditions of charge transfer overpotential control. As a result, the reduction of copper ions is controlled by concentration overpotential, the amount of codeposition of  $\text{Al}_2\text{O}_3$  particles gradually decreases.

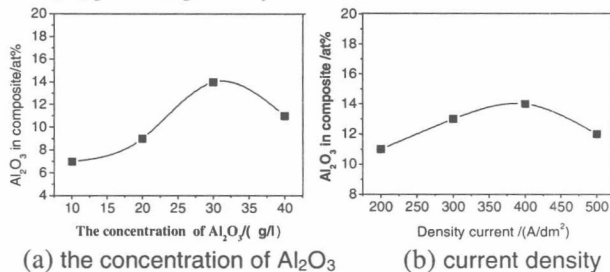


Fig. 2 The at% of  $\text{Al}_2\text{O}_3$  in composite.

### 3-2. Effect of electrolyte temperature and jet velocity

The influence of electrolyte temperature (20–40 °C) on  $\text{Al}_2\text{O}_3$  incorporation at 30 g/l  $\text{Al}_2\text{O}_3$ , current densities  $300 \text{ A/dm}^2$ , jet velocity 8 m/s, and pH 4.0 is shown in Fig. 3(a). It is clear that the temperature of the solution noticeably influences the amount of  $\text{Al}_2\text{O}_3$  in deposit. The result indicates that  $\text{Al}_2\text{O}_3$  incorporation increases from 11.2 at% at 20 °C to 14.4 at% at 30 °C. With further increase of the temperature, a decreasing trend is observed, resulting from decrease in the current efficiency of the bath. The electrolyte jet velocity also plays an important role in the electrodeposition process for the transportation of  $\text{Al}_2\text{O}_3$  particles to the cathode for the codeposition. Fig. 3(b) shows the effect of jet velocity on the at% of  $\text{Al}_2\text{O}_3$  in the composite at pH 4.0, 30 °C, current densities  $300 \text{ A/dm}^2$ , and 30 g/l  $\text{Al}_2\text{O}_3$  in the electrolyte. It is seen that the amount of  $\text{Al}_2\text{O}_3$  in the composite increases with increasing jet velocity up to 8 m/s. The highest at% of  $\text{Al}_2\text{O}_3$  in the composite is obtained at 8 m/s. The at% of  $\text{Al}_2\text{O}_3$  in the composite decreases beyond 8 m/s.

Increasing the jet velocity of the electrolyte flow in jet deposition is equivalent to increasing the stirring intention of the electrolyte. This results in the reduction of the diffusion layer thickness and it is accompanied by the increasing of the metallic ion concentration in the diffusion layer. The  $\text{Al}_2\text{O}_3$  particles concentration in the diffusion layer is therefore increased. Hence, the increasing of jet velocity results in the increase of  $\text{Al}_2\text{O}_3$  content in the deposit. Under high jet velocity, the  $\text{Al}_2\text{O}_3$  particles

absorbed on the cathode are partly taken away, which resulted in a decreased amount of the  $\text{Al}_2\text{O}_3$  codeposition.

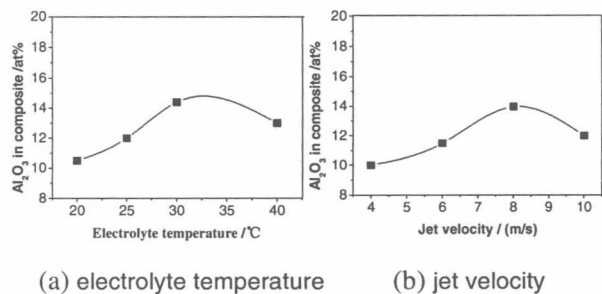


Fig. 3 The at% of  $\text{Al}_2\text{O}_3$  in composite.

### 3-3 Surface microstructure analysis

The SEM surface morphologies of electrodeposited pure Cu and Cu- $\text{Al}_2\text{O}_3$  nanocomposites is represented in Fig. 4. It shows that there is the formation of finer grains in the deposited layer. It seems as compact and smooth.

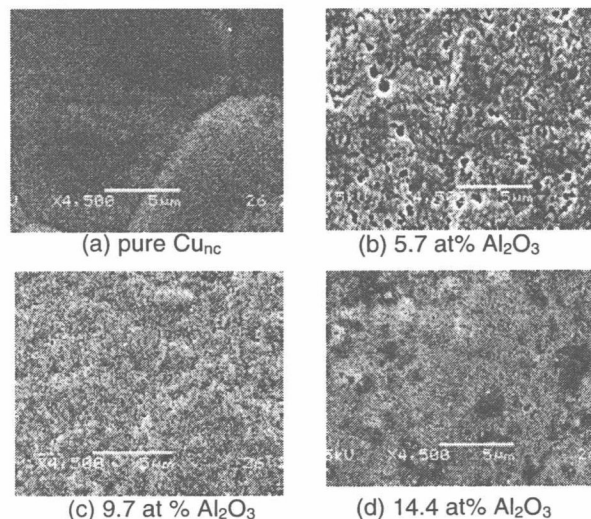


Fig. 4 SEM surface micrographs of the copper

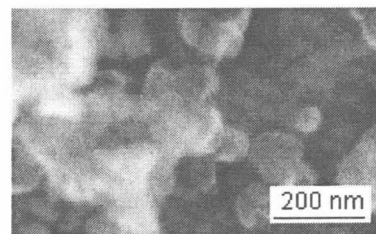


Fig. 5 SEM image of deposited layer.

Fig.5 is a high magnified view of Fig.6(d), displaying the typical nanostructure of copper electrodeposite layer, it clear see that average grain size is various from 50nm to 60nm evaluating by the staff in SEM graph.

### 3-4 Microhardness

The microhardness of materials depends upon many factors and the most important factor is the composition of the electrodepositing bath. The relation between the incorporation of  $Al_2O_3$  in deposit and microhardness is shown in Table 1.

Tab.1 Microhardness of  $Cu_{nc}-Al_2O_3$  composite coatings

Example	Microhardness/GPa
Crude Cu	0.2
pure $Cu_{nc}$	1.2
$Cu_{nc}/Al_2O_3$ (5.7 at%)	1.7
$Cu_{nc}/Al_2O_3$ (9.0 at%)	1.9
$Cu_{nc}/Al_2O_3$ (14.4 at%)	2.1

The results indicate that the pure  $Cu_{nc}$  provide the far higher microhardness than crude Cu, it is up to 1.2 Gpa , about 6 time as high as the latter, additional , the incorporation of  $Al_2O_3$  particles with copper also gives much higher values . The hardness increases with increasing of the  $Al_2O_3$  particles in the deposit. The higher hardness is produced due to the dispersion hardening effect of the  $Al_2O_3$  particles and also as a result of the fine-grained structure of the composites. During microhardness measurements, the dispersed particles in the fine-grained matrix may obstruct the easy movement of dislocations and resist plastic flow. This resistance to deformation is shown by an increasing hardness value for Cu- $Al_2O_3$  composite.

### 4. CONCLUSIONS

The results of this investigation suggest some general conclusions, which can be summarized as follows.

1. The electrodeposited layer grain size was greatly finned because of supply of much more current density nanostructured composites were obtained through jet electrodeposition.

2. The amount of  $Al_2O_3$  in composites first increased and the decreased with an increase in the concentration of  $Al_2O_3$ , cathodic current density, eletrolyte temperature and jet velocity. The composite with maximum value (14.4 at%)

can be obtained at the concentration of 30 g/l current densities 300 A/dm<sup>2</sup>,electrolyte temperature 30 °C,and jet velocity 8 m/s.

3. The microhardness of the composites increases gradually in the direction of the growth of the deposit. The top hardness is high up to 2.1Gpa.

### ACKNOWLEDGEMENTS

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## A STUDY ON THE ELECTRODEPOSITED CU-AL<sub>2</sub>O<sub>3</sub> COMPOSITES COATING WITH LASER TREATMENT

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### ABSTRACT

One kind of jet electrodeposition machine with multi-spindle function has been successfully designed and launched. With the jet electro-deposition device, Al<sub>2</sub>O<sub>3</sub> particles of average size 30 nm were co-deposited with Copper on a steel substrate using a Watts bath at 50°C and the compound layer was processed by laser in order to make the layer clad on the substrate in a well binding force. The compound layer's microstructure was examined by scanning electron microscopy (SEM), the mechanical properties of the coated steels were examined with hardness and tensile tests. The effects exerted by the current density, weight percentage of Al<sub>2</sub>O<sub>3</sub> in electrolyte and the presence of laser treatment was investigated respectively. It shows a relatively small current density and a certain of Al<sub>2</sub>O<sub>3</sub> particles have a positive effect on both surface morphology and coated material's mechanical behavior. In addition, result also shows the coating processed by laser, attained a hardness up to 820 HV, which is considerably increased than substrate.

Keywords: electrodeposition; copper; nanosized Al<sub>2</sub>O<sub>3</sub>; laser; Mechanical properties;

### 1. INTRODUCTION

30CrMnSiA is a kind of high strength structural steel, which has been found well suited for applications on aircraft and aerospace vehicles manufacturing. To improve wear performance and strength, as well as other surface properties such as oxidation and corrosion, these materials are generally surface coated and the resulting coatings are expected to achieve a particular property. Nowadays, many surface techniques have been applied to improve the surface properties

of metals. Among them, electro methods are considered as the comparatively economical ways involved in surface modification [1]. Electrodeposition of composite coatings, based on hard particles dispersed in a metallic matrix, is attracting much interest in recent years.

The second phase in composite particles can be hard oxide (Al<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub>, SiO<sub>2</sub>), carbides particles (SiC, WC), diamond, solid lubricate (PTFE, graphite, MoS<sub>2</sub>), and even liquid containing microcapsules [2].

However, due to the limit of electro chemistry mechanism, the mechanical bond of deposit layer and substrate tends to break away and shell under adequate force outside. As a potential solution, the present work was undertaken, by conducting the intensification of laser surface with deposit coating. A new method called jet electrodeposit was used to deposit a Copper-nanoAl<sub>2</sub>O<sub>3</sub> layer and another procedure of laser scanning on compound layer follows last one to melt the layer to turn mechanical bond between deposit layer and matrix into a metallurgical bond, thereby strengthening the binding force and enhancing the characteristics of the material [1][2].

The compound layer was examined by microhardness measurements, stretch test and scanning electron microscopy (SEM) in this work.

### 2. EXPERIMENTAL DEVICE AND PARAMETER SET

The Jet electrodeposition system is composed of CNC unit and electrolyte circulation unit. CNC unit includes industrial PC, software and servo system, in charge of the desired movements of nozzle. Electrolyte circulation unit was responsible for the management of electrochemistry parameters including voltage, current, and temperature.



The schematic representation of the equipment and measurement circuit of jet electroplating is shown in Fig 1. The apparatus fundamentally consists of an electrodepositing section, a set of circulation system and stirrer.

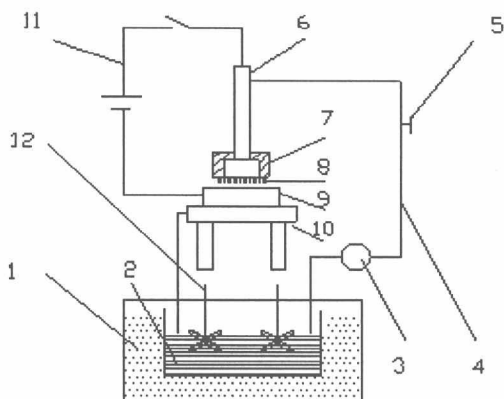


Fig.1. Schematic diagram of circuit applied for jet electrodeposition. (1) normal temperature water bath for electrolyte; (2) electrolyte; (3) pump; (4) PVC pipe; (5) electrolyte valve; (6) Cu anode; (7) nozzle; (8) electrolyte stream; (9) substrate (cathode); (10) worktable; (11) power supply and current circuit; (12) churn-dasher

Table 1. Composition of the electrolytic

Electrolyte Material	Amount(g/L)
$\text{CuSO}_4 \cdot 5\text{H}_2\text{O}$	250
Surfuric. acid	50
Dodecyl sodium sulphate	0.1

### 3. EXPERIMENTAL PROCEDURE

To provide uniform surface activity, prior to electrodeposition, cleaning and conditioning treatments were necessary to be performed on 30CrMnSiA with the following steps. Initially, the substrate was polished with diamond abrasive to obtain an extreme smooth surface and degreased with acetone to remove oil and grease. Further more, 30CrMnSiA should be fully immersed in 15% nitric acid for 20 minutes to clear away rust and other contamination [3].

After cleaning, specimens were immediately taken on the electrolytic worktable as a cathode. The electrolyte's temperature was kept around 50 °C through the whole experiment and the composition of electrolyte was given in Table 1. In procedure, nozzle, controlled by CNC, continued scanning backwards and forwards along the worktable with a constant distance of 1 mm between anode (nozzle) and cathode (substrate). For an optimal deposition, the cathode current was precisely set in a range of 0.01 to 0.1 A. All the electrodeposition experiments were carried out in the bath for 1 h with constant stirring by a magnetic stirrer so that all the

$\text{Al}_2\text{O}_3$  particles could be sufficiently wetted and remained suspended uniformly in the electrolyte.

One 2 kW transverse-flow  $\text{CO}_2$  laser made by Prima Laser Machinery Company, was used to melt the electrodeposited compound layer together with 30CrMnSiA substrate. Laser process was performed with optimized parameters, including laser power of 1 KW, scan speed of 1 m per min, a constant beam diameter of 3 mm. Fig 2 illustrates the process.

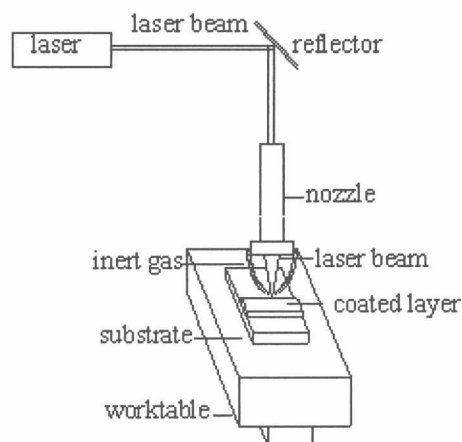


Fig. 2. Diagram of laser processing on the compound deposition layer

### 4. RESULTS AND DISCUSSION

#### 4-1. Effects from nanosized $\text{Al}_2\text{O}_3$ on surface morphology of deposition layer

Fig 3 shows surface morphology, which was respectively obtained under different current density. From SEM, we can find under a condition of low current density, a flat coating surface on which the grain size seems obviously decreased can be obtained. With the current increasing, coating surface begins with a transition to growth morphology of cystiform grain. On the contrary, when the current was set relatively high, a dramatically growth of cystiform grain occurred and as a response, a tendency of deposit layer deteriorating off compactness and flatness appeared in the end.

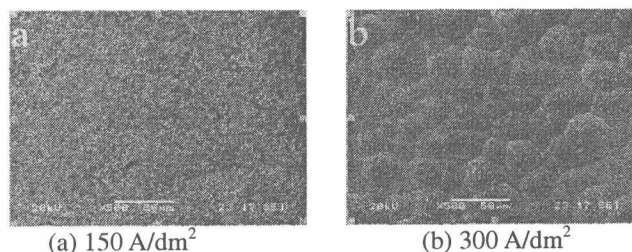


Fig.3. SEM photographs of Cu- $\text{Al}_2\text{O}_3$  layer with relatively low current density